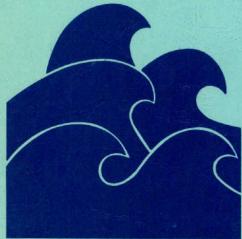
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ANALYTICAL STUDY OF THE OGALLALA AQUIFER IN POTTER AND OLDHAM COUNTIES, TEXAS Projections of Saturated Thickness, Volume of Water in Storage, Pumpage Rates, Pumping Lifts, and Well Yields

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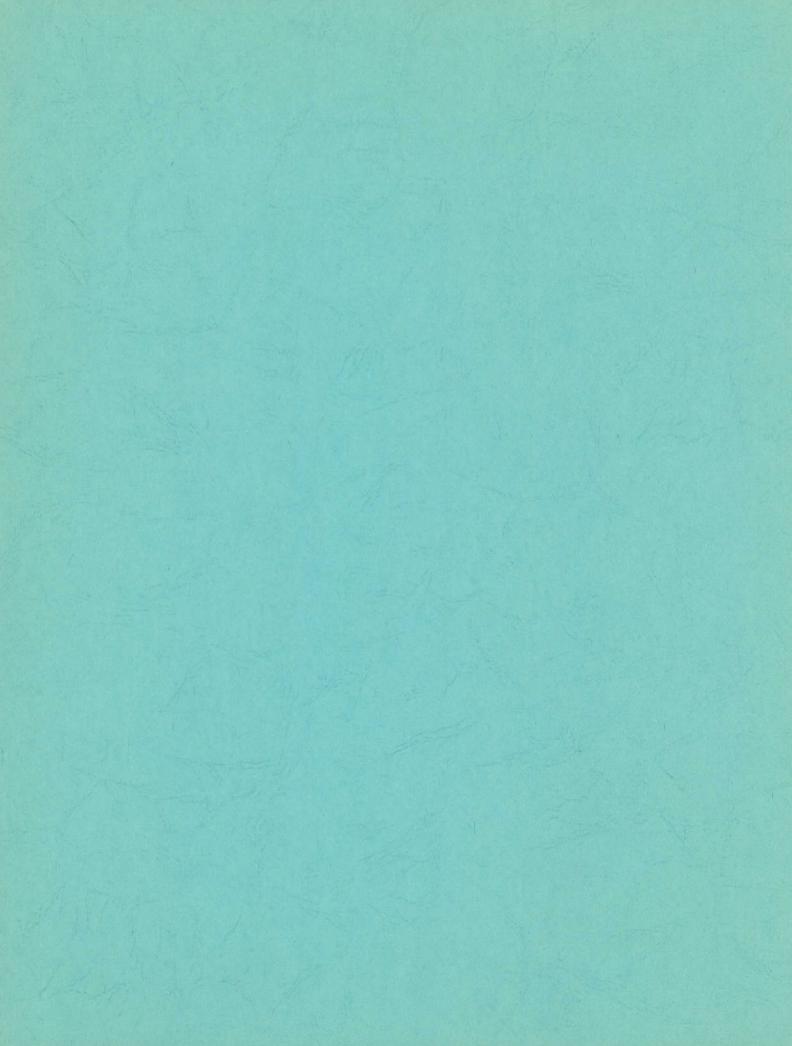
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TEXAS DEPARTMENT OF WATER RESOURCES

January 1982





TEXAS DEPARTMENT OF WATER RESOURCES

REPORT 265

ANALYTICAL STUDY OF THE OGALLALA AQUIFER IN POTTER AND OLDHAM COUNTIES, TEXAS Projections of Saturated Thickness, Volume of Water in Storage,

Pumpage Rates, Pumping Lifts, and Well Yields

By

Ann E. Bell and Shelly Morrison

January 1982

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ANALYTICAL STUDY OF THE OGALLALA AQUIFER IN POTTER AND OLDHAM COUNTIES, TEXAS

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Projections of Saturated Thickness, Volume of Water in Storage,

Pumpage Rates, Pumping Lifts, and Well Yields

CONCLUSIONS

The Ogallala aquifer in Potter and Oldham Counties contained approximately 2.1 million acre-feet (2.6 km^3) of water in 1974. Historical pumpage has exceeded 50,000 acre-feet (0.06 km^3) annually, which is approximately twice the rate of natural recharge to the aquifer in the counties. This overdraft is expected to continue, ultimately resulting in reduced well yields, reduced acreage irrigated, and reduced agricultural production.

There is a very uneven distribution of ground water in the two counties. Some areas have ample ground-water resources to support current usage through the year 2020; whereas, in other areas, ground water is currently in short supply.

To obtain maximum benefits from the remaining ground-water resources, water users should implement all possible conservation measures so that the remaining ground-water supply is used in the most prudent manner possible and with the least amount of waste.

INTRODUCTION

Potter and Oldham Counties are situated in the High Plains of Texas. Vega, the county seat of Oldham County, is located approximately 30 miles (48 km) west of Amarillo, the county seat of Potter County. The counties have a total population of approximately 96,200 and contain a total area of about 2,376 square miles (6,154 km²), of which approximately 1,190 square miles (3,082 km²) is underlain by the Ogallala Formation. This report deals only with that area of the counties where the Ogallala Formation occurs.

Potter and Oldham Counties produce a total farm income of over \$22 million annually (Texas Almanac

and State Industrial Guide 1978-79). Leading crops in these counties are grain sorghums and wheat. Livestock feeding accounts for two-thirds of the farm income, while other agribusinesses, including the sale of irrigation equipment supplies, feed and seed, and fertilizer, also make significant contributions to the total two-county income.

Ground water is extremely important to the economy of the area inasmuch as most of the crops are irrigated with ground water. Additionally, the water used by rural residents, municipalitites, and local industries is mostly ground water.

The principal source of fresh ground water in the area is the Ogallala aquifer. During the past three decades, the withdrawal of ground water has greatly exceeded the natural recharge to the aquifer. If this



Location of Potter and Oldham Counties, and Extent of the Ogallala Aquifer in Texas

overdraft continues, the aquifer ultimately will be depleted to the point that it may not be economically feasible to produce water for irrigation.

This is one of numerous planned county studies covering the declining ground-water resource of the Ogallala aquifer in the High Plains of Texas. The report contains maps, charts, and tabulations which reflect estimates of the volume of water in storage in the Ogallala aquifer in Potter and Oldham Counties and the projected depletion of this water supply by decade periods through the year 2020. The report also contains estimates of pumpage, pumping lifts, and other data related to current and future water use in the counties. However, the report does not attempt to project that portion of the volume of water in underground storage which may be ultimately recoverable.

PURPOSE AND SCOPE OF STUDY

This study resulted from an immediate need for information to illustrate to the High Plains water users that the ground-water supply is being depleted. It is hoped that this study will help persuade the water users to implement all possible conservation measures, so that the remaining ground-water supply will be used in the most prudent manner possible and with the least amount of waste.

The study was also conducted to provide information to local, State, and federal officials for their use in implementing plans to alleviate the water-shortage problem in the High Plains of Texas.

These immediate needs for current information have resulted in a concerted effort by the Texas Department of Water Resources to utilize high-speed computers to conduct evaluation and projection studies of ground-water resources. The results of one of these computer studies is contained in this report.

This report does not represent a detailed ground-water study of the two counties; rather, the report was prepared using only those data which were readily available in the files of the Texas Department of Water Resources. Information provided for 1974 is considered reliable; however, the projections of future conditions should be used only as a guide to reasonable expectations.

This study represents a new approach by the Department in making and presenting appraisals of ground-water resources. Consequently, a detailed explanation of the methods and assumptions used in the study is included. A complete set of tabulations and illustrations resulting from this study is presented at the end of the report.

The illustrations were prepared to answer four questions believed to be of prime importance to the Potter and Oldham County landowners and water users. These questions, and methods by which a set of answers can be obtained from the illustrations, are as follows:

> 1. Question: How much water is in storage under any given tract of land and what is expected to happen to this water in the future?

> > Answer: First, determine the approximate location of the tract on the most current (1974) map of saturated thickness. Read the value of the contour line at this location (if midway between two contour lines, take an average of the two). This thickness value can then be converted to the approximate volume of water in storage, in acre-feet per surface acre, by multiplying it by the coefficient of storage of 0.15, or 15 percent. To obtain estimates of what can be expected in the future, the same procedure can be followed by using the maps which illustrate projected saturated thickness in the years 1980, 1990, 2000, 2010, and 2020.

 Question: What can be expected to happen to well yields if the saturated thickness diminishes as illustrated by the maps?

> Answer: Well yields are expected to decline as the aquifer thins; therefore, a map of estimated well yields has been prepared for each year of the study. The landowner need only find the approximate location of his property on the well-yield map that applies to the year in question and read the well-yield estimates directly from the map.

3. Question: With energy cost increasing, pumping lifts (pumping levels) are becoming more and more important. What are the estimates of current pumping lifts and what are they expected to be in the future?

> Answer: Contour maps depicting estimated pumping lifts have been prepared for each year of the study. These maps are contoured in feet below land surface. The landowner need only find the approximate location of his property on the map that applies to the year in question to read the pumping-lift estimates.

4. Question: If an all-out effort is made to conserve ground-water resources, how can landowners and water users determine how they are doing compared to the projections in the study?

> Answer: Using the maps that show rates of water-fevel declines, the landowners and water users can determine what the changes in water levels are in their area and what they are projected to be in the future. This can be accomplished by finding the approximate location of their property on the map pertaining to the year in question and by reading the estimates of water-level changes which are recorded in feet. To determine how he is doing from year to year, the landowner or water user can make measurements of depth to water in his own wells or obtain copies of measurements made by the Department or the ground-water district for his area. These measurements can then be compared to the projected values on the map nearest to the year of interest to obtain an estimate of the effectiveness of the conservation efforts.

NATURE OF THE OGALLALA AQUIFER

Because thorough understanding of the Ogallala aquifer is not necessary for the water user, the following discussion of aquifer geology and hydrology is rather general. Readers interested in pursuing the subject in more detail may do so from the numerous reports which have been published on the Ogallala. Many of these publications are included in the list of selected references of this report.

General Geology

Fresh ground water in Potter and Oldham Counties is obtained prinicipally from the Ogallala Formation of Pliocene age. Water in the Ogallala Formation is unconfined and is contained in the pore spaces of unconsolidated or partly consolidated sediments.

The Ogallala Formation principally consists of interfingering bodies of fine to coarse sand, gravel, silt, and clay-material eroded from the Rocky Mountains which was carried southeastward and deposited by streams. The earliest sediments, mainly gravel and coarse sand, filled the valleys cut in the pre-Ogallala surface. Pebbles and cobbles of guartz, guartzite, and chert are typical of these early sediments. After filling the valleys, deposition continued until the entire area that is now the Texas High Plains was covered by sediments from the shifting streams.

The upper part of the formation contains several hard, caliche-cemented, erosionally resistant beds called the "caprock." A wind-blown cover of fine silt, sand, and soil overlies the caprock.

The Ogallala deposits overlie rocks of Triassic and Permian ages. These rocks, principally red shale, serve as a nearly impermeable floor for the aquifer. On a broad scale, the erosional surface at the top of the Triassic and Permian rocks dips gently (about 10 feet per mile [2 m/km]) toward the southeast, similar to the slope of the land surface. In general, however, this pre-Ogallala surface had greater relief than the present land surface. Low hills and wide valleys which contain deep, narrow stream channels are typical features of the Triassic and Permian erosional surfaces. Because the Ogallala was deposited on top of this irregular surface, the formation is very thin in some areas and very thick in others. Often this contrast occurs in relatively short distances.

The Canadian River has cut deeply through the Ogallala Formation in the northern part of the Texas High Plains area. The valley effectively separates the formation geographically into two units having little hydraulic interconnection. Erosion has also removed the Ogallala from much of its former extent to the east, and to the west in New Mexico. As a result, the Southern High Plains, although relatively flat, stands in high relief and is hydraulically independent of adjacent areas. For this reason, coupled with the scarcity of local rainfall, water that is being withdrawn from the aquifer cannot be replaced quickly by natural recharge and is in effect being mined.

Storage Properties

The coefficient of storage of an aquifer is defined as the volume of water released from or taken into storage per unit surface area of the aquifer per unit change in the component of head normal to that surface. In water-table aquifers such as the Ogallala, the coefficient of storage is nearly equal to the specific yield, which is defined as the quantity of water that a formation will yield under the force of gravity, if it is first saturated and then allowed to drain, the quantity of water being expressed as a percentage of the volume of the material drained.

A coefficient of storage of 15 percent has been selected for use in this study based on past studies and the results of numerous aquifer tests published in Texas Water Development Board Report 98 (Myers, 1969). The following chart shows the volumes of water corresponding to various amounts of aquifer saturated thickness, based on a storage coefficient of 15 percent. These are the approximate amounts of water that would drain from the aquifer material by gravity flow if the entire saturated thickness could be drained.

SATURATED THICKNESS (feet)	VOLUME OF WATER IN STORAGE (acre-feet, per surface acre)
25	3.75
50	7.50
75	11.25
100	15.00
150	22,50
200	30.00
250	37.50
300	45.00
400	60.00
500	75.00

Natural Recharge and Irrigation Recirculation

Recharge is the addition of water to an aquifer by either natural or artificial means. Natural recharge results chiefly from infiltration of precipitation. The Ogallala aquifer receives natural recharge by precipitation that falls within the county boundaries and in adjoining areas.

The amount and rate of natural recharge from precipitation depend on the amount, distribution, and intensity of the precipitation; the amount of moisture in the soil when the rain or snowmelt begins; and the temperature, vegetative cover, and permeability of the materials at the site of infiltration. Because of the wide variations in these factors, it is difficult to estimate the amount of natural recharge to the ground-water reservoir. Estimates of annual natural recharge to the Ogallala aquifer made by Barnes and others (1949, p. 26-27) indicate only a fraction of an inch. Theis (1937, p. 546-568) suggested less than half an inch, and Havens (1966, p. F1), in a study of the Ogallala in New Mexico, indicated about 0.8 inch (2 cm) per year.

The authors of this report believe that recharge from precipitation may be more than these earlier estimates, due to changes in the soil and land surface that have accompanied large-scale irrigation development in the area. Some of the farming practices which are believed to have altered the recharge rate are: clearing the land of deep-rooted native vegetation; deep plowing of fields, which eliminates compacted zones in the soil (locally called "hard pans"), and the plowing of playa fake bottoms and sides; bench leveling, contour farming, and terracing; maintaining a generally higher soil moisture condition by application of irrigation water prior to large rains; and increasing the humus level in the root zone by plowing under a large amount of foliage from crops grown under irrigation.

Obtaining a reliable estimate of the present recharge rate is further complicated by the consideration which must be given to irrigation recirculation. A substantial portion of the water pumped from the Ogallala for irrigation percolates back to the aquifer. This does not constitute an additional supply of water, but reduces the net depletion of the aquifer. As with natural recharge, many factors are involved in making estimates of recirculation. Some of these factors are the rate, amount, and type of irrigation application; the soil type and the infiltration rate of the soil profile in the root zone; the amount of moisture in the soil prior to the irrigation application; the type of crop being grown, its root development, and its moisture extraction pattern; and the climatic conditions during and following the irrigation application. Tentative estimates of the actual amounts of recharge and irrigation recirculation in Potter and Oldham Counties will be found in a subsequent section on "Calculating Pumpage."

PROCEDURES USED TO OBTAIN PROJECTIONS

Hydrologic Data Base

The Texas Department of Water Resources, the High Plains Underground Water Conservation District No. 1, and the Panhandle Ground Water Conservation District No. 3 cooperatively maintain a network of water level observation wells in Potter County, while the Department exclusively maintains a similar network in Oldham County. Records from these wells provided the principal data base used in this study. This data base was supplemented in some areas with records from water well drillers' logs collected by both the Districts and the Department.

The data base included: (1) measurements of the depth to water below land surface, which have been made annually in the wells in the observation network; (2) the dates these measurements were made; and (3) the depth from land surface to the base of the Ogallala aquifer (In many cases, this was identical to the well depth). To facilitate automatic data processing with modern, high-speed computers, the data base also

included a unique number for each well and the geographical coordinates of each well location.

Wells chosen from the data base for use in obtaining projections of future conditions were those in which depth to the base of the aquifer could be determined or estimated, and those needed to provide spaced data coverage in the two counties. Locations of the wells that were selected and used for control are shown on the various maps in this report.

Projecting the Depletion of Saturated Thickness

The water-use patterns between 1960 and 1972 as reflected in the changes in water levels in wells measured in the High Plains of Texas were used as the principal data source for developing an aquifer depletion schedule. The depletion schedule generally reflects average precipitation and precipitation distribution in the area for the duration of the study period. Additionally, in developing and applying the depletion schedule, adjustments through time were made to reflect the effects of depletion of the aquifer on its ability to yield water. That is, as the aquifer's saturated thickness decreases, its ability to yield water to wells is reduced, the well yields decline, less water is pumped, and there results a lessened rate of further aquifer depletion.

The aquifer's hydraulics are such that if a well penetrates the total saturated section and the pump is sized to produce the maximum the aquifer will yield, the well yield will decline at a disproportionately greater rate than the reduction in saturated thickness. Actually, the remaining well yield expressed as a percentage of former yield will be only about half of the remaining saturated thickness expressed as a percentage of former thickness. For example, a well with 60 feet (18.3 m) of saturated section and a maximum yield of 900 gallons per minute (56.8 l/s) will probably yield only 225 gallons per minute (14.2 l/s) when the saturated section is reduced to 30 feet (9.1 m).

The depletion schedule for Potter, Oldham, and surrounding counties was developed in the following manner:

1. The records for all water level observation wells for the years 1960 through 1972 in Armstrong, Carson, Donley, Gray, Oldham, Potter, Randall, and Wheeler Counties were separated from the master file. These counties have similar soil types, cropping patterns, depths to water, saturated thickness, and climatic conditions.

- These well records were then sorted into groups according to the saturated thickness in each well as of 1966 (the middle year). Each group included records of all wells in a 20-foot (6.1-meter) range of saturated thickness. (Ranges are shown in the tabulation below.)
- 3. The average decline in water level was calculated for each year for each well group, and these decline values were adjusted to remove the effects of each year's deviation from long-term average precipitation.
- 4. The average annual decline in water level for the total period (1960-72) was calculated for each well group, incorporating the adjustments for departure from average precipitation.

From the foregoing procedure, the following depletion schedule was developed (no depletion was allowed for areas with 10 feet or less of saturated thickness):

D to 10 0.00 10 to 20 .40 20 to 40 .85	RANGE OF SATURATED THICKNESS (feet)	AVERAGE ANNUAL WATER-LEVEL DECLINE, 1960-72 (feet)
10 to 20 .40 20 to 40 .85		I
20 to 40 .85	0 to 10	0.00
	10 to 20	.40
10	20 to 40	.85
40 to 60 1.47	40 to 60	1.47
60 to 80 1.60	60 to 80	1.60
80 to 100 1.80	80 to 100	1.80
100 to 120 2.07	100 to 120	2.07
120 to 140 2.56	120 to 140	2.56
140 to 160 2.50	140 to 160	2.50
160 to 180 2,47	160 to 180	2.47
180 to 200 3.04	180 to 200	3.04
200 to 220 2.97	200 to 220	2.97
220 to 240 2,87	220 to 240	2,87
240 to 260 3.49	240 to 260	3.49
260 to 280 4.05	260 to 280	4.05

Based on this depletion schedule, a computer program was written to calculate future saturated thickness at individual well sites. The following problem is presented to show the computational procedures used.

Problem: A well has a saturated thickness of 110 feet in 1974 and one wants to project what the saturated thickness will be in this well for every year to the year 2020.

Factors: 1. The beginning saturated thickness is 110 feet in 1974.

- 2. The average decline rate is 2.07 feet per year for wells with saturated sections of 100 to 120 feet.
- 3. The average decline rate is 1.80 feet per year for wells with saturated sections of 80 to 100 feet.
- 4. The average decline rate is 1.60 feet per year for wells with saturated sections of 60 to 80 feet.
- 5. The average decline rate is 1.47 feet per year for wells with

saturated sections of 40 to 60 feet.

- 6. The average decline rate is 0.85 foot per year for wells with saturated sections of 20 to 40 feet.
- 7. The average decline rate is 0.40 foot per year for wells with saturated sections of 10 to 20 feet,
- 8. The time interval is 1974 through 2020.

The projected saturated thicknesses in the subject well are calculated and shown in the following table:

	SATURATED THICKNESS,		SATURATED THICKNESS
	BEGINNING OF YEAR	DECLINE RATE	END OF YEAR
YEAR	(feet)	(feet)	(feet)
1974	110.00	2.07	107.93
1975	107.93	2.07	105,86
1976	105.86	2.07	103.79
1977	103,79	2.07	101.72
1978	101.72	2.07	99.65
1979	99.65	1,80	97.85
1980	97,85	1.80	96.05
1981	96.05	1.80	94.25
1982	94.25	1,80	92.45
1983	92.45	1.80	90.65
1984	90.65	1.80	88.85
1985	88,85	1.80	87.05
1986	87,05	1,80	85.25
1987	85.25	1.80	83.45
1988	83.45	1.80	81.65
1989	81.65	1.80	79.85
1990	79,85	1.60	78.25
1991	78.25	1.60	76.65
1992	76.65	1.60	75,05
1993	75.05	1,60	73,45
1994	73.45	1.60	71.85
1995	71.85	1.60	70,25
1996	70.25	1.60	68.65
1997	68,65	1.60	67,05
1998	67.05	1.60	65,45
1999	65,45	1.60	63,85
2000	63.85	1,60	62.25
2001	62.25	1,60	60,65
2002	60.65	1,60	59.05
2003	59,05	1.47	57.58
2004	57,58	1.47	56.11
2005	56,11	1.47	54,64
2005	/ 54.64	1.47	53.17
2008	53.17	1.47	51,70
2007	51.70	1.47	50,23
	50.23	1.47	48.76
2009			46.76
2010	48.76	1.47	47.29 45.82
2011	47.29	1.47	45.82
2012	45.82	1.47	
2013	44.35	1,47	42.88
2014	42.88	1.47	41.41
2015	41.41	1.47	39.94
2016	39.94	.86	39,09

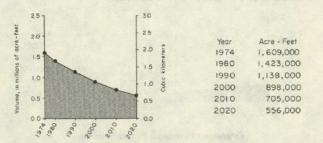
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YEAR	SATURATED THICKNESS, BEGINNING OF YEAR (feet)	AVERAGE DECLINE RATE (feet)	SATURATED THICKNESS, END OF YEAR (feet)
2017	39.09	.85	38.24
2018	38.24	.85	37.39
2019	37.39	.85	36.54
2020	36.54	.85	35.69

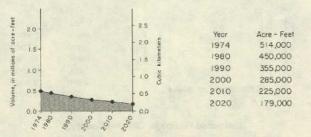
Similar computations were made for each of the selected data-control wells in Potter and Oldham Counties, and the saturated-thickness values for 1974, 1980, 1990, 2000, 2010, and 2020 were extracted from this data set for use in further calculations and mapping.

Mapping Saturated Thickness, and Calculating Volume of Water in Storage

To obtain estimates of the volume of water in storage in the Ogallala aquifer, an electronic digital computer was used to construct maps which reflect the saturated thickness of the aquifer for those years included in the study. These maps were then refined by the computer to reflect the number of acres corresponding to each range of saturated thickness. The number of acres for each range was multiplied by the saturated thickness in feet for that range and then by the coefficient of storage (0.15 or 15 percent), to yield an estimate of the volume of water in storage in each saturated-thickness range. Totaling these volumes produced an estimate of the volume of water in storage in each county. The current (1974) and projected volume estimates are shown in the following graphs:



Estimated Volume of Water in Storage, Potter County



Estimated Volume of Water in Storage, Oldham County

Preparing a data base and writing the necessary programs for the computer to use in constructing the saturated-thickness maps and in making the necessary calculations is time consuming; however, once the data base is prepared and programs written, the computer can perform in a few hours calculations that would have required many years of manual effort.

A generalized description of the methodology used in mapping and in computing water volume follows: A base map with a scale of 1 inch equals 2 miles (1:125,000) was selected to prepare data for computer processing. All data points (observation wells) were plotted on these base maps by hand and assigned identifying numbers. A machine called a digitizer was then used to translate these mapped location data (well locations, county boundaries, etc.) into information processible by the computer. To accomplish this, a latitude and longitude coordinate was recorded on each base map as a central reference point, and all data points and county boundaries were then digitized; that is, measurements were made by the digitizer to reference these data points and boundaries to the initial latitude and longitude coordinate. Then the digitized information was processed by the computer and the maps were re-created by a computer-driven plotter. The computer-plotted image maps were ultimately checked against the hand-constructed maps to verify that the data were plotted accurately.

The assignment of a unique number to each data point (observation well) on the base maps made it possible to machine process the data related to these points and to plot these data back on the maps at the proper location.

To compute the volume of water in storage, the computer was instructed to subdivide the counties into squares measuring approximately 0.5 mile (0.8 km). The known saturated-thickness values obtained from the data points were filled into the squares in which the data points were located. Based on these known values, the computer filled in a weighted-average value for each remaining square, taking into consideration all known values within a radius of 7 miles (11 km). After this step was completed, the computer then counted the numbers of squares having equal values, thus obtaining the approximate area in square miles (later converted to acres) corresponding to each range of saturated thickness. As previously stated, the number of acres in each 25-foot (7.6-meter) range of saturated thickness was multiplied by the corresponding saturated-thickness value and the storage coefficient (0.15 or 15 percent) to obtain the approximate volume of water in acre-feet in that saturated-thickness range.

Although the calculations were made by the computer from information stored in its image field, the data in the image field were printed out in the form of contoured saturated-thickness maps, which are reproduced in this report. Facing each saturated-thickness map in the report are corresponding tabulations of the approximate volume of water in storage in each county.

Calculating Pumpage

Estimates of current pumpage were obtained in this study by calculating the storage capacity of the dewatered section of the Ogallala aquifer as reflected in changes in the annual depth-to-water measurements made in the water level observation wells. Factors for natural recharge and irrigation recirculation were then added to these volumetric figures to obtain more realistic pumpage estimates.

The step-by-step procedure involved in making pumpage estimates is similar to the procedures used in calculating the estimates of volume of water in storage; therefore, a more general explanation follows.

Change in water level (decline) maps for the aquifer were made by the computer for the years considered. From these maps, the volume of desaturated material was multiplied by the number of acres corresponding to each 0.25-foot (.076-meter) range of decline and then multiplied by the storage coefficient of the aquifer (0.15 or 15 percent), which resulted in an estimate of the volume of water taken from storage for each decline range. Estimates for natural recharge and irrigation recirculation were added to these values to obtain estimates of pumpage.

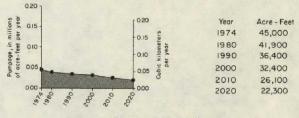
An attempt was made to obtain a reliable estimate of the natural recharge and recirculation for use in this study. This involved obtaining an estimate of the amount of water required by each of the major crops grown in the area. These values, generally referred to as "duty of water," were obtained from Texas Agricultural Experiment Stations located in the High Plains area. The duty of water figure for each major crop was multiplied by the number of crop acres, and the resulting numbers were added together to yield an estimate of the total crop water demand.

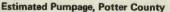
The amount of precipitation which fell just prior to and during the growing season was subtracted from the total water demand estimate. The difference between these values should equal that amount which would have been supplied by irrigation, which will be referred to as irrigation makeup water.

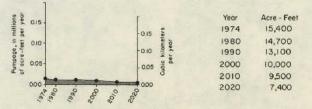
The volume figure represented by the dewatered section was then compared to the volume of water which should have been supplied to crops by irrigation makeup water. In all tests, the volume of water represented by the depletion of the aquifer was considerably less than the makeup water estimate. This difference was attributed to irrigation recirculation and natural recharge.

Various combinations of estimates for natural recharge and recirculation were added to the volume represented by aquifer depletion, in an attempt to obtain comparable values with the makeup water estimated for the test years. One-half inch (1.3 cm) per year of natural recharge added to the volume represented by the depletion of the aquifer, and then adding 10 percent of this for recirculation, most nearly equaled the makeup water estimated in the largest number of instances in Potter and Oldham Counties and in adjoining counties with similar conditions.

These amounts were added to the previously calculated storage capacity of the dewatered section to obtain estimates for current (1974) and future pumpage. The following graphs show the current and projected estimates of pumpage for each county:







Estimated Pumpage, Oldham County

Calculating Pumping Lifts

The pumping lift (pumping level) is the depth from land surface to the water level in a pumping well; it is equal to the depth of the static water level plus the drawdown due to pumping. The amount of pumping lift largely determines the amount of energy required to produce the water, and thus strongly affects the pumping costs.

In calculating pumping lifts, procedures were used that are similar to those used in making estimates of the volume of water in storage and the estimates of pumpage. Again, the computer and original data base were used as previously described.

In making estimates of pumping lifts, it was assumed (1) that the yield of each pumping well is 900 gallons per minute (56.8 l/s) except as limited by the capacity of the aquifer (this conforms with the historical trend of equipping new wells with 8-inch [20-centimeter] or smaller pumps), (2) that the specific well yield is 15 gallons per minute per foot of drawdown (3.1 [l/s] /m), and (3) that once the well yield equals the capacity of the aquifer, the well will continue to be produced at a rate near the capacity of the aquifer until pumping lifts are within 10 feet (3 m) of the base of the aquifer. After that time, it is assumed that the pumping lift will remain constant because of greatly diminished well yields. It should be noted that this 10-foot (3-meter) minimum is somewhat arbitrarily chosen, as one cannot predict accurately the minimum saturated thickness that will be feasible for producing irrigation water under future economic conditions.

The above assumptions restrict the drawdown in wells to a maximum of 60 feet (18.3 m); that is, the maximum well yield of 900 gallons per minute (56.8 l/s) divided by specific well yield of 15 gallons per minute per foot (3.1 [I/s]/m) equals 60 feet (18.3 m) of maximum drawdown.

Based on the above assumptions, pumping lifts were calculated separately for each of the selected data-control wells in the counties. The factors involved were the historical and projected saturated-thickness values, the historical and projected static water levels, and the drawdown value assigned to the Potter and Oldham County area.

In all areas where the aquifer's saturated thickness was 70 feet (21.3 m) or greater (areas where a well, pumped at full capacity, would be drawn down 60 feet [18.3 m] to yield 900 gallons per minute [56.8 l/s]), the computer was instructed to add 60 feet (18.3 m)—the drawdown—to the static water level to determine pumping lift. For a well with a saturated thickness of less than 70 feet (21.3 m), the pumping lift was calculated by subtracting 10 feet (3 m) from the depth of the well (base of the aquifer). These calculations were made for each year of record to be reported (1974, 1980, 1990, 2000, 2010, and 2020) for each well. The pumping-lift values were stored in the computer and printed out in the form of contour maps. Additionally, the surface area corresponding to each interval between the mapped contours was calculated and printed out in tabular form.

Well-Yield Estimates

Estimates of the rate, in gallons per minute, at which the Ogallala aquifer should be capable of yielding water to wells in various areas of the two counties are presented on maps for each year of record reported (1974, 1980, 1990, 2000, 2010, and 2020). These well-yield estimates are based on capabilities of the aquifer to yield water to irrigation wells of prevailing construction as reflected by the very large number of aquifer tests which have been conducted in various saturated-thickness intervals in the Texas High Plains. The estimates are adjusted to reflect the expected decreases in well yields through time due to the reduced saturated thickness as depletion of the aquifer progresses.

The well-yield estimates are subject to deviations caused by localized geological conditions. The Ogallala is not a homogeneous formation; that is, the silt, clay, sand, and gravel which generally comprise the formation vary from place to place in thickness of layers, layering position, and grain-size sorting. The physical composition of the formation material can drastically affect the ability of the formation to yield water to wells. As an example, in areas where the saturated portion of the formation is comprised of thick beds of coarse and well-sorted grains of sand, the well yields probably will exceed the estimates shown on the maps. In other localized areas, the saturated portion of the formation may be comprised principally of thick beds of silt and clay which can be expected to restrict well yields to less than those shown on the maps.

The following can be used as a general guide in Potter and Oldham Counties in estimating well yields based on saturated thickness:

SATURATED THICKNESS (feet)	WELL YIELD (gallons per minute)					
Less than 20	Less than 100					
20 to 30	100 to 250					
30 to 40	250 to 500					
40 to 60	500 to 800					
60 to 80	800 to 1,000					
More than 80	More than 1,000					

The maps presented in this report are intended for use as general guidelines only and are not recommended for use in determining water availability when buying and selling specific tracts of land. Inasmuch as the availability of ground water constitutes a large portion of the price of land bought and sold in this area, it is recommended that a qualified ground-water hydrologist be consulted to make appraisals of ground-water conditions when such transactions are contemplated.

DISTINCTION BETWEEN PROJECTIONS AND PREDICTIONS

The actions of the Potter and Oldham County water users will determine whether the projections of this study come to pass, as the rate of depletion of the ground-water resource is determined by the rate of water use. The authors have not made predictions of what will occur, but have furnished projections based on past trends and presently available information.

There are many unpredictable factors which can influence the future rates of withdrawal of ground water from the Ogallala aquifer for irrigation farming. These factors include: (1) the amounts and distribution of precipitation which will be received in the area in the future; (2) federal crop acreage controls or the lack of these; (3) the price and demand for food and fiber grown in the area; (4) the cost and availability of energy to produce water from the aquifer; (5) farm labor cost and availability of farm labor; (6) results of continuing research that seeks to develop more frugal water-application methods for irrigation, crops having less water demand, and methods for inducing clouds to yield more water as rain; and (7) most important, the degree to which feasible soil and water conservation measures are employed by the High Plains irrigator, Any of these factors could appreciably influence the rate of use of ground water in the future; however, the projections in this study provide a reasonable set of general expectations on the further depletion of the aquifer.

SATURATED THICKNESS AND VOLUME OF

WATER IN THE OGALLALA AQUIFER

1974

Volume of Water in Storage Corresponding to Mapped Saturated-Thickness Intervals

(Coefficient of Storage: 15 percent)

MAPPED SATURATED THICKNESS INTERVAL (feet)	SURFACE AREA (acres)	VOLUME OF WATER IN STORAGE (acre-feet)
0- 25	83,486	33,397
25 50	40,423	247,288
50- 75	51,331	480,309
75-100	34,632	449,493
100125	12,278	203,992
125-150	4,588	93,144
150—175	1,886	46,293
175200	512	13,774
200-225	342	10,948
225-250	343	11,882
250-275	342	13,230
275-300	129	5,563
TOTAL.	230,292	1,609,313

OLDHAM COUNTY

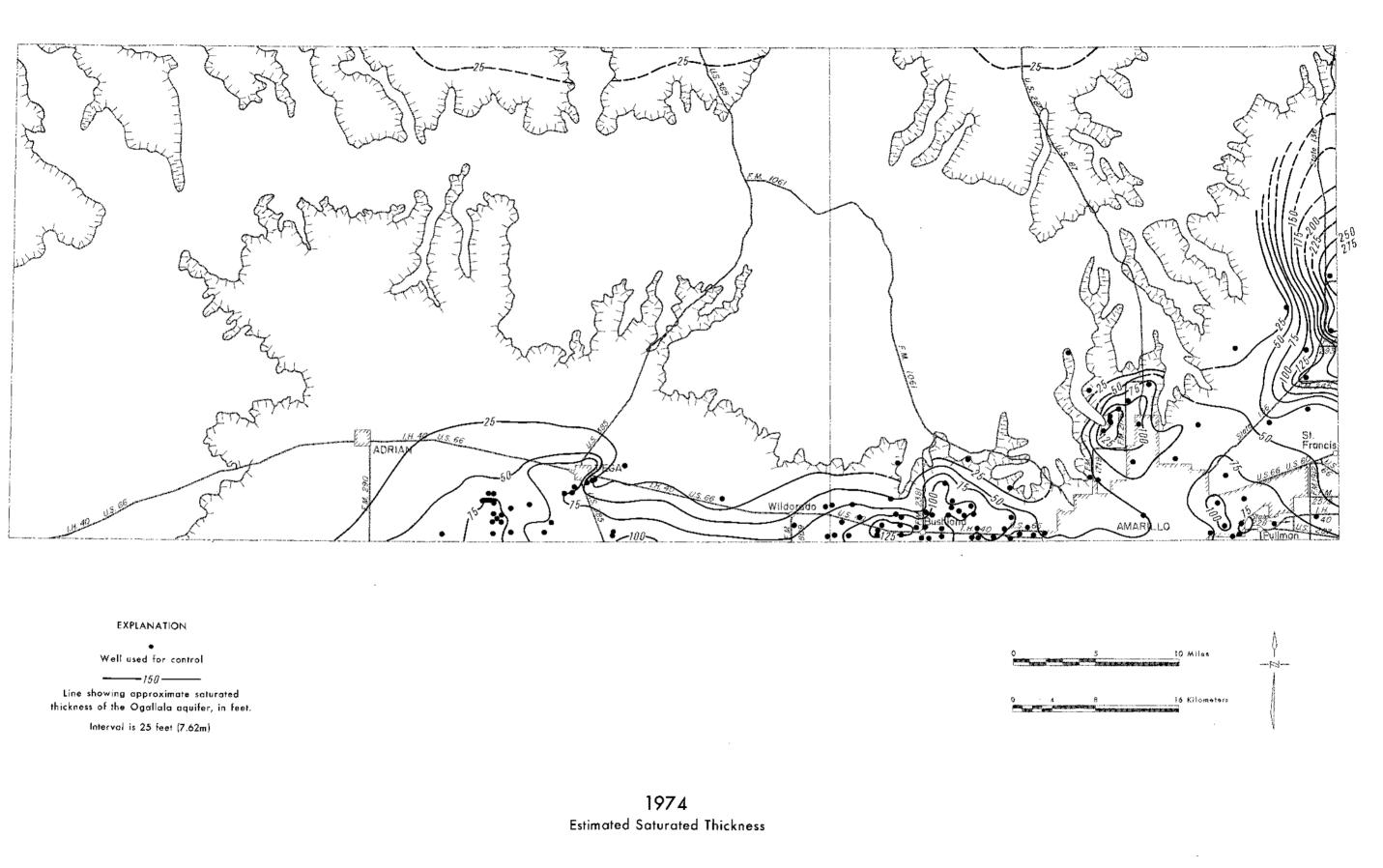
1974

Volume of Water in Storage Corresponding to Mapped Saturated-Thickness Intervals

(Coefficient of Storage: 15 percent)

MAPPED SATURATED- THICKNESS INTERVAL (feet)	SURFACE AREA (acres)	VOLUME OF WATER IN STORAGE (acre-feet)
0— 25	398,006	49,518
25- 50	23,997	132,879
60— 75	14,708	141,675
75—1 00	13,094	164,751
100125	1,395	24,695
TOTAL	451,200	513,518

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1980 Volume of Water in Storage Corresponding to Mapped Saturated-Thickness Intervals

SUR ____

1980

Volume of Water in Storage Corresponding to Mapped Saturated-Thickness Intervals

(Coefficient of Storage: 15 percent)

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MAPPED SATURATED-THICKNESS INTERVAL (feet) 0- 25 25- 50 50- 75 75-100

MAPPED SATURATED-THICKNESS INTERVAL

(feet)

TOTAL

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TOTAL

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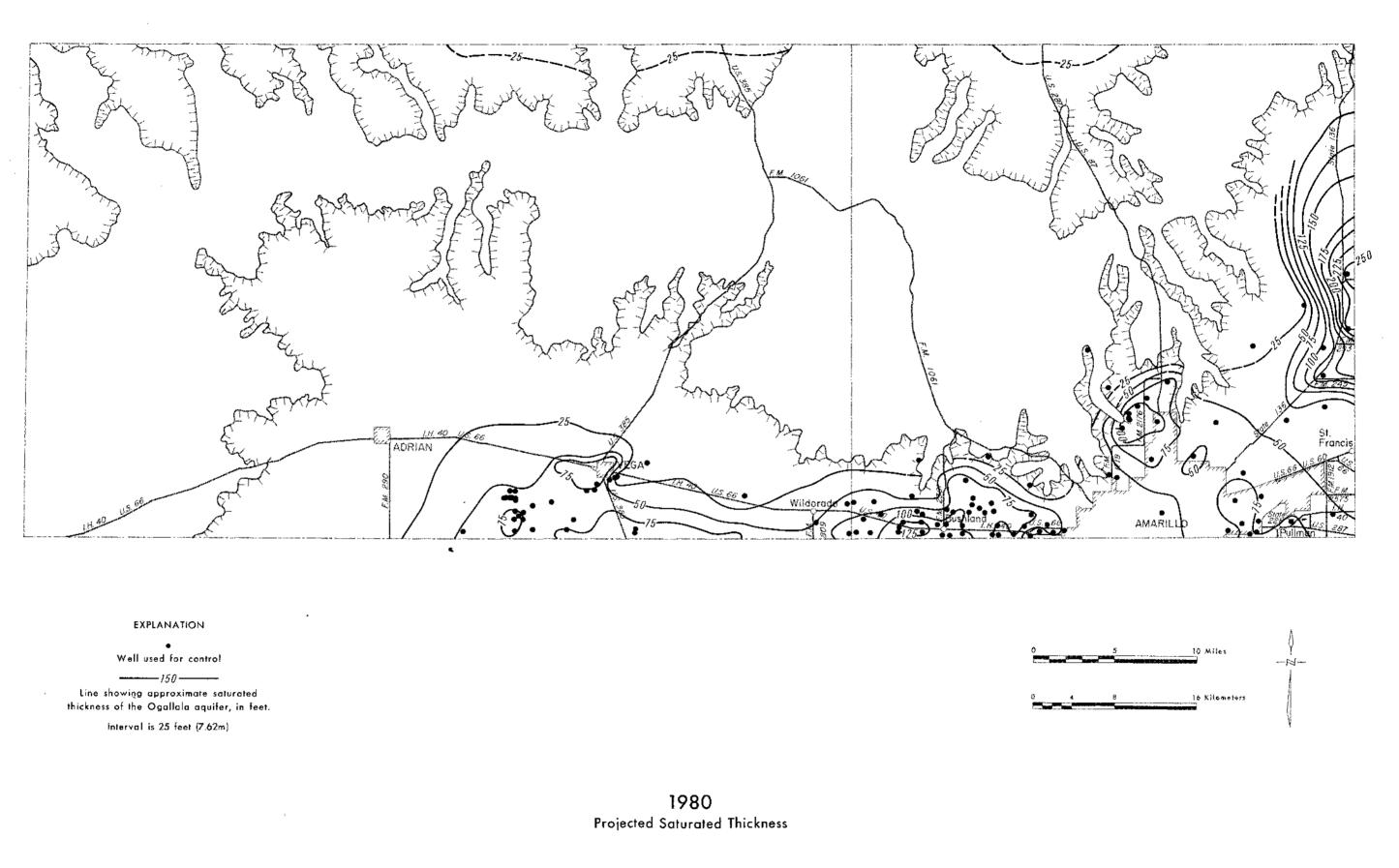
(Coefficient of Storage: 15 percent)

RFACE AREA	VOLUME OF WATER IN STORAGE
(acres)	(acre-feet)
86,097	44,413
53,637	314,312
51,597	477,177
25,397	324,276
8,645	142,853
2,401	49,122
1,369	32,703
171	4,747
514	16,222
342	12,162
122	4,804
230,292	1,422,791

OLDHAM COUNTY

*

FACE AREA (acres)	VOLUME OF WATER IN STORAGE (acre-feet)
400,790	54,518
24,841	131,639
19,645	186,623
5,924	76,763
451,200	449,543



1990

SURFACE AREA	VOLUME OF WATER IN STORAGE (acre-feet)
94,839	72,921
76,211	420,291
41,695	380,519
12,406	160,864
2,745	46,335
1,369	27,792
171	4,117
856	24,839
230,292	1,137,678

MAPPED SATURATED-THICKNESS INTERVAL (feet) 0-- 25 25-- 50 50- 75 75-100 100-125 125-150 150-175 175-200 TOTAL

OLDHAM COUNTY

Volume of Water in Storage Corresponding to Mapped Saturated-Thickness Intervals

410,538 25,894 14,768 451,200

MAPPED SATURATED-THICKNESS INTERVAL (feet) \$ 0—25 25—50 50—75

TOTAL

Volume of Water in Storage Corresponding to Mapped Saturated-Thickness Intervals

(Coefficient of Storage: 15 percent)

1990

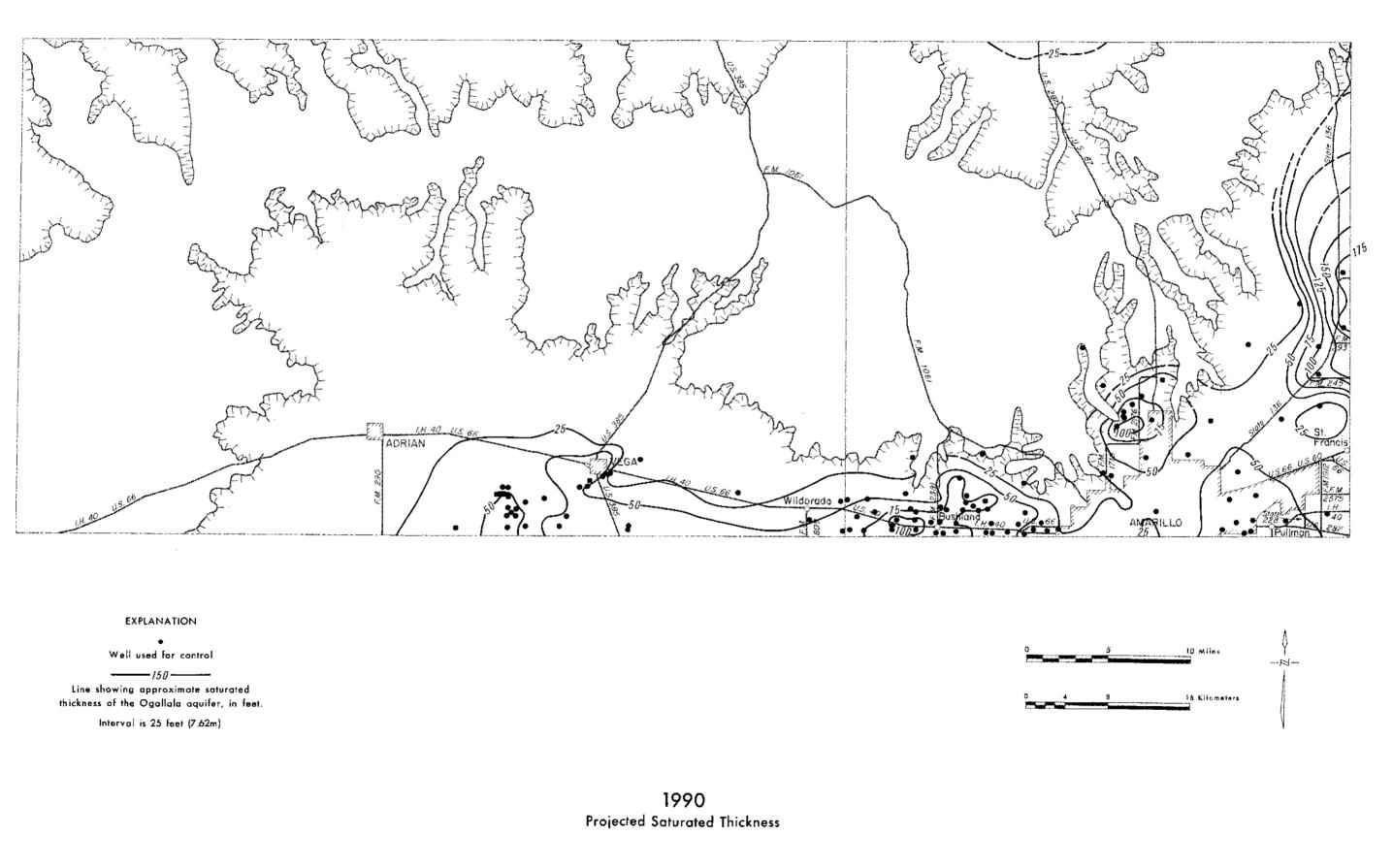
(Coefficient of Storage: 15 percent)

SURFACE AREA (acres)

VOLUME OF WATER IN STORAGE (acre-feet)

.

81,288
139,758
134,441
355,487



2000

Volume of Water in Storage Corresponding to Mapped Saturated-Thickness Intervals

(Coefficient of Storage: 15 percent)

MAPPED SATURATED- THICKNESS INTERVAL (feet)	
0 - 2 5	
25- 50	
5 0 - 75	
75-100	
100-125	
125-150	
150-175	
TOTAL	

OLDHAM COUNTY

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Volume of Water in Storage Corresponding to Mapped Saturated-Thickness Intervals

(Coefficient of Storage: 15 percent)

SURF

THICKNESS INTERVAL (feet)

MAPPED SATURATED-

0—25 25—50 50—75 TOTAL

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SURFACE AREA	VOLUME OF WATER IN STORAGE (acre-feet)
121,802	154,162
76,900	412,118
23,233	207,016
5,618	71,368
1,712	28,689
171	3,497
856	21,309
230,292	898,159

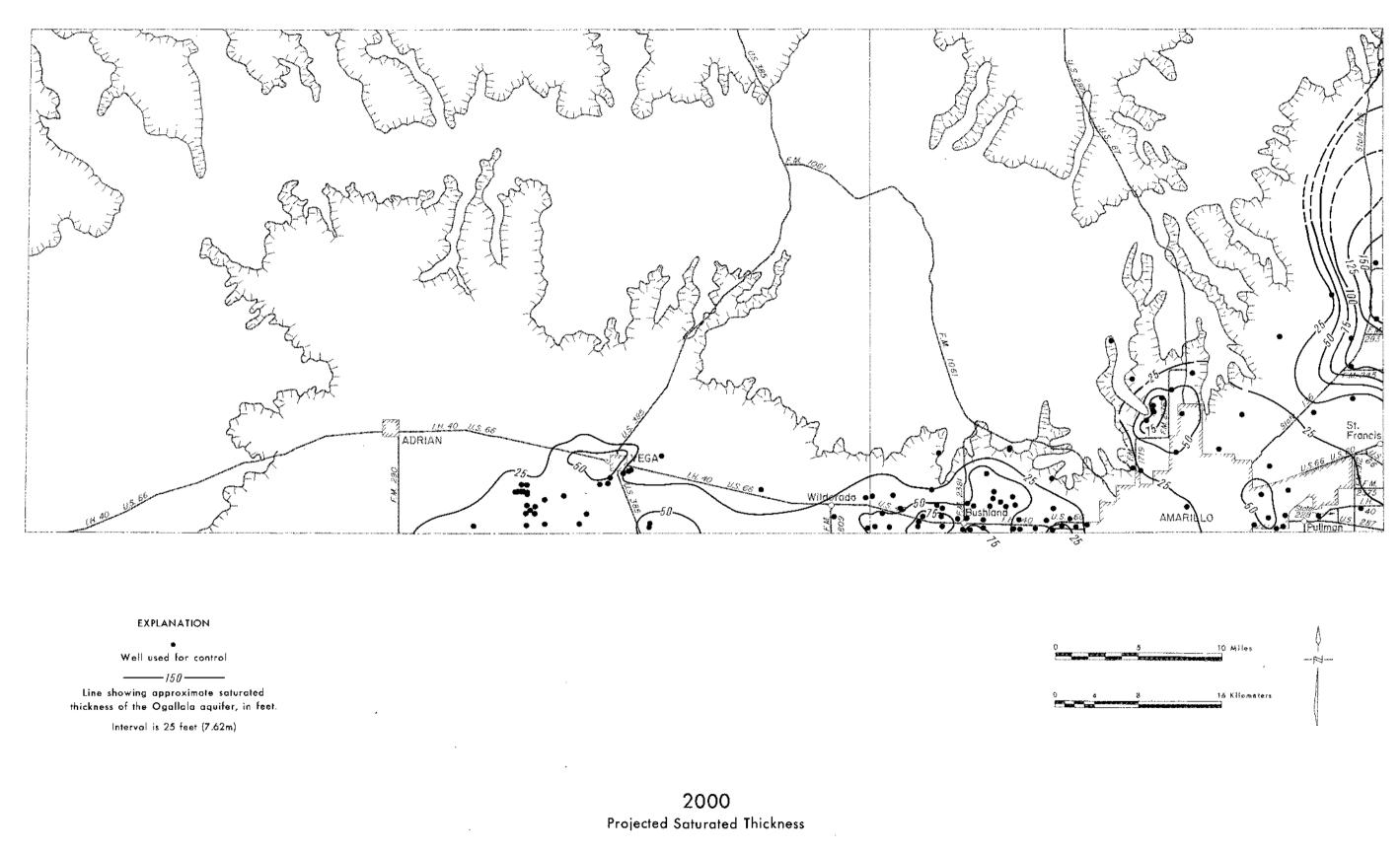
2000

FACE AREA	
(acres)	

420,048 27,649 3,503 451,200

VOLUME OF WATER IN STORAGE (acre-feet)

102,688
150,794 31,721
285,203



Volume of Water in Storage Corresponding to Mapped Saturated-Thickness Intervals

SUR

(Coefficient of Storage: 15 percent)

SURFACE AREA (acres)

. /

0--25 25--50 TOTAL

(feet)

MAPPED SATURATED-THICKNESS INTERVAL

MAPPED SATURATED-THICKNESS INTERVAL

(feet)

0- 25 25- 50 50- 75 75-100 100-125 125-150

TOTAL

2010

(Coefficient of Storage: 15 percent)

RFACE AREA	VOLUME OF WATER IN STORAGE
(acres)	(acre-feet)
152,696	227,997
63,295	324,268
10,361	93,175
2,570	33,164
514	8,336
856	18,339
230,292	705,279

OLDHAM COUNTY

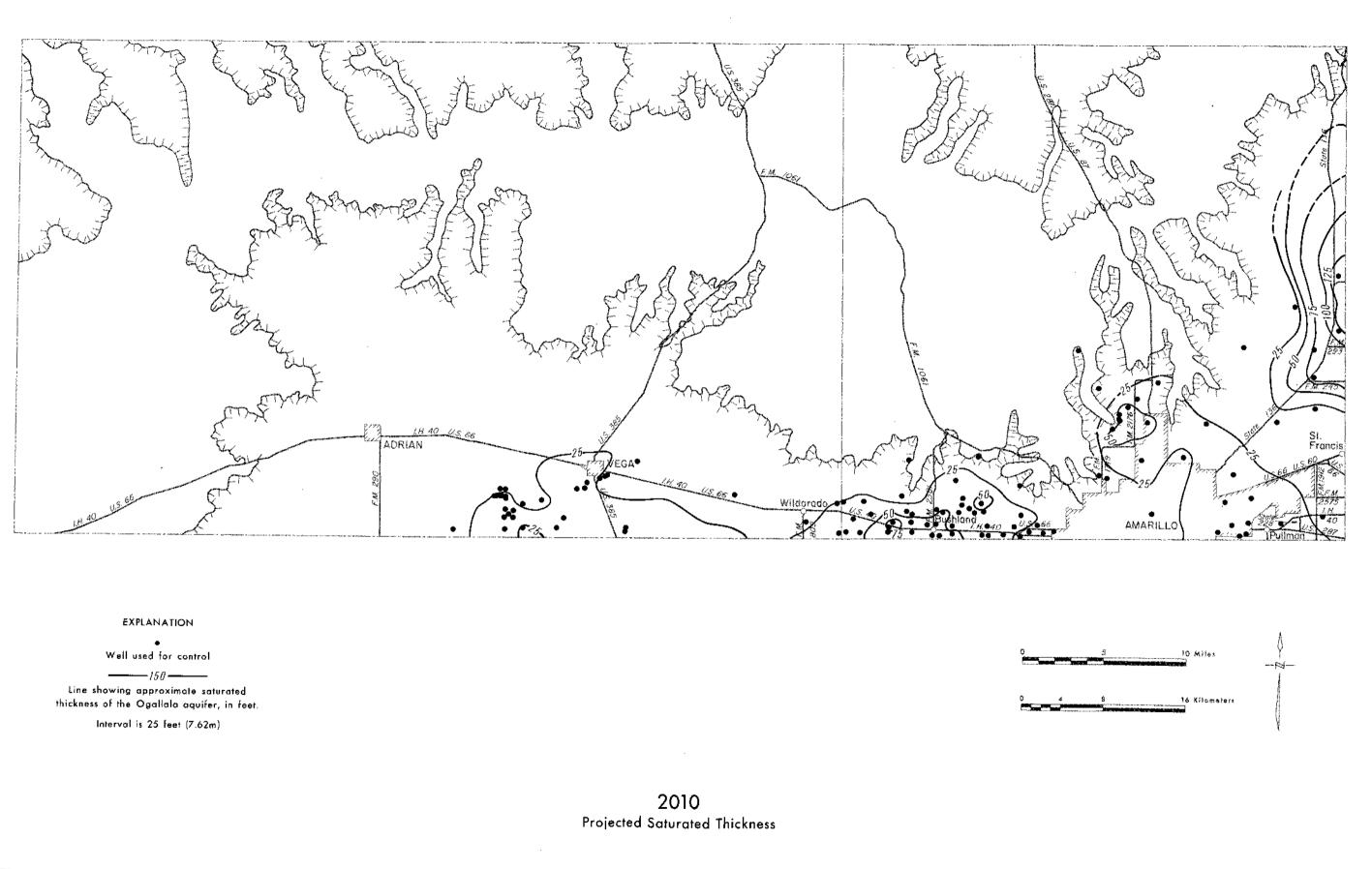
2010

Volume of Water in Storage Corresponding to Mapped Saturated-Thickness Intervals

> 429,498 21,702 451,200

VOLUME OF WATER IN STORAGE (acre-feet)

> 118,162 107,061 225,223



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2020

MAPPED SATURATED- THICKNESS INTERVAL (feet)	SURFACE AREA	VOLUME OF WATER IN STORAGE (acre-feet)
0- 25	184.370	290,313
25- 50	. 38,701	189,713
50- 75	5,338	47,679
75-100	1,027	12,974
100-125	856	15,413
TOTAL	230,292	556,092
TOTAL	230,292	556,092

OLDHAM COUNTY

SURFA	
44	

MAPPED SATURATED-THICKNESS INTERVAL (feet)

0–25 25–50

TOTAL

POTTER COUNTY

Volume of Water in Storage Corresponding to Mapped Saturated-Thickness Intervals

(Coefficient of Storage: 15 percent)

2020

Volume of Water in Storage Corresponding to Mapped Saturated-Thickness Intervals

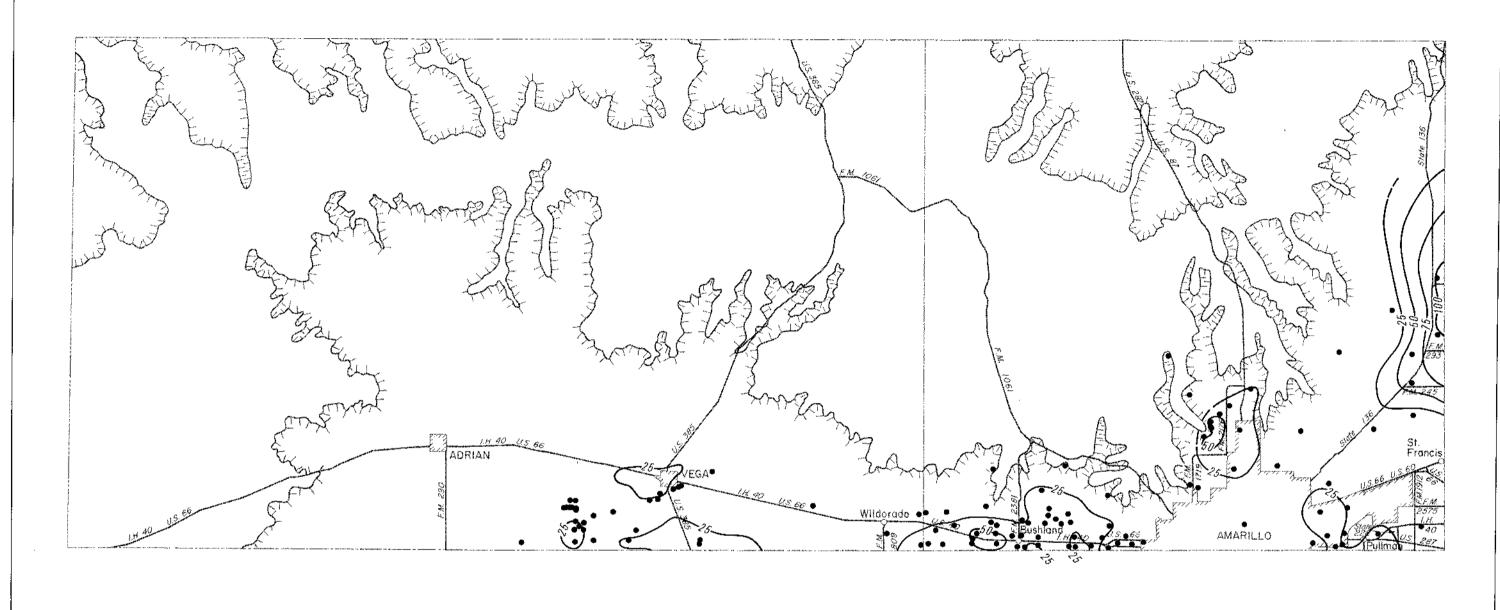
(Coefficient of Storage: 15 percent)

ACE AREA (acres)

43,600 7,600 451,200

VOLUME OF WATER IN STORAGE (acre-feet)

> 144,849 34,401 179,250



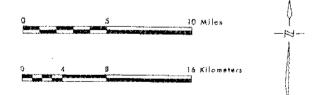
EXPLANATION

• Well used for control

Line showing approximate saturated thickness of the Ogallala aquifer, in feet.

Interval is 25 feet (7.62m)

2020 Projected Saturated Thickness

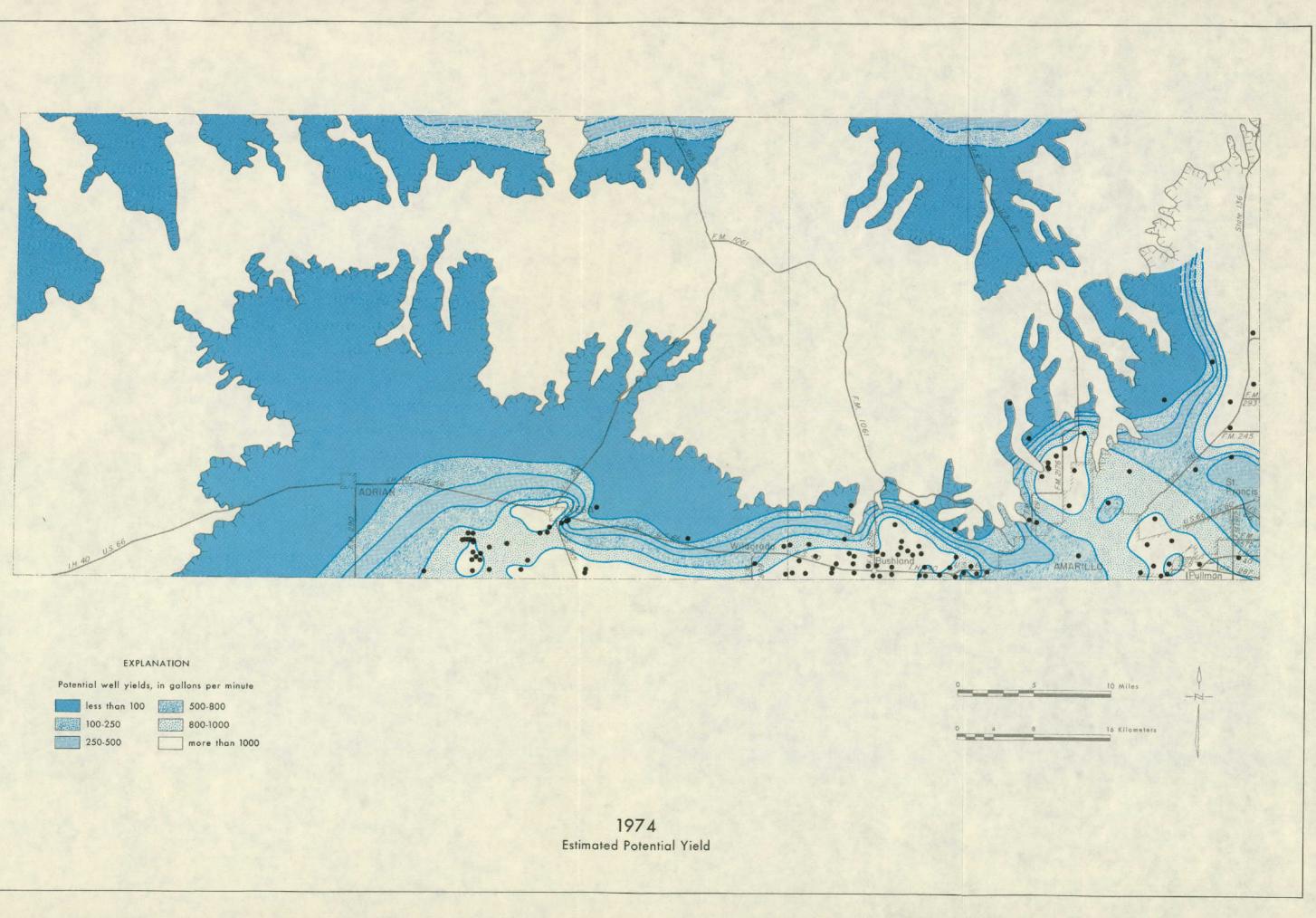


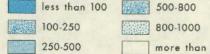
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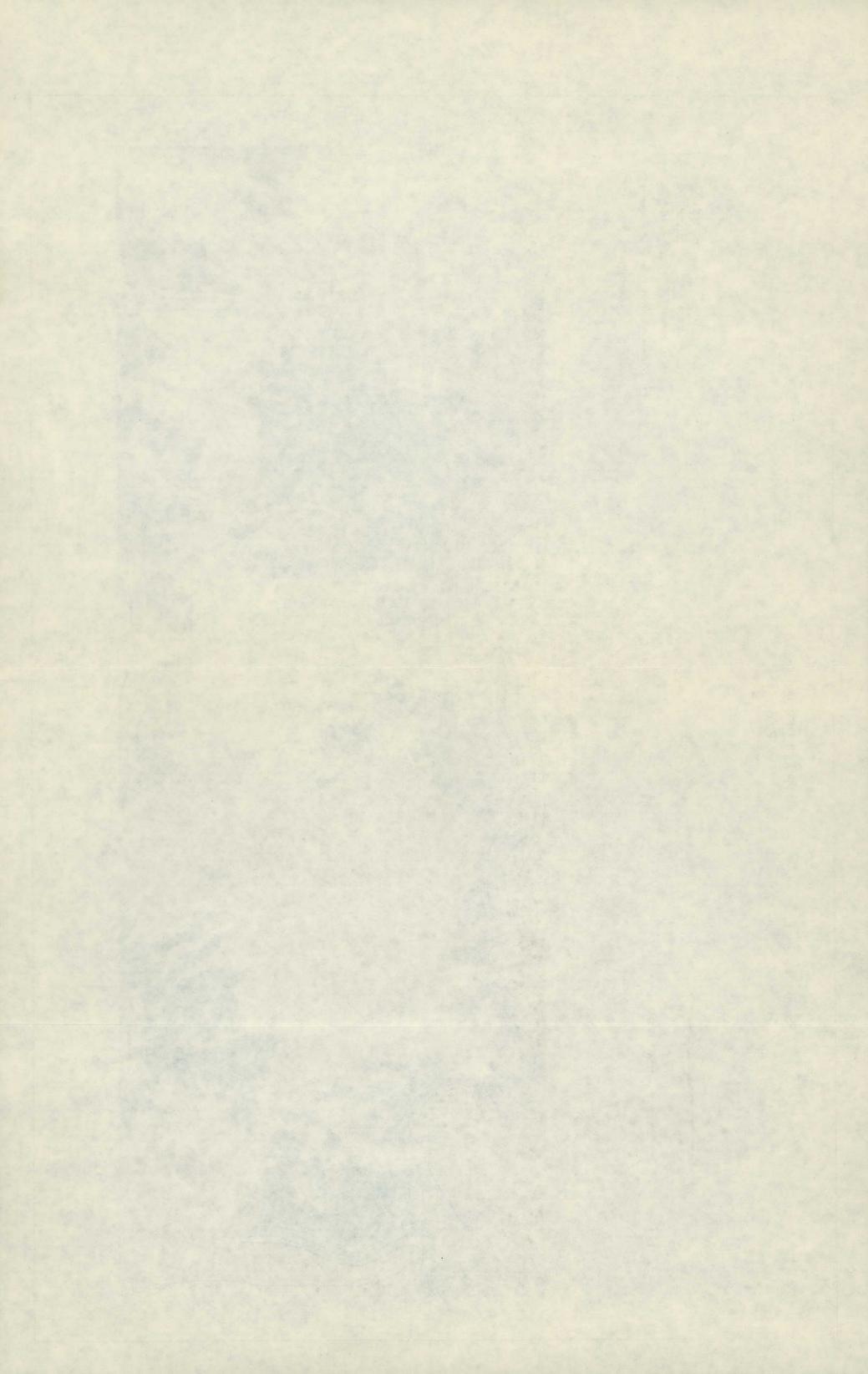
POTENTIAL WELL YIELD OF THE

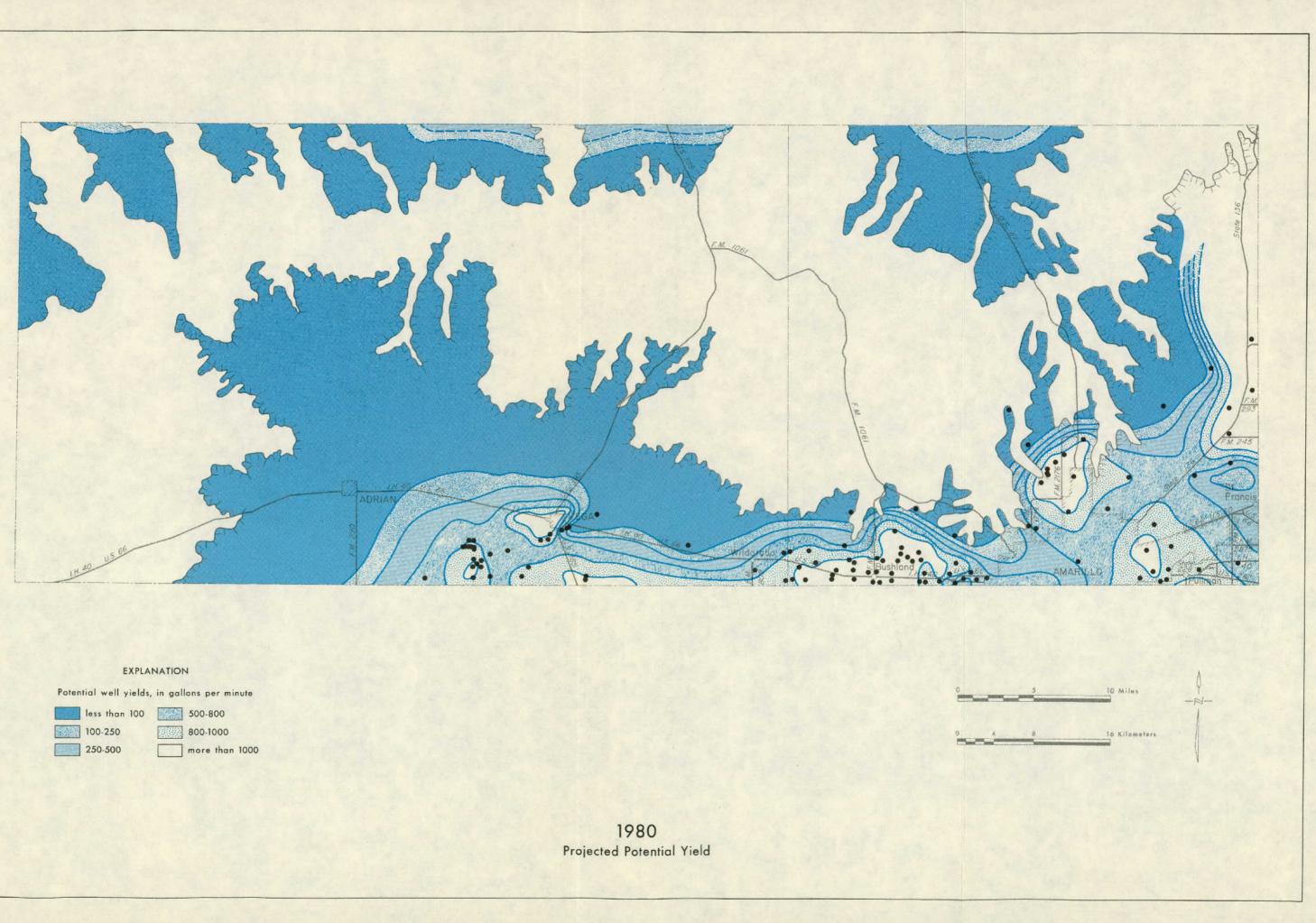
OGALLALA AQUIFER

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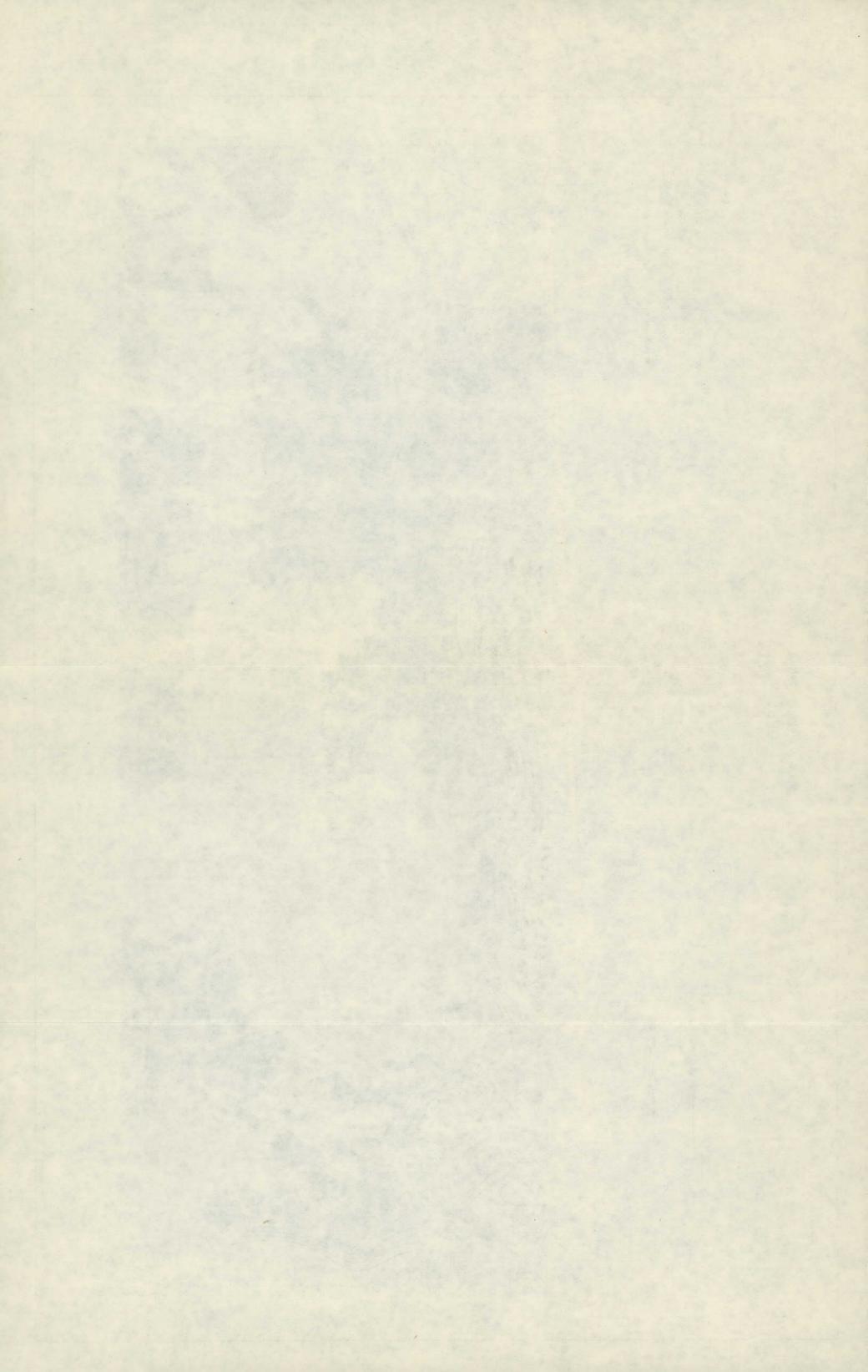


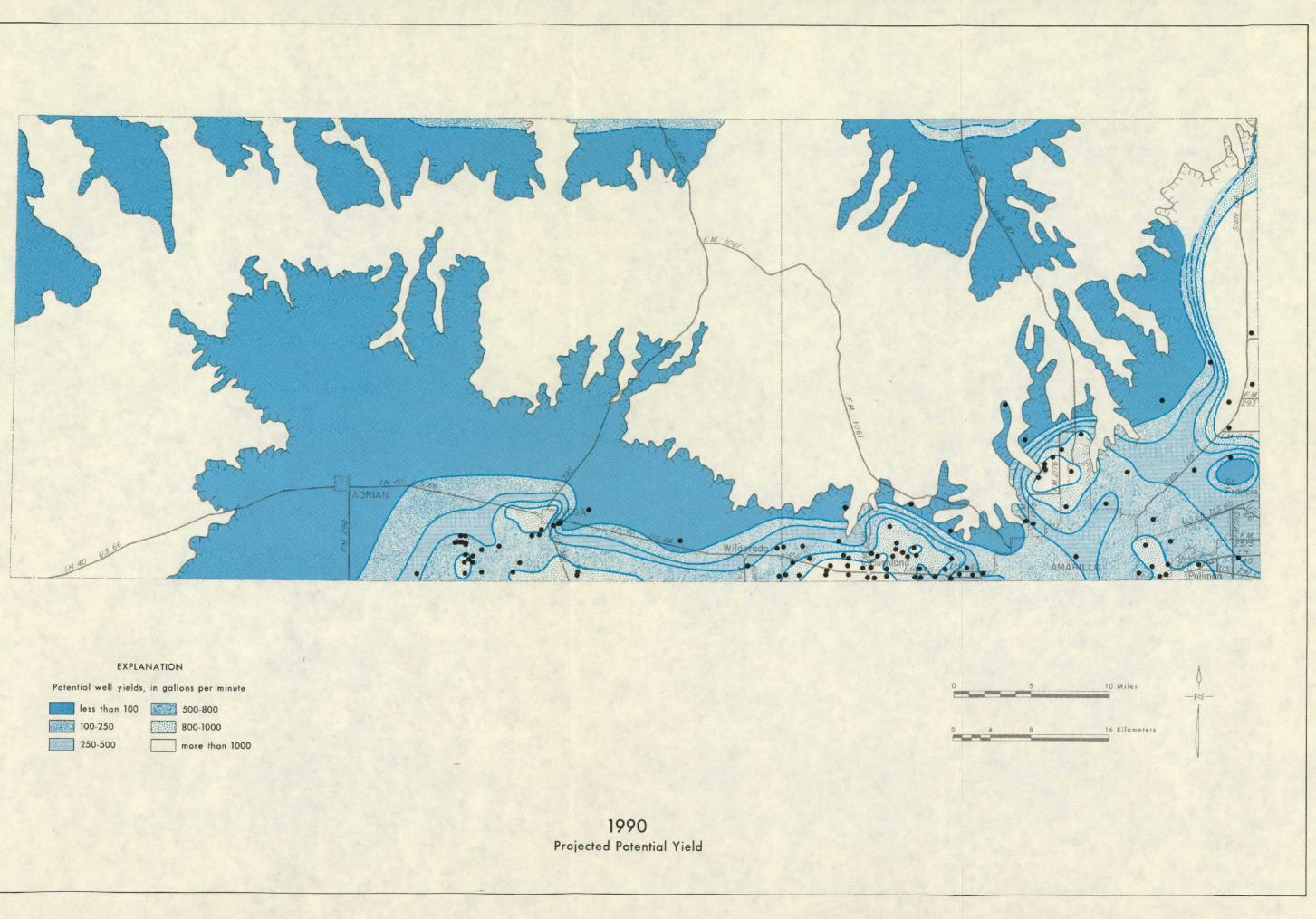




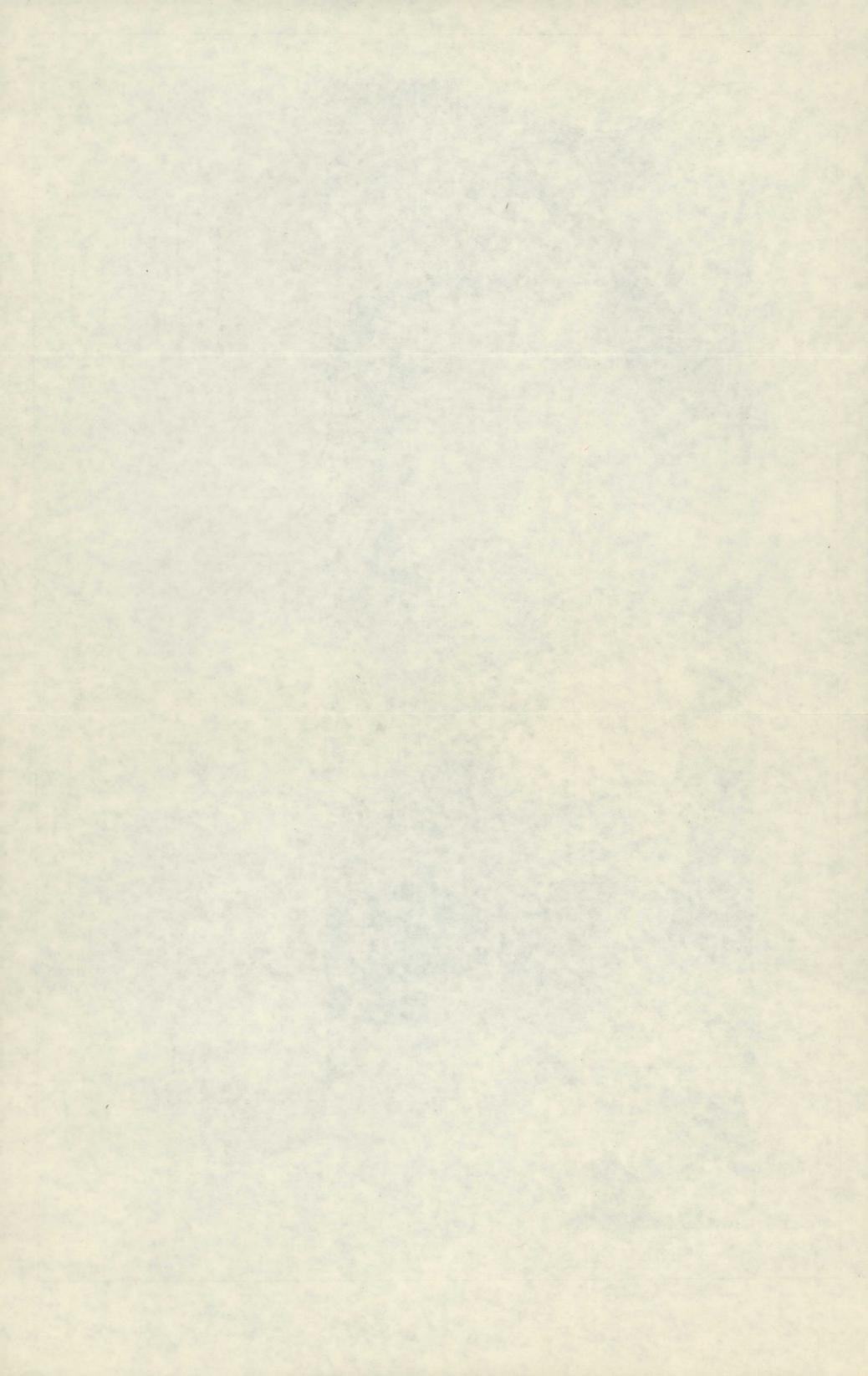


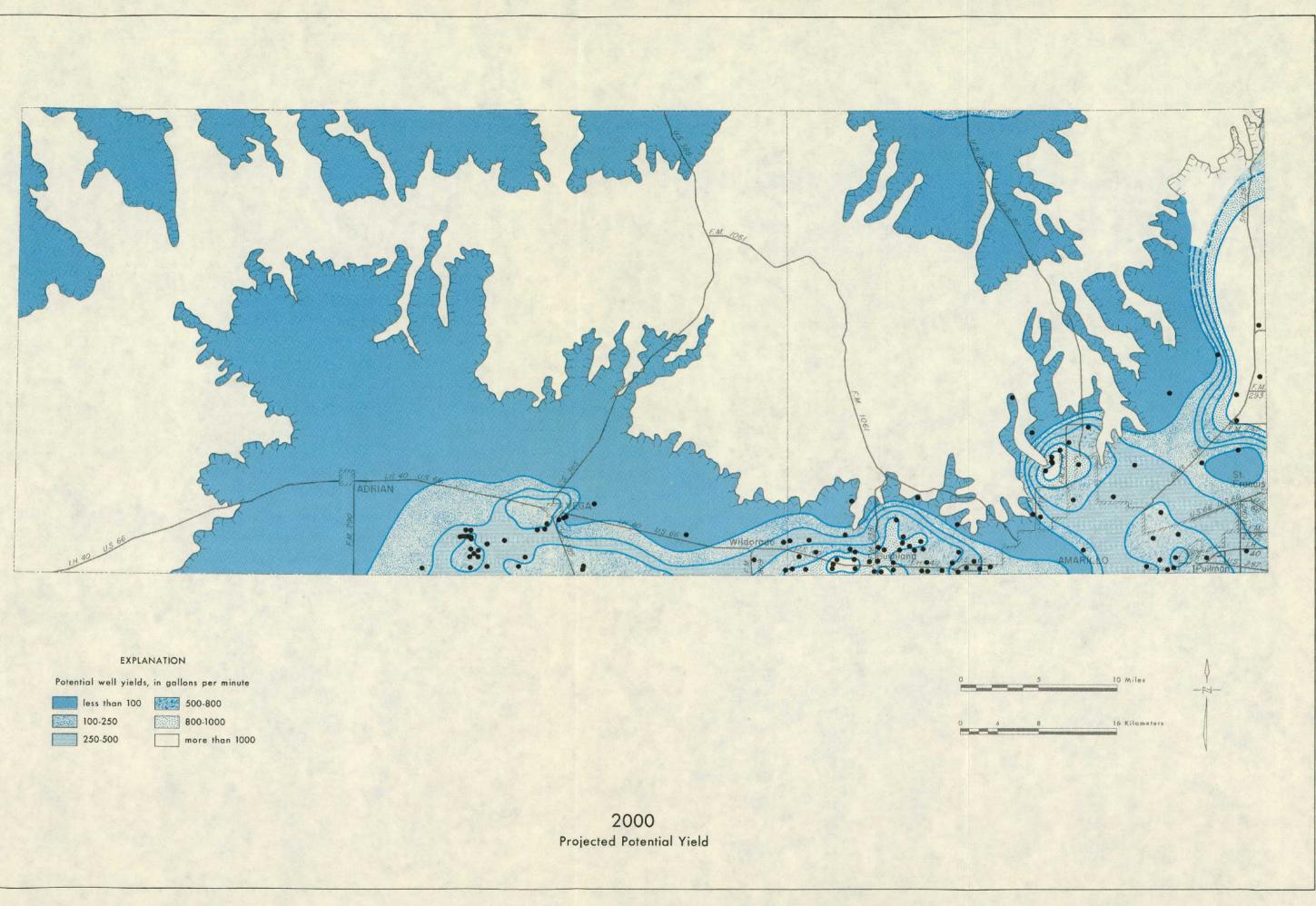
less than 100	500-800
100-250	800-1000
250-500	more than 10



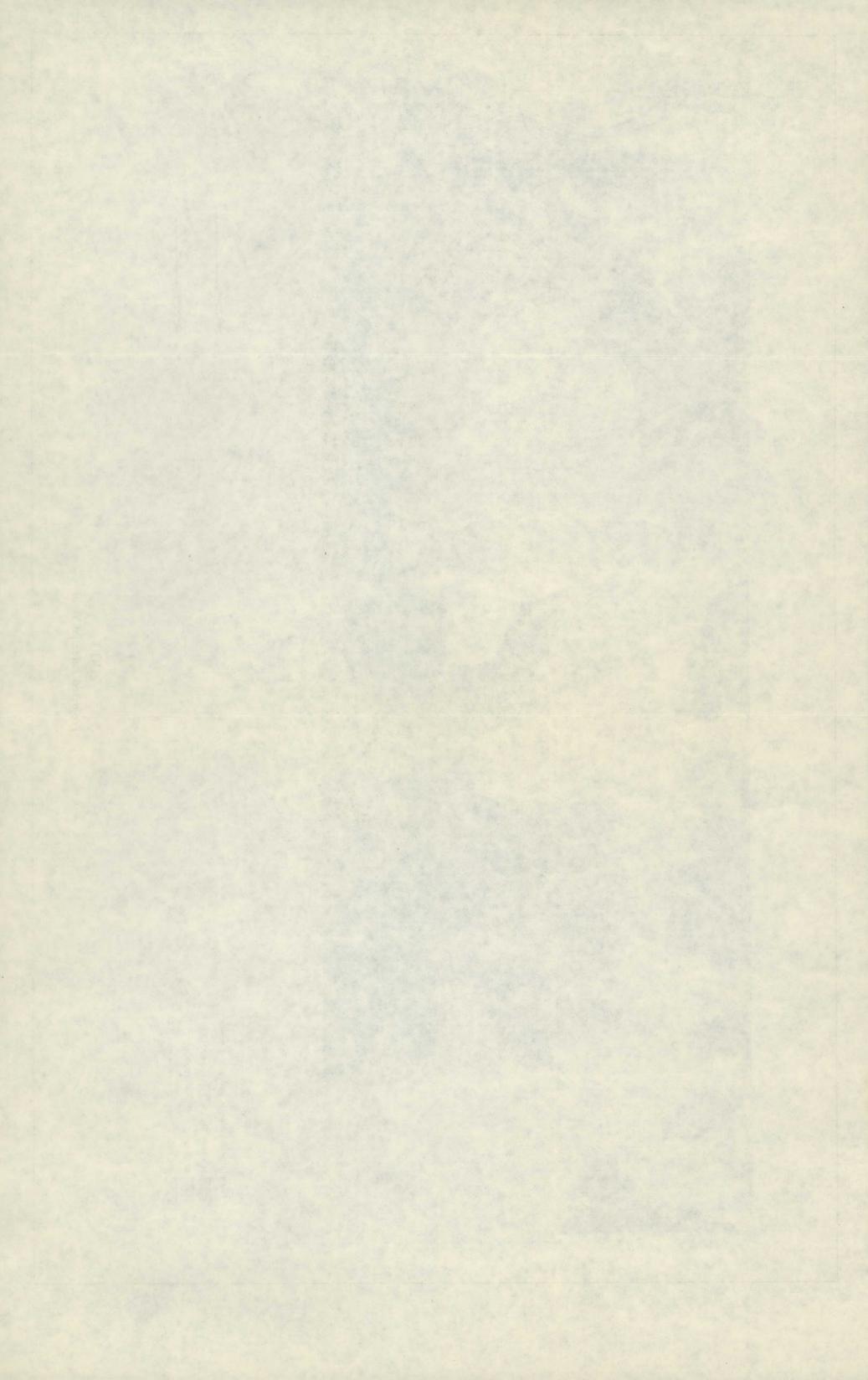


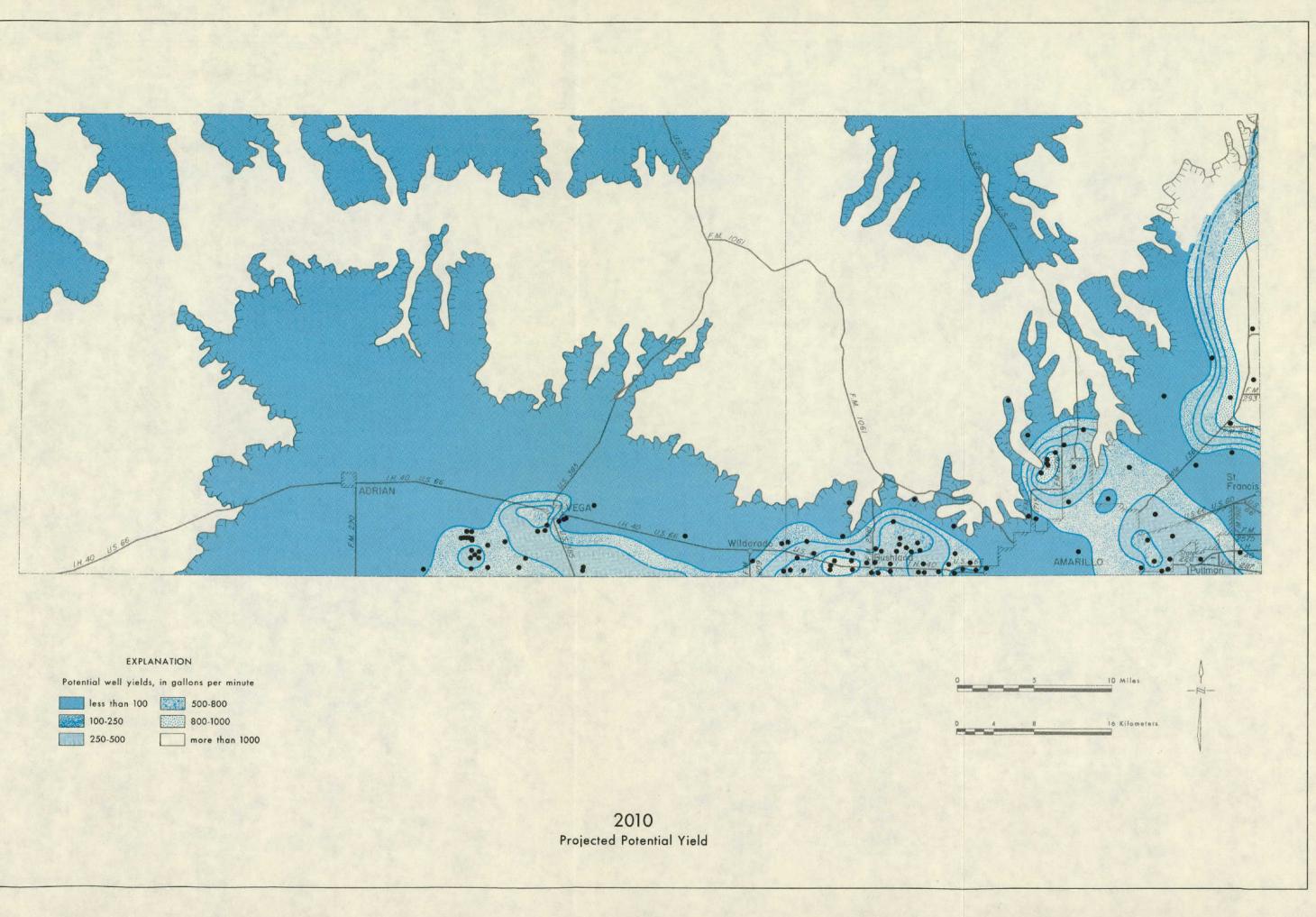


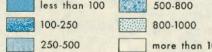


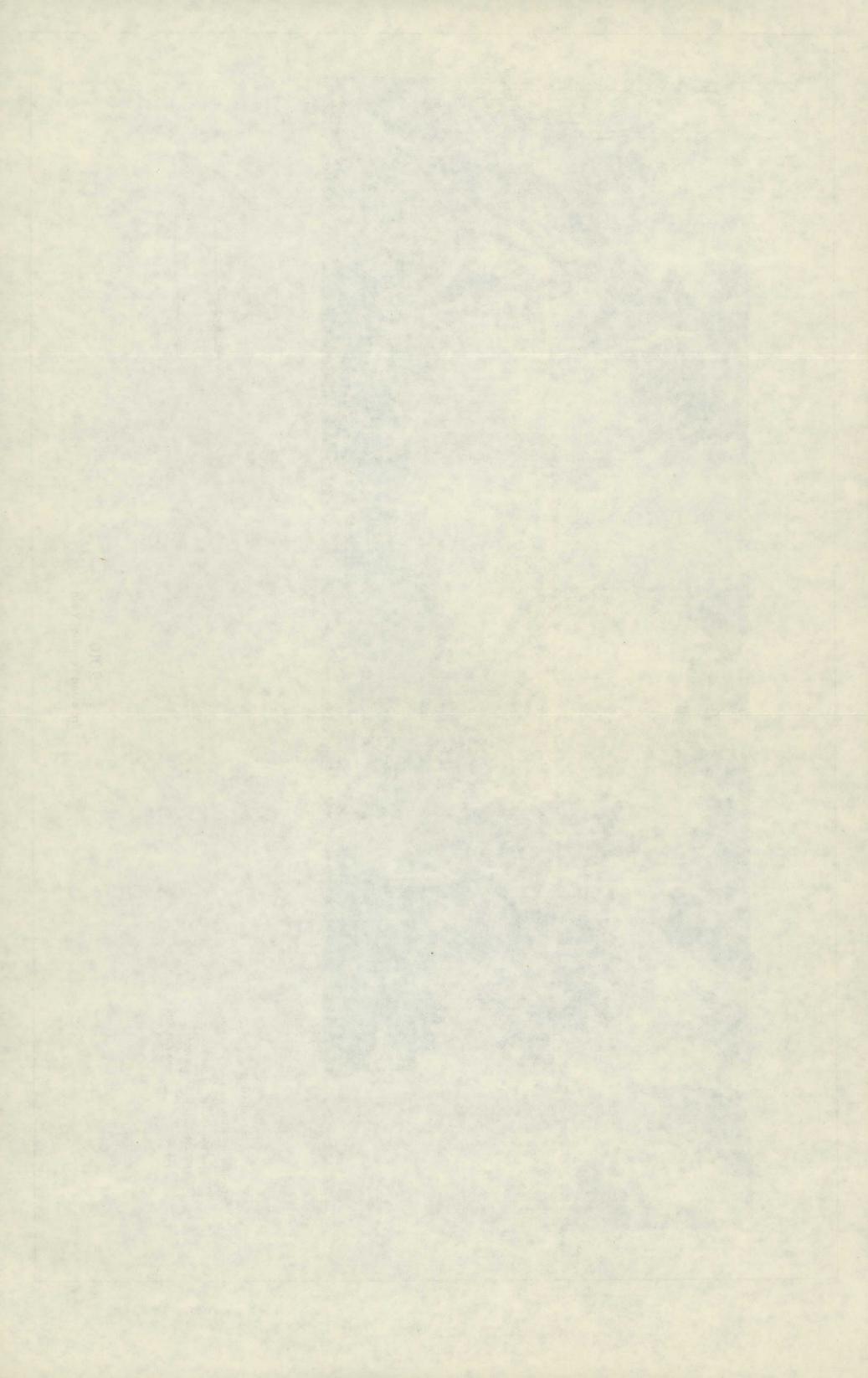


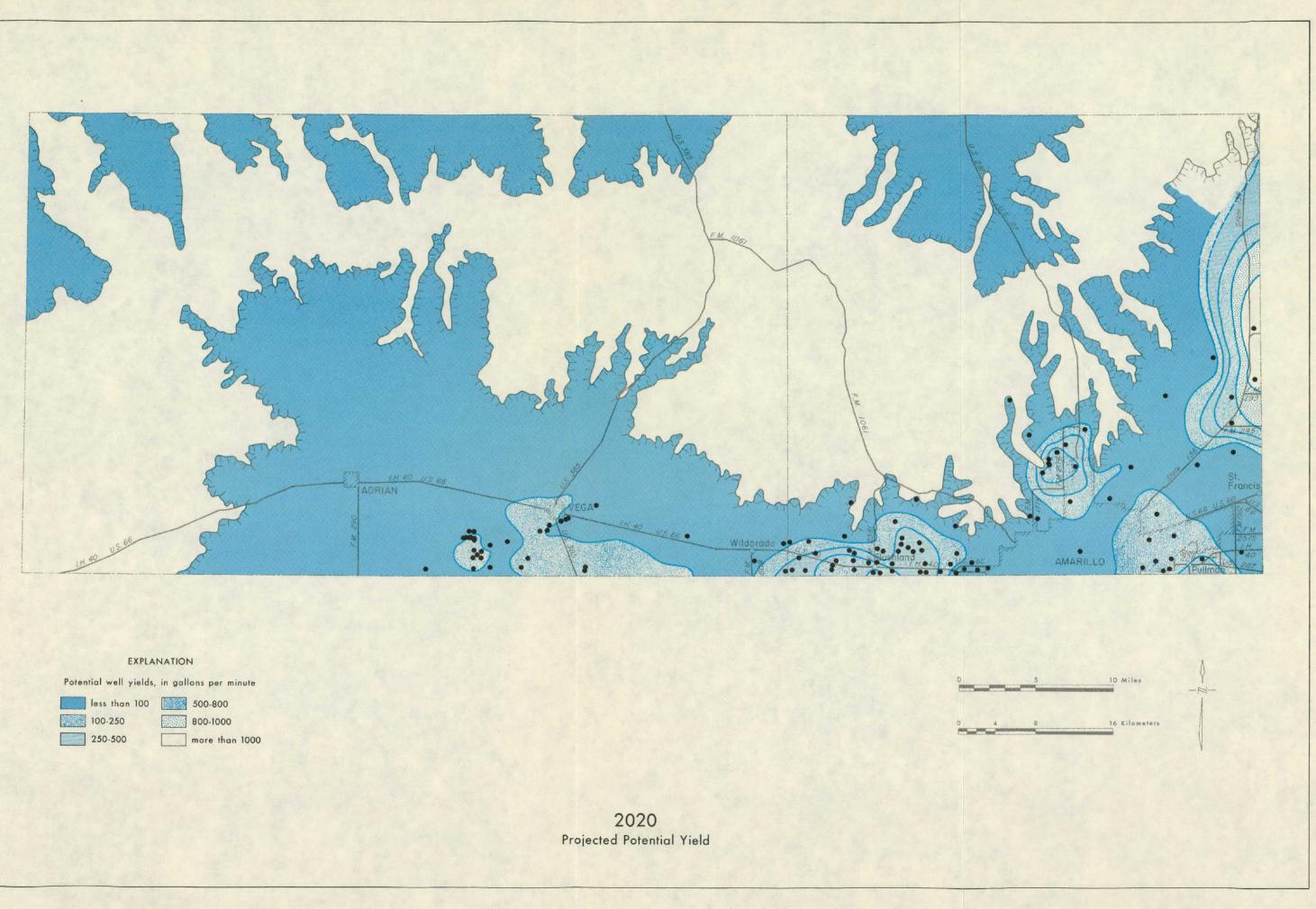
less than 100	500-800
100-250	800-1000
250-500	more than 10

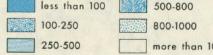


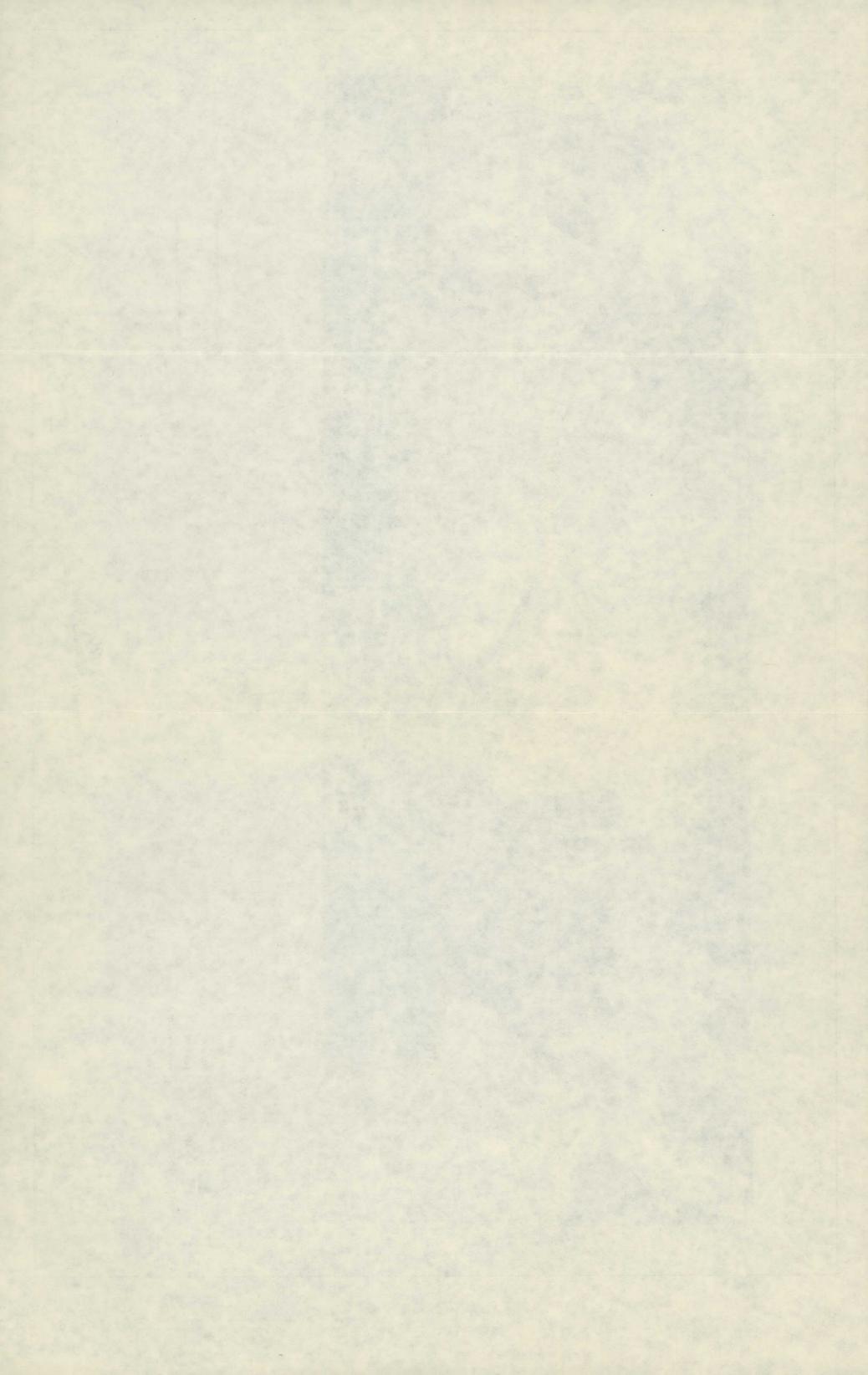












PUMPING LIFTS IN THE OGALLALA AQUIFER

1974

Surface Area Corresponding to Mapped Pumping-Lift Intervals

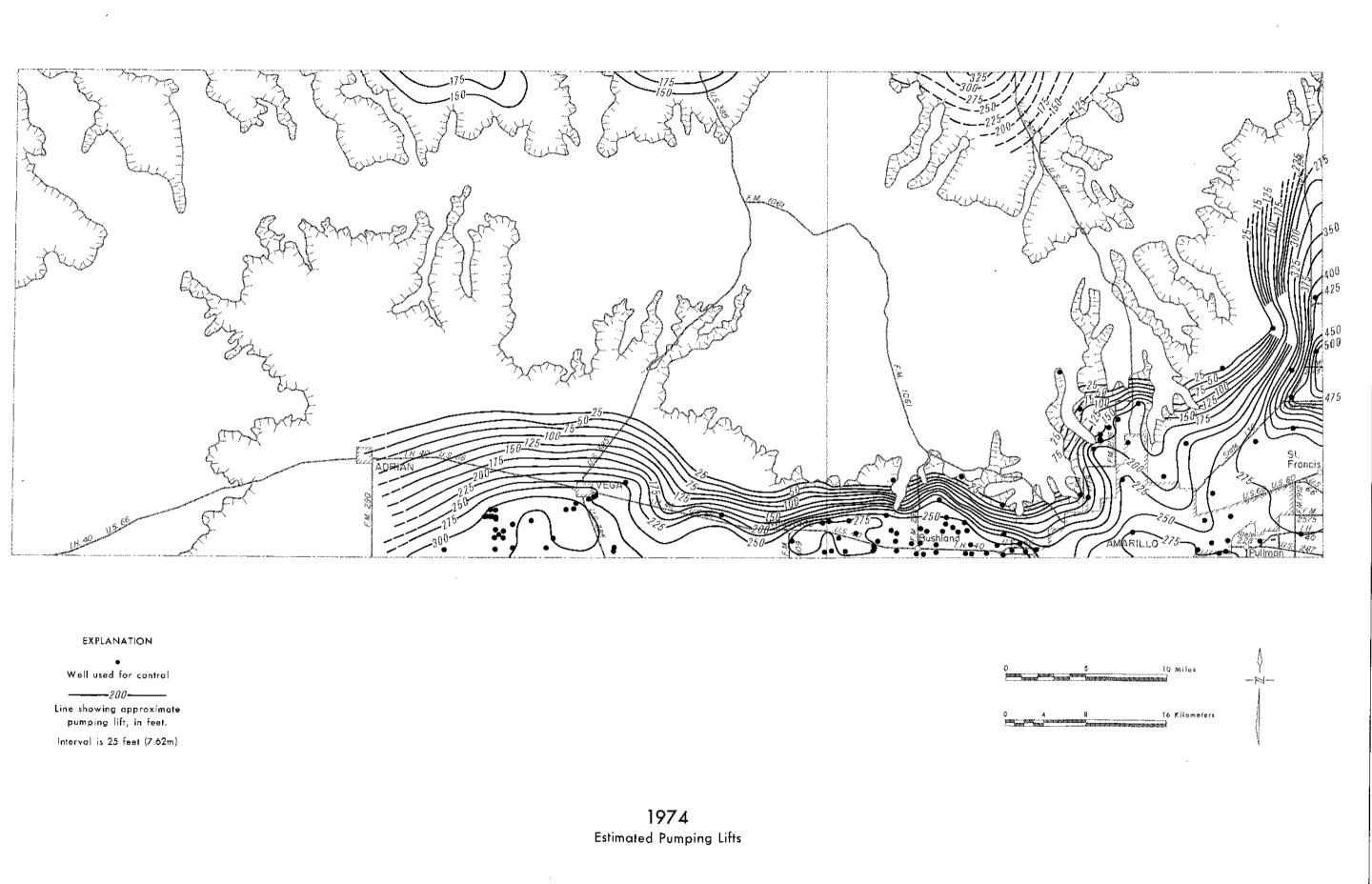
MAPPED PUMPING-LIFT	
INTERVAL	SURFACE AREA
(feet)	(acres)
0- 25	28,952
25 50	3,922
50- 75	5,483
75-100	4,500
100-125	28,643
125-160	19,524
150—175	19,183
175-200	16,957
200225	16,570
225-250	19,453
250-275	34,241
275-300	20,180
300-325	4,115
325-350	1,543
350-375	1,543
375-400	686
400-425	857
425-450	857
450-475	1,544
475-500	514
500525	1,025
τοται	230,292

OLDHAM COUNTY

1974

Surface Area Corresponding to Mapped Pumping-Lift Intervals

MAPPED PUMPING-LIFT INTERVAL (feet)	SURFACE AREA (acres)
0- 25	329,558
25- 50	2,245
50- 75	3,327
75-100	3,757
100-125	4,899
125150	35,125
150-175	24,943
175-200	3,630
200225	3,071
225250	2,789
250-275	7,184
275-300	11,531
300-325	19,141
TOTAL	451,200



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Surface Area Corresponding to Mapped Pumping-Lift Intervals

	MAPPED
	PUMPING-LIFT
	INTERVAL
	(feet)
,	(1001)
	025
	25- 50
	50- 75
	75-100
	100-125
	125-150
	150-175
	175-200
	200225
	225-250
	250-275
	275-300
	300-325
	325350
	350-375
	375-400
	400-425
	425-450
	450475
	475-500
	500-525
	525-550
	TOTAL

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Surface Area Corresponding to Mapped Pumping-Lift Intervals

MAPPED PUMPING-LIFT INTERVAL (feet) 0-25 25-50 50-75 75-100 100-125 125-150 150-175 175-200 200-225 225-250 250-275 275-300 300-325 325-350

TOTAL

1980

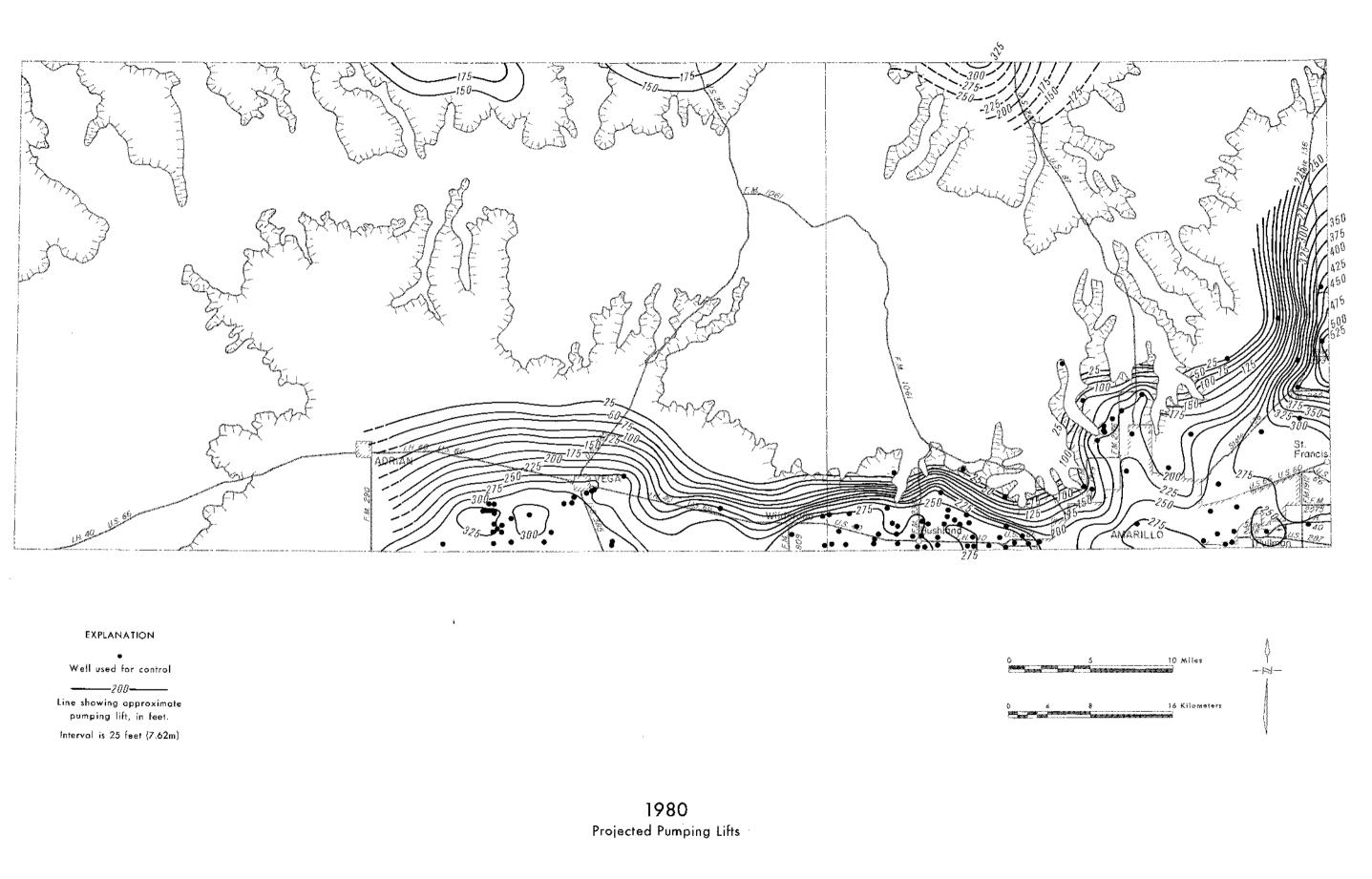
SURFACE AREA (acres)
28,923
3,922
4,968
4,757
28,872 18,776 -
19,142
12,307
16,754
16.441
34,984
28,474
3.060
1,543
857
1,716
170
1,372
514
1,543
684
513
230,292

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OLDHAM COUNTY

1980

SURFACE AREA (acres)
329,558
2,245
3.327
3,757
4,899
35,125
24,663
3,909
2,792
3,068
5,861
8,859
17,274
5,863
451,200



1990

Surface Area Corresponding to Mapped Pumping-Lift Intervals

	MAPPED
	PUMPING-LIFT
	INTERVAL
	(feet)
	0- 25
	25- 50
	50- 75
	75-100
·	100-125
	125-150
	150-175
	175-200
	200225
	225-250
	250-275
	275-300
	300-325
	325-350
	350-375
	375-400
	400-425
	425450
	450-475
·	475-500
	500-525
	525-550
	550-575

TOTAL

0 25 25 50
50- 75 75-100 100-125 125-150 150-175 175-200 200-225 225-250 250-275 275-300 300-325 325-350
TOTAL

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SURFACE AREA
28,876
3,695
4,559
4,862
28,455
19,033
18,253
11,577
14,993
16,619
30,111
34,144
6,032
1,543 857
1.544
514
171
1,372
514
1,371
684
513
230,292

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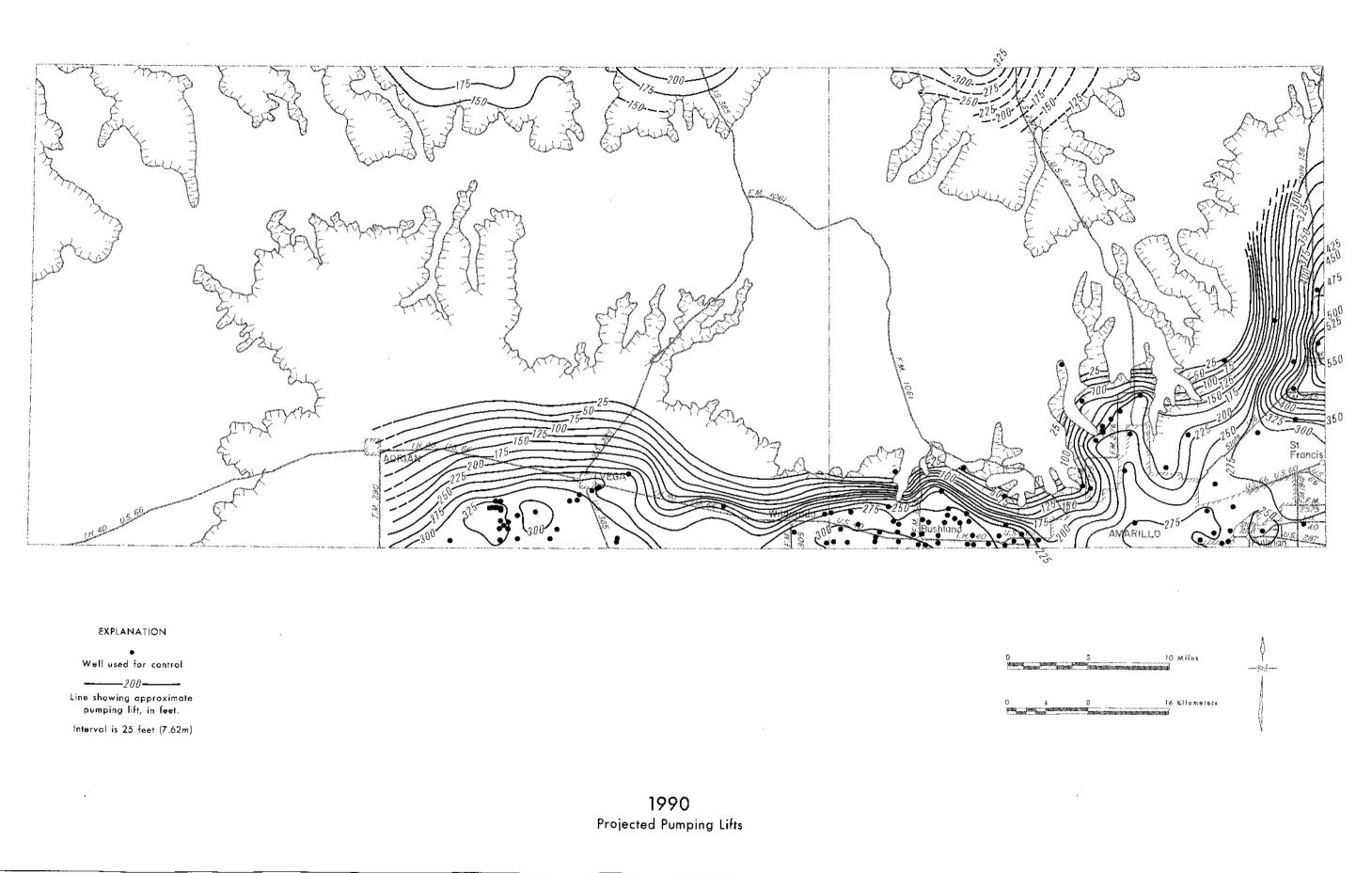
.

OLDHAM COUNTY

1990

Surface Area Corresponding to Mapped Pumping-Lift Intervals

(acres)	
329,558 2,245 3,067 3,996 4,921 34,845 23,384 4,909 3,350 2,789 5,861 8,859 17,037 6,379 451,200	



Surface Area Corresponding to Mapped Pumping-Lift Intervals

MAPPED PUMPING-LIFT INTERVAL (feet)
0-25
25- 50 50- 75
50-75
75-100
100-125
125-150
150175
175–200
200–225
225-250
250-275
275-300
300–325
325350
350375
375–400
400-425
425450
450-475
475–500
500-525
525-550
550-575
575-600
TOTAL

2000

Surfa	ce Area	Corre
	Pum	ping-l

MAPPED PUMPING-LIFT INTERVAL (feet)
0- 2 5
0- 25 25- 50
50- 75
75100
100-125
125–150
150-175
175– 20 0
200~225
225-250
250-275
275-300
300-325
325-350
TOTAL

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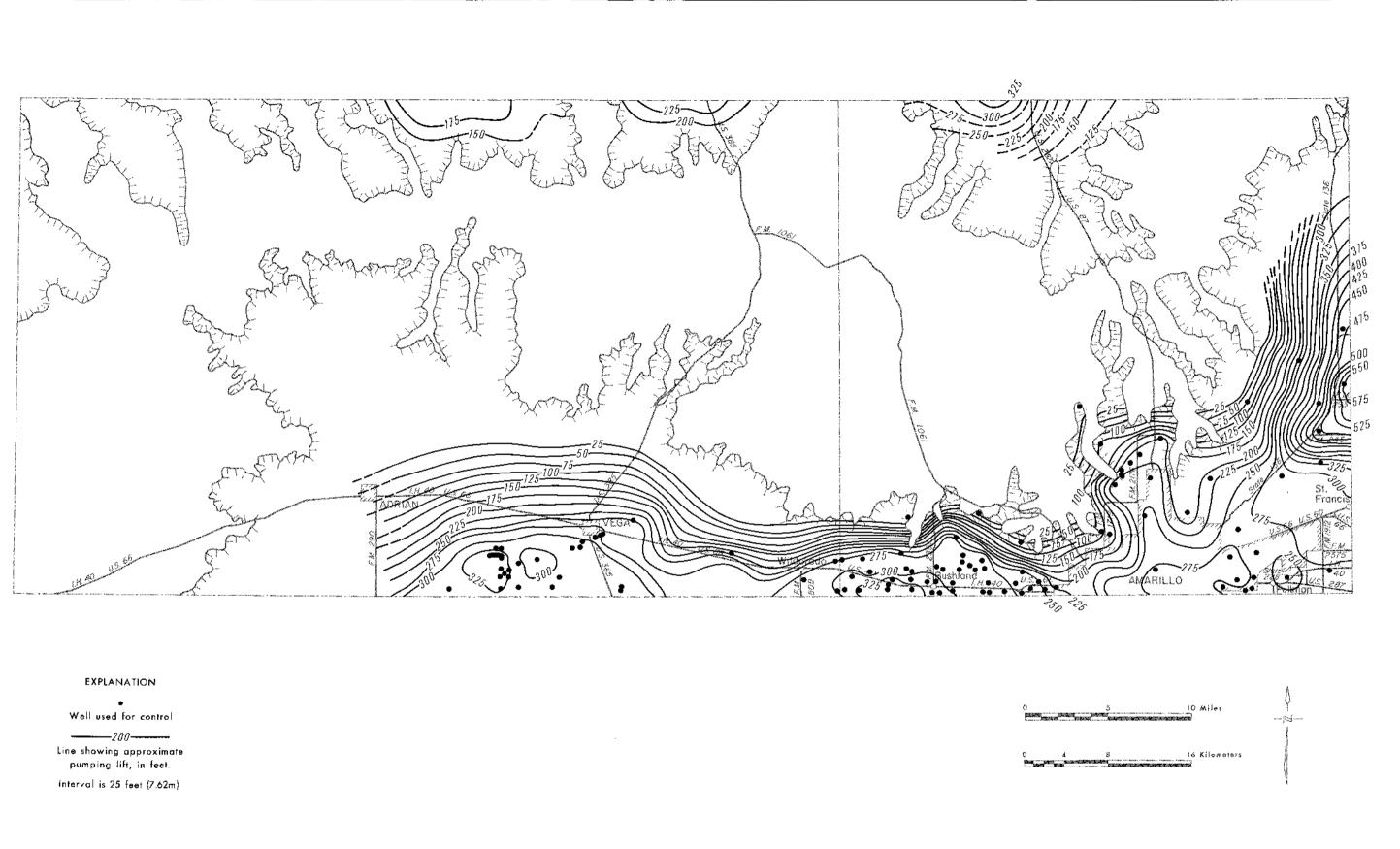
2000

(acres)
28,555
3,850
4,650
4,593
28,455
19,232
17,711
10,387
14,982
17,477
28,913
34,324
6,286
3,337
514
858
1,372
170
1,029
514
858
1,200
512
513
230,292

OLDHAM COUNTY

responding to Mapped -Lift Intervals

SURFACE AREA (acres)
329,558 2,245 3,067 3,996 4,919 24,567 32,663 5,630 3,630 2,789 5,303 9,138
17,595 6,100 451,200
•



2000 Projected Pumping Lifts

2010

INTE (f)))))))))))))	APPED
(f 0 25 50 76 100 125 150 125 200 225 255 300 400 425 355 3555 35555 55555555555555555555	ING-LIFT
(f 0 0 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	ERVAL
0 25 30 75 100 125 200 225 250 300 325 350 350 355 355 355 355 355 3555 35	(feet)
25 50 75 100 125 150 200 225 225 225 225 235 300 325 330 325 340 325 340 345 345 345 355 355 355 355 355 355 355	
26 50 75 100 125 130 135 135 200 225 250 300 325 330 325 350 355 355 555 555	0- 25
50 76 100 125 150 178 220 225 250 225 300 325 300 325 360 375 400 425 450 475 575 575	5- 50
76 100 125 150 177 200 225 275 300 302 375 360 375 450 450 450 450 450 555 550 575	0- 75
100 125 150 175 200 275 250 275 300 325 360 375 360 375 360 375 360 375 360 375 360 375 360 375 360 375 360 375 375 375 375 375 375 375 375 375 375	5-100
126 150 220 225 250 275 300 375 360 375 400 425 450 575 575	0-125
150 175 200 225 250 300 325 350 350 400 425 450 450 450 455 550 550 555 550 575	6–150
175 200 225 250 275 300 325 350 375 400 425 450 475 550 575	0-175
225 250 275 300 325 350 375 400 425 450 475 550 575	5-200
250 275 300 325 350 375 400 425 450 475 500 525 550 575	0-225
275 300 325 350 375 400 425 450 475 500 525 550 575	5-250
300 325 350 400 425 450 475 500 525 550 575	0-275
325 350 375 400 425 450 475 500 525 550 575	5-300
350 375 425 450 475 500 525 550 575	0-325
375 400 425 450 475 500 525 550 575	5-350
400 425 450 575 500 525 550 575	0375
425 450 475 500 525 550 575	5-400
450 475 500 525 550 575	0-425
475 500 525 550 575	5-450
500 525 550 575	0-475
525 550 575	5-500
550 575	0-525
575	5-550
	0-575
то	5-600
	OTAL

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OLDHAM COUNTY

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Surface Area Corresponding to Mapped Pumping-Lift Intervals

MAPPED PUMPING-LIFT INTERVAL (feet)
0- 25 25- 50 50- 75 75-100 100-125 125-150 150-175 175-200 200-225 225-250 250-275 275-300 300-325 325-350 TOTAL

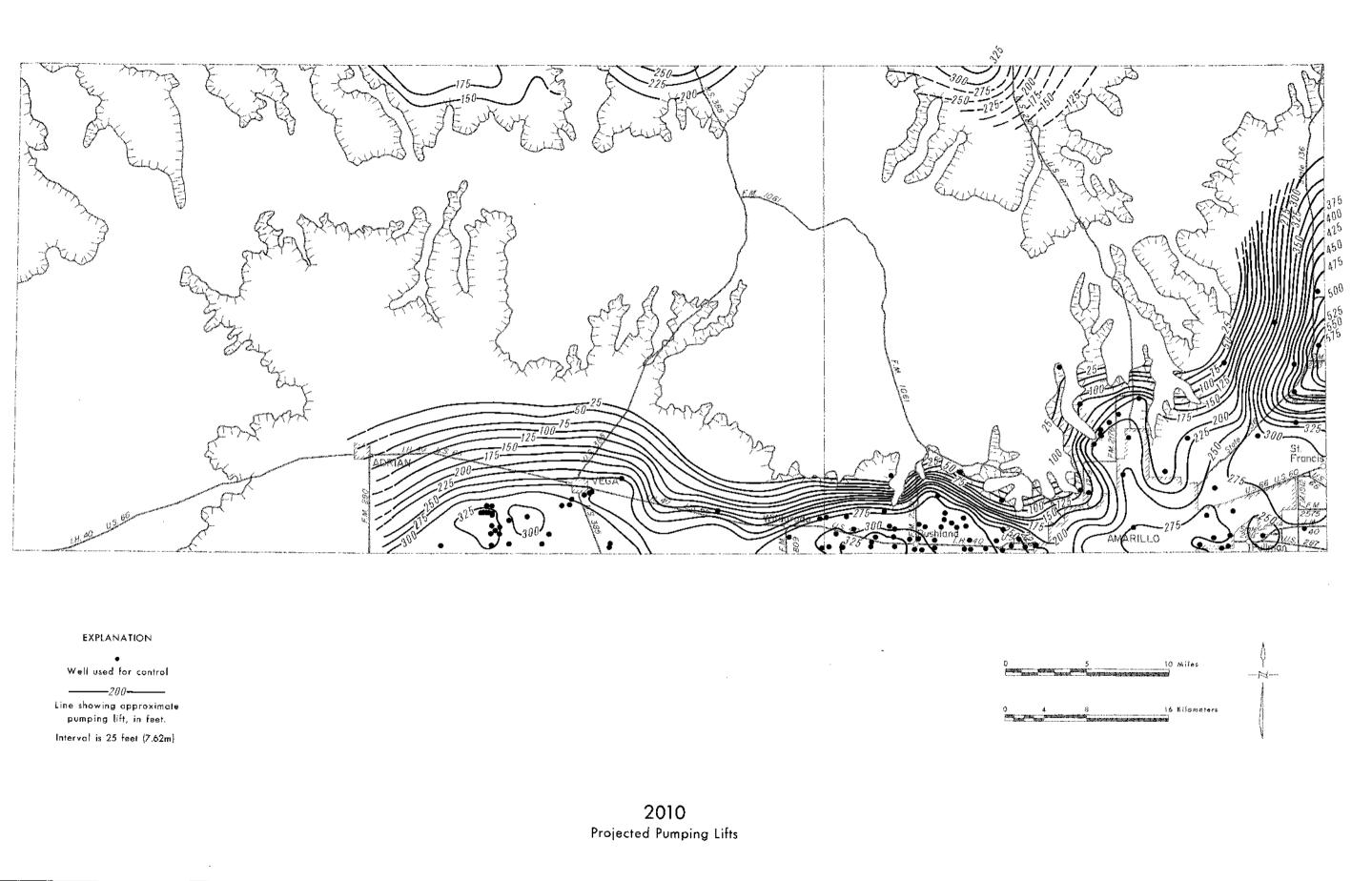
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Surface Area Corresponding to Mapped Pumping-Lift Intervals

SURFACE AREA
(acres)
28.015
28,215 3.678
3,678
4,479
· · ·
28,363
18,816 17,512
10,751
14.776
17,510
29,428
33,809
6,126
3,325
1,029
685
1.201
857
514
1.201
342
1.029
1.028
1.025
230,292

2010

SURFACE AREA (acres)
329,558
2,245
3,067
3,996
4,919
24,567
30,663
7,630
3,630
2,789
5,303
8,932
17,801
6,100
451,200



MAPPED PUMPING-LIFT INTERVAL (feet)
$\begin{array}{c} 0-25\\ 25-50\\ 50-75\\ 75-100\\ 100-125\\ 125-150\\ 150-175\\ 175-200\\ 200-225\\ 225-250\\ 250-275\\ 275-300\\ 300-325\\ 325-350\\ 350-375\\ 375-400\\ 400-425\\ 425-450\\ 450-475\\ 475-500\\ 500-575\\ 525-550\\ 550-575\\ 575-600\\ TOTAL \end{array}$
IOTAL

Surface Area Corresponding to Mapped Pumping-Lift Intervals

MAPPED
PUMPING-LIFT
INTERVAL
(feet)
0-25
25- 50
50- 75
75-100
100 -125
125-150
150-175
175-200
200-225
225-250
250-275
275-300
300-325
325-350
TOTAL

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2020

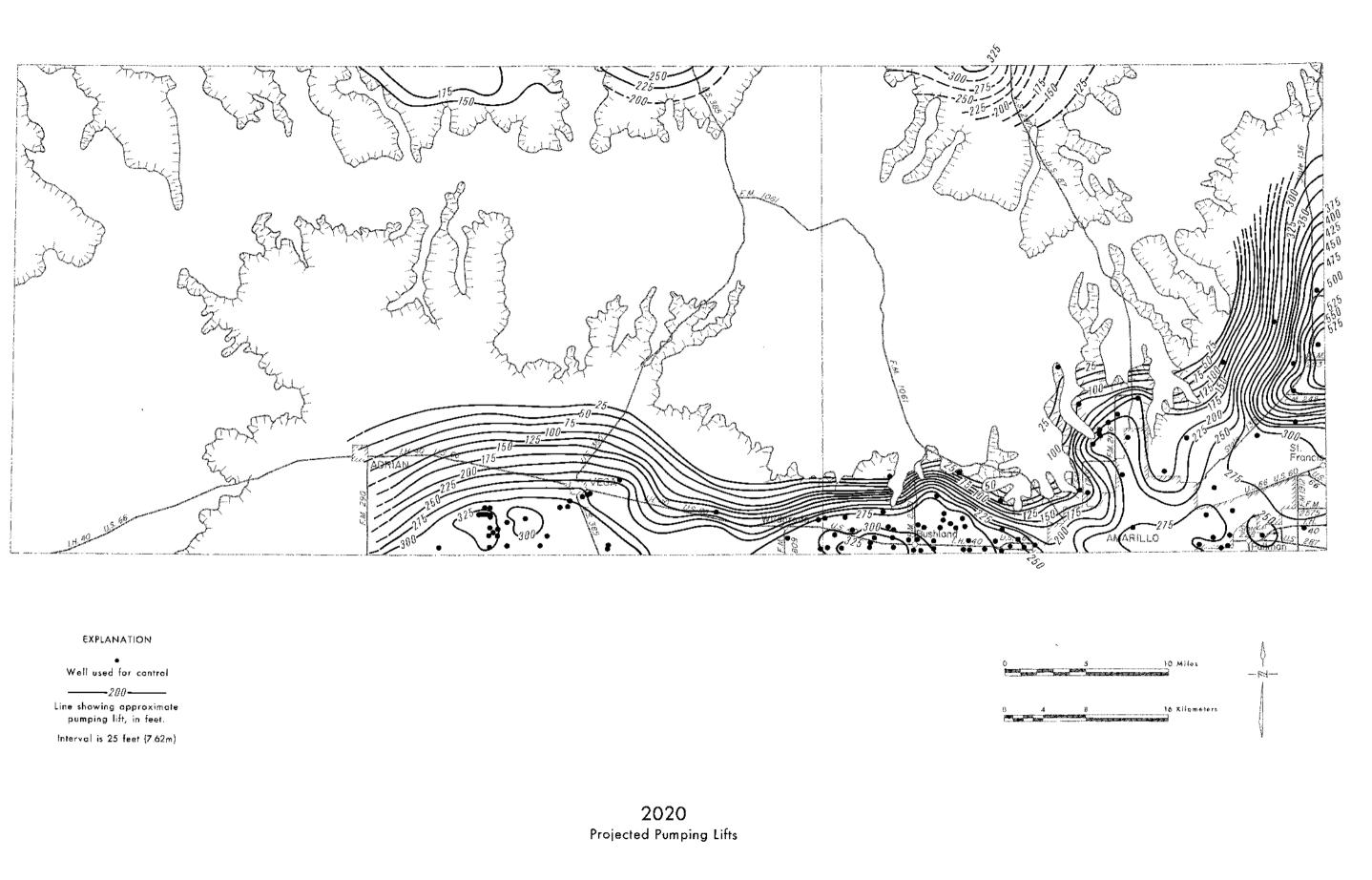
Surface Area Corresponding to Mapped Pumping-Lift Intervals

(acres) 28,730 3,678 4,479 4,421 28,535 18,816 17,341 10,922 14,432 17,682 29,428 33,809 5,955 3,497 1,201 514 1,029 1,028 171 1,029 514 514 857 1,710 230,292	SURFACE AREA
3,678 4,479 4,421 28,535 18,816 17,341 10,922 14,432 17,682 29,428 33,809 5,955 3,497 1,201 514 1,029 1,028 171 1,029 514 514 514 857 1,710	(acres)
3,678 4,479 4,421 28,535 18,816 17,341 10,922 14,432 17,682 29,428 33,809 5,955 3,497 1,201 514 1,029 1,028 171 1,029 514 514 514 857 1,710	· · · ·
3,678 4,479 4,421 28,535 18,816 17,341 10,922 14,432 17,682 29,428 33,809 5,955 3,497 1,201 514 1,029 1,028 171 1,029 514 514 514 857 1,710	
4,479 4,421 28,535 18,816 17,341 10,922 14,432 17,682 29,428 33,809 5,955 3,497 1,201 514 1,029 1,028 171 1,029 514 514 514 514 857 1,710	•
4,421 28,535 18,816 17,341 10,922 14,432 17,682 29,428 33,809 5,955 3,497 1,201 514 1,029 1,028 171 1,029 514 514 514 514 857 1,710	,
28,535 18,816 17,341 10,922 14,432 17,682 29,428 33,809 5,955 3,497 1,201 514 1,029 1,028 171 1,029 514 514 514 514 857 1,710	
18,816 17,341 10,922 14,432 17,682 29,428 33,809 5,955 3,497 1,201 514 1,029 1,028 171 1,029 514 514 514 514 857 1,710	
17,341 10,922 14,432 17,682 29,428 33,809 5,955 3,497 1,201 514 1,029 1,028 171 1,029 514 514 514 514 514 514	
10,922 14,432 17,682 29,428 33,809 5,955 3,497 1,201 514 1,029 1,028 171 1,029 514 514 514 514 857 1,710	
14,432 17,682 29,428 33,809 5,955 3,497 1,201 514 1,029 1,028 171 1,029 514 514 514 514 514	
17,682 29,428 33,809 5,955 3,497 1,201 514 1,029 1,028 171 1,029 514 514 514 857 1,710	
29,428 33,809 5,955 3,497 1,201 514 1,029 1,028 171 1,029 514 514 514 857 1,710	14,432
33,809 5,955 3,497 1,201 514 1,029 1,028 171 1,029 514 514 514 857 1,710	17,682
5,955 3,497 1,201 514 1,029 1,028 171 1,029 514 514 514 857 1,710	29,428
3,497 1,201 514 1,029 1,028 171 1,029 514 514 857 1,710	33,809
1,201 514 1,029 1,028 171 1,029 514 514 857 1,710	5,955
514 1,029 1,028 171 1,029 514 514 857 1,710	3,497
1,029 1,028 171 1,029 514 514 514 857 1,710	1,201
1,028 171 1,029 514 514 857 1,710	514
171 1,029 514 514 857 1,710	1,029
1,029 514 514 857 1,710	1,028
514 514 857 1,710	171
514 857 1,710	1,029
857 1,710	514
1,710	514
	857
230,292	1,710
230,292	230 292
	200,292

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OLDHAM COUNTY

SURFACE AREA (acres)
329,558
2,245
3,067
3,996
4,919
24,567
30,663
7,630
3,630
2,789
5,303
8,932
17,801
6,100
451,200



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PUMPAGE FROM THE OGALLALA AQUIFER

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1974

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Pumpage Corresponding to Mapped Decline-Rate Intervals

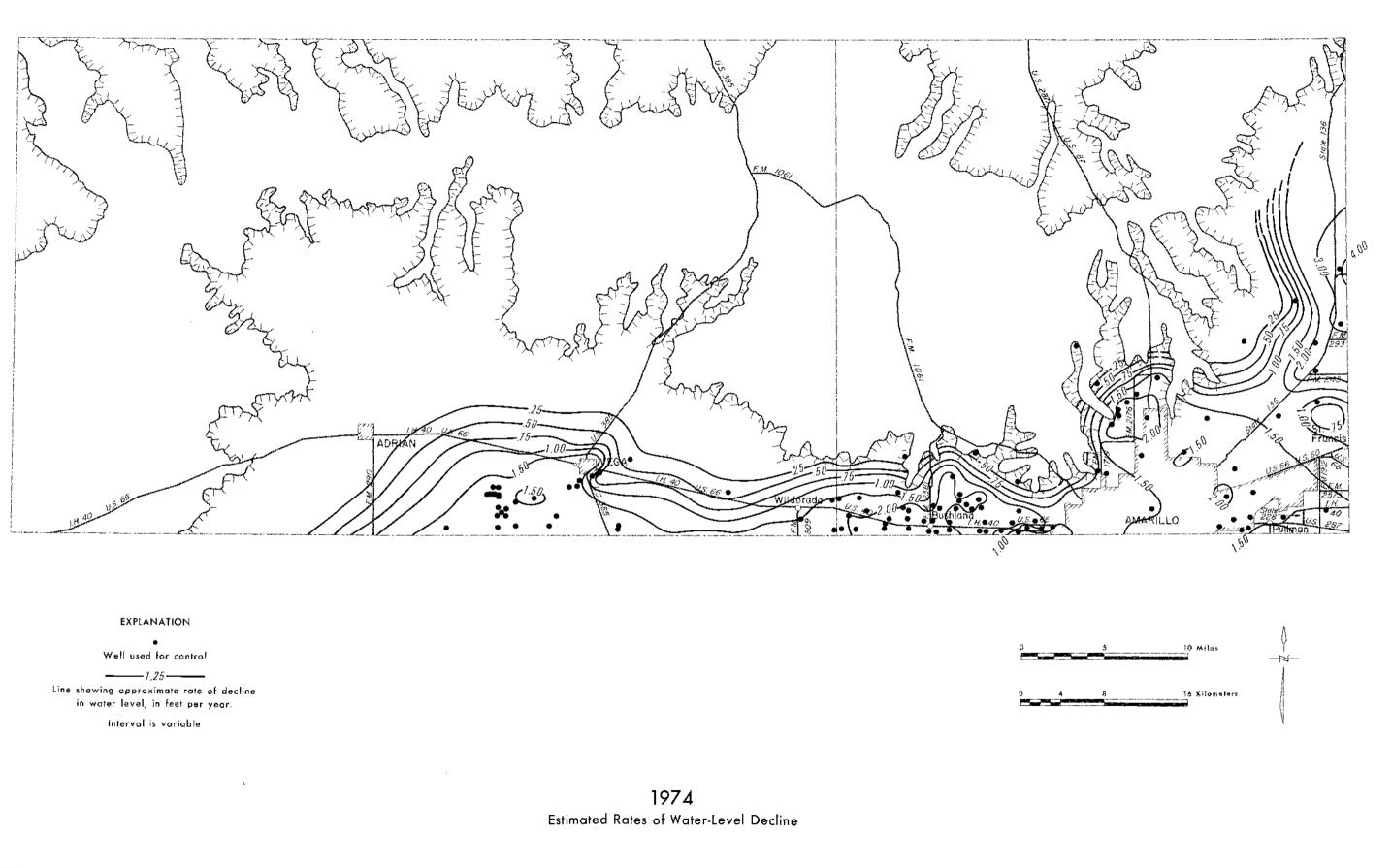
MAPPED DECLINE- RATE INTERVAL (feet)	SURFACE AREA	STORAGE CAPACITY OF DEWATERED SECTION (acre-feet)	ESTIMATED PUMPAGE RATE, INCLUDING NATURAL RECHARGE AND IRRIGATION RECIRCULATION (acre-feet per year)
0.00-0.25	78,496	133	572
.2550	8,136	456	875
.5075	8,539	813	1,285
.75-1.00	10,668	1,414	2,044
1.00-1.50	38,365	7,504	10,013
1.50-2.00	67,519	17,279	22,101
2.00-3.00	17,224	5,865	7,241
3.00-4.00	1,053	500	597
4.00-5.00	292	198	230
TOTAL	230,292	34,162	44,958

OLDHAM COUNTY

1974

Pumpage Corresponding to Mapped Decline-Rate Intervals

MAPPED DECLINE- RATE INTERVAL (feet)	SURFACE AREA (acres)	STORAGE CAPACITY OF DEWATERED SECTION {acre-feet}	ESTIMATED PUMPAGE RATE, INCLUDING NATURAL RECHARGE AND IRRIGATION RECIRCULATION (acre-feet per year)
0.00-0.25	385,445	168	492
.25— .50	11,989	657	1,272
.5075	10,858	1,004	1,603
.751.00	8,126	1,068	1,547
1.00-1.50	12,004	2,329	3,112
1.50-2.00	22,778	5,787	7,406
TOTAL	451,200	11,013	15,432



1980

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MAPPED DECLINE- RATE INTERVAL (feet)	SURFACE AREA (acres)	STORAGE CAPACITY OF DEWATERED SECTION (acre-feet)	ESTIMATED PUMPAGE RATE, INCLUDING NATURAL RECHARGE AND IRRIGATION RECIRCULATION (acre-feet per year)
0.00-0.25	78,830	169	667
,2550	7,705	416	811
.5075	10,697	1,031	1,625
.75-1.00	15,559	2,067	2,987
1.00-1.50	48,688	9,271	12,430
1.50-2.00	56,259	14,066	18,051
2.00-3.00	11,698	3,891	4,816
3.00-4.00	856	416	497
TOTAL	230,292	31,327	41,884

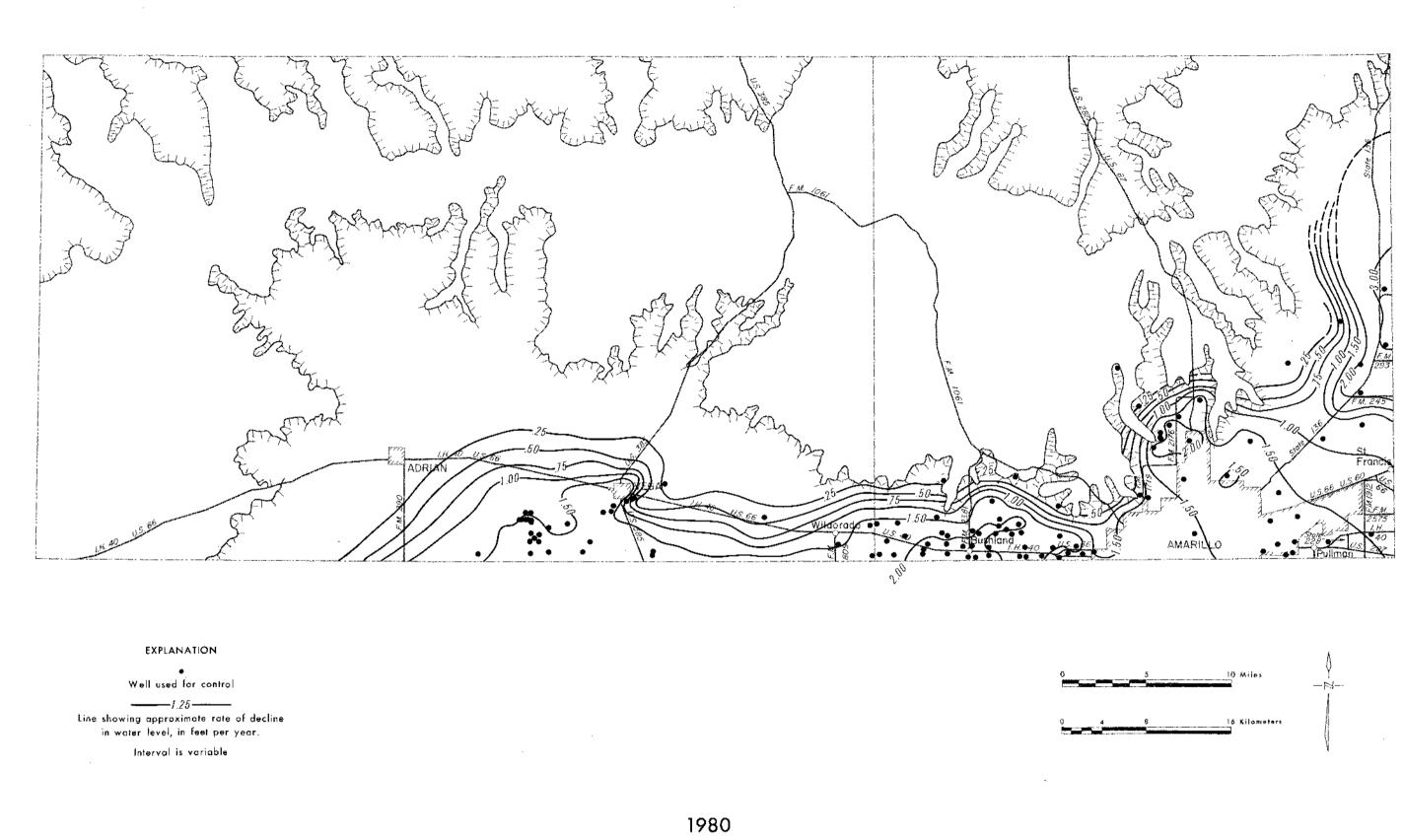
Pumpage Corresponding to Mapped Decline-Rate Intervals

MAPPED DECLINE- RATE INTERVAL (feet)	SURFACE AREA	STORAGE CAPACITY OF DEWATERED SECTION (acre-feet)	ESTIMATED PUMPAGE RATE, INCLUDING NATURAL RECHARGE AND IRRIGATION RECIRCULATION (acre-feet per year)
0.00-0.25	389,156	194	652
.2550	11,908	666	1,278
.50— .75	9,182	843	1,348
.75-1.00	6,730	874	1,269
1.00-1.50	13,679	2,655	3,548
1.50-2.00	20,545	5,132	6,584
TOTAL	451,200	10,364	14,679

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Pumpage Corresponding to Mapped Decline-Rate Intervals

OLDHAM COUNTY



Projected Rates of Water-Level Decline

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MAPPED DECLINE- RATE INTERVAL (feet)	SURFACE AREA	STORAGE CAPACITY OF DEWATERED SECTION (acre-feet)	ESTIMATED PUMPAGE RATE, INCLUDING NATURAL RECHARGE AND IRRIGATION RECIRCULATION (acre-feet per year)
0.00-0.25	79.834	194	734
.2550	9,190	496	966
.5075	19,837	1,928	3,030
.751.00	32,243	4,208	6,107
1.00-1.50	52,231	9,784	13,157
1.50-2.00	31,815	7,906	10,155
2.00-3.00	5,142	1,835	2,255
TOTAL	230,292	26,351	36,404

Pumpage Corresponding to Mapped **Decline-Rate Intervals**

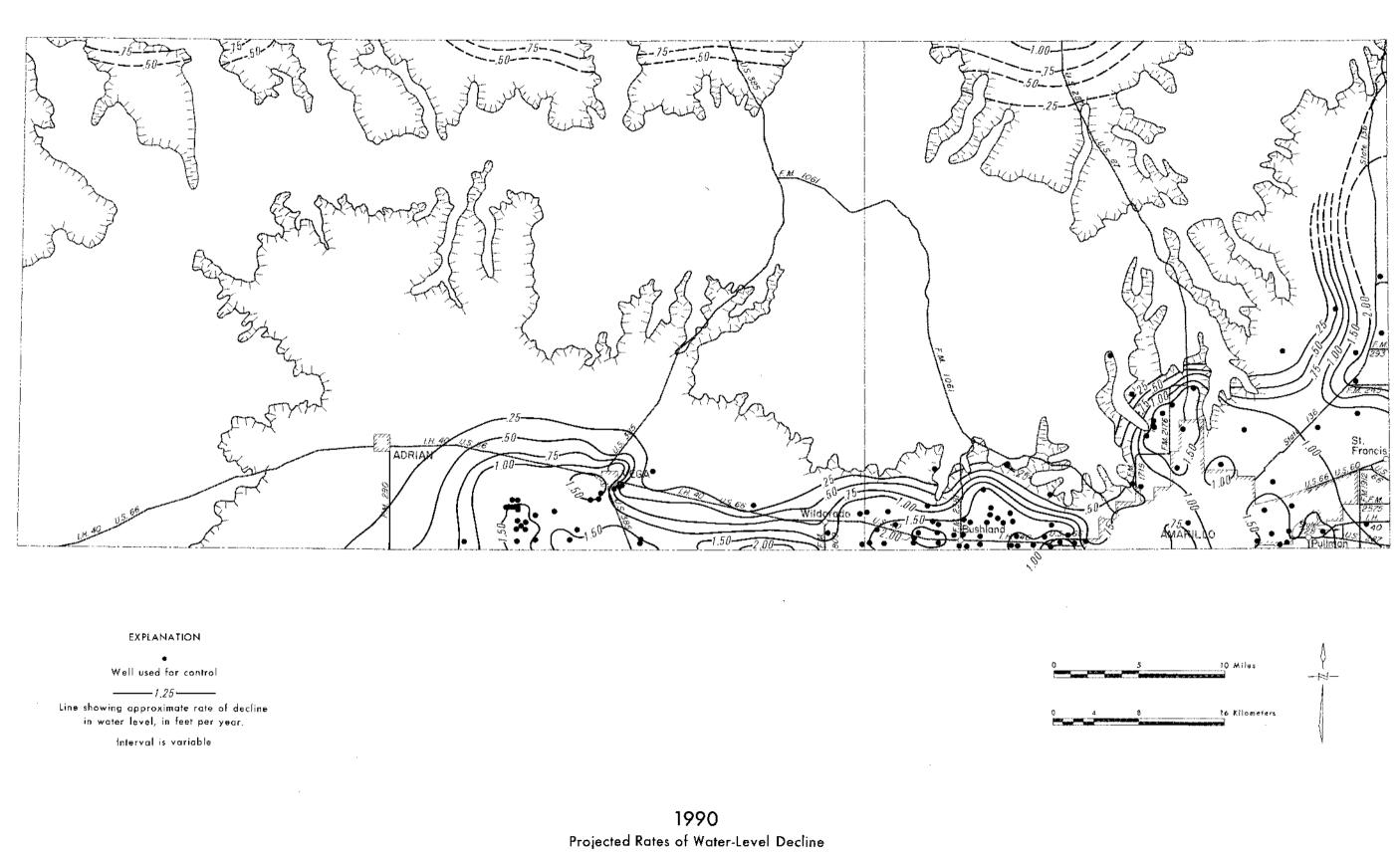
MAPPED DECLINE- RATE INTERVAL (feet)	SURFACE AREA (acres)	STORAGE CAPACITY OF DEWATERED SECTION (acre-feet)	ESTIMATED PUMPAGE RATE, INCLUDING NATURAL RECHARGE AND IRRIGATION RECIRCULATION (acre-feet per year)
0.00-0.25	396,242	295	1,096
.2550	11,379	649	1,236
.50— .75	7,205	684	1,083
.75-1.00	6,021	776	1,130
1.00-1.50	20,095	4,044	5,369
1.50-2.00	9,979	2,354	3,047
2.00-3.00	279	84	106
TOTAL	451,200	8.886	13,067

1990

Pumpage Corresponding to Mapped Decline-Rate Intervals

OLDHAM COUNTY

1990



MAPPED DECLINE- RATE INTERVAL (feet)	SURFACE AREA	STORAGE CAPACITY OF DEWATERED SECTION (acre-feet)	ESTIMATED PUMPAGE RATE, INCLUDING NATURAL RECHARGE AND IRRIGATION RECIRCULATION (acre-feet per year)
0.00-0.25	83,221	259	965
.2550	14,551	813	1,559
.5075	26,249	2,519	3,974
.75-1.00	35,389	4,659	6,747
1.00-1.50	52,694	9,820	13,217
1.50-2.00	16,305	3,975	5,120
2.00-3.00	1,883	679	833
TOTAL	230,292	22,724	32,415

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Pumpage Corresponding to Mapped Decline-Rate Intervals

			ESTIMATED PUMPAGE RATE,
		STORAGE CAPACITY	INCLUDING NATURAL
MAPPED DECLINE-		OF DEWATERED	RECHARGE AND
RATE INTERVAL	SURFACE AREA	SECTION	IRRIGATION RECIRCULATION
(feet)	(acres)	(acre-feet)	(acre-feet per year)
0.00-0.25	400.084	352	1,340
.2550	17,731	968	1,877
.5075	8,653	785	1,260
.75-1,00	9,171	1,209	1,750
1.00-1.50	15,561	2,777	3,766
TOTAL	451,200	6,091	9,993

2000

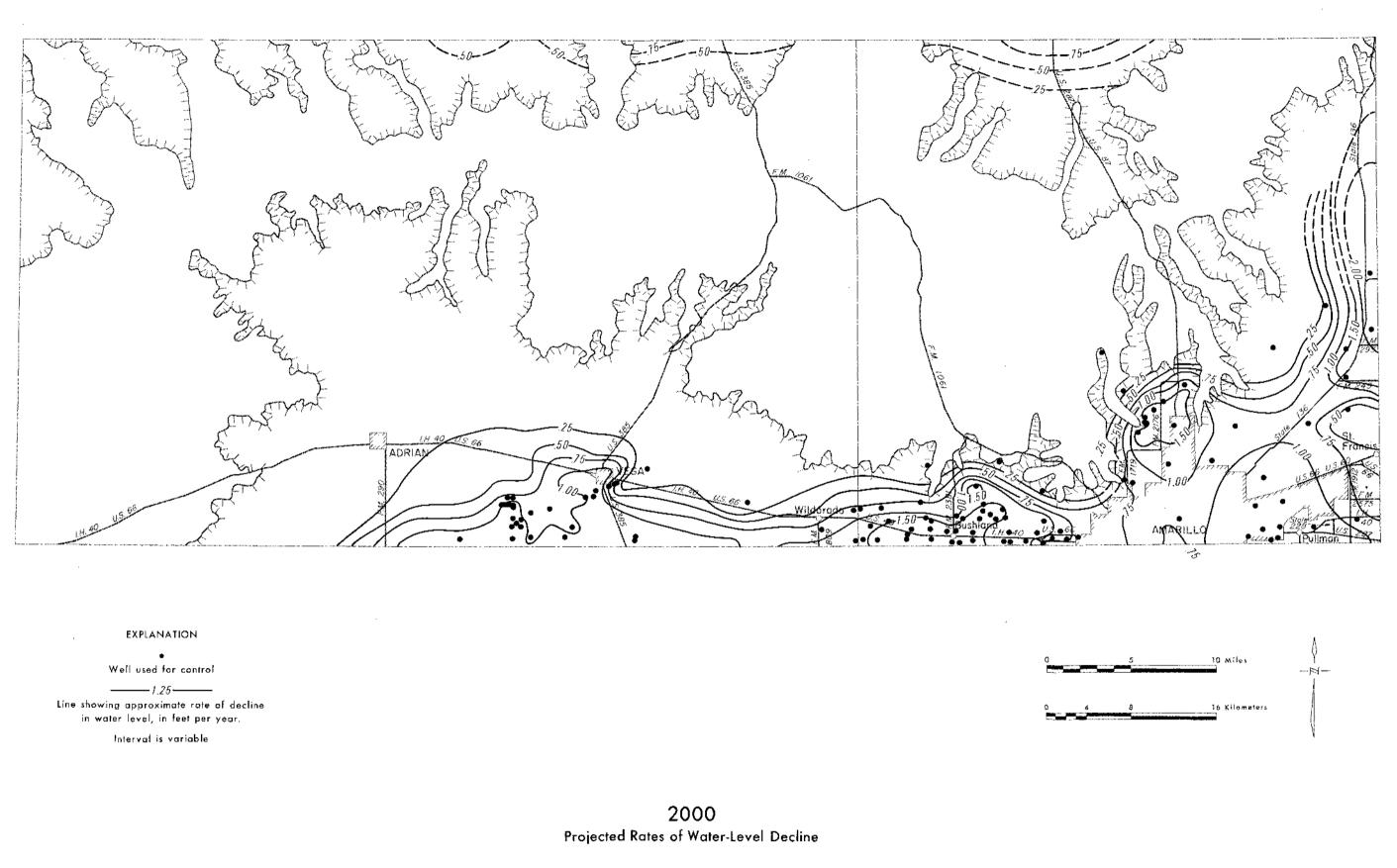
Pumpage Corresponding to Mapped Decline-Rate Intervals

OLDHAM COUNTY

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2000

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STORAGE CAPACITY	ESTIMATED PUMPAGE RATE, INCLUDING NATURAL	
OF DEWATERED	RECHARGE AND	
SECTION	IRRIGATION RECIRCULATION	
(acre-feet)	(acre-feet per year)	
344 2,177	1,239 4,076	
3,969 4,0 4 4	6,303 5,886	
4,955	6,688	
1,224	1,570	
290	359	
17.002	00 101	

MAPPED DECLINE- RATE INTERVAL (feet)	SURFACE AREA (acres)	STORAGE CAPACITY OF DEWATERED SECTION (acre-feet)	INCLUDING NATURAL RECHARGE AND IRRIGATION RECIRCULATION (acre-feet per year)
0.00-0.25	87,253	344	1,239
.2550	36,671	2,177	4,076
.5075	42,253	3,969	6,303
.75-1.00	31,357	4,044	5,886
1.001.50	27,007	4,955	6,688
1.50-2.00	4,895	1,224	1,570
2.00-3.00	856	290	359
TOTAL	230,292	17,003	26,121

MAPPED DECLINE- RATE INTERVAL (feet)	SURFACE AREA (acres)	STORAGE CAPACITY OF DEWATERED SECTION (acre-feet)	INCLUDING NATURAL RECHARGE AND IRRIGATION RECIRCULATION (acre-feet per year)
0.00-0.25	402,336	376	1,470
.2550	13,046	703	1,372
.5075	8,290	769	1,225
.75-1.00	22,069	2,830	4,125
1.00-1.50	5,459	995	1,341
TOTAL	451,200	5,673	9,534

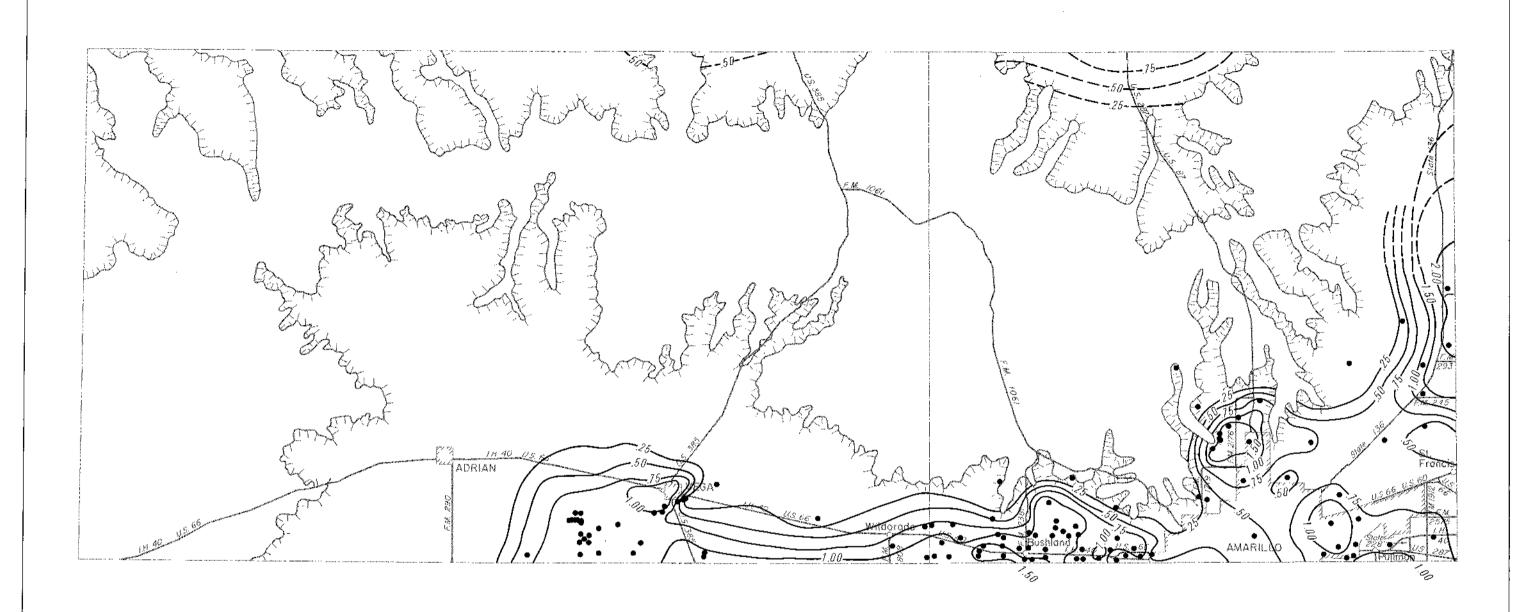
2010

Pumpage Corresponding to Mapped Decline-Rate Intervals

OLDHAM COUNTY

2010

Pumpage Corresponding to Mapped Decline-Rate Intervals



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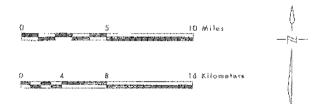
EXPLANATION

• Well used for control

Line showing approximate rate of decline in water level, in feet per year.

Interval is variable

2010 Projected Rates of Water-Level Decline



MAPPED DECLINE- RATE INTERVAL (feet)	SURFACE AREA	STORAGE CAPACITY OF DEWATERED SECTION (acre-feet)	ESTIMATED PUMPAGE RATE, INCLUDING NATURAL RECHARGE AND IRRIGATION RECIRCULATION (acre-feet per year)
0.00-0.25	102.301	604	2,034
.2550	47,042	2,656	5,078
.5075	34,815	3,210	5,127
.75–1.00	27,016	3,456	5,040
1.00-1.50	16,721	3,092	4,168
1.50-2.00	1,541	379	488
2.00-3.00	856	296	365
TOTAL	230,292	13,693	22,300

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MAPPED DECLINE- RATE INTERVAL (feet)	SURFACE AREA (acres)	STORAGE CAPACITY OF DEWATERED SECTION (acre-feet)	ESTIMATED PUMPAGE RATE, INCLUDING NATURAL RECHARGE AND IRRIGATION RECIRCULATION (acre-feet per year)
0.00-0.25	417,352	667	2,464
.2550	13,261	733	1,415
.50— .75	10,195	940	1,502
.75-1.00	8,159	1,036	1,513
1.00-1.50	2,233	418	559
TOTAL	451,200	3,794	7,453

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2020

Pumpage Corresponding to Mapped Decline-Rate Intervals

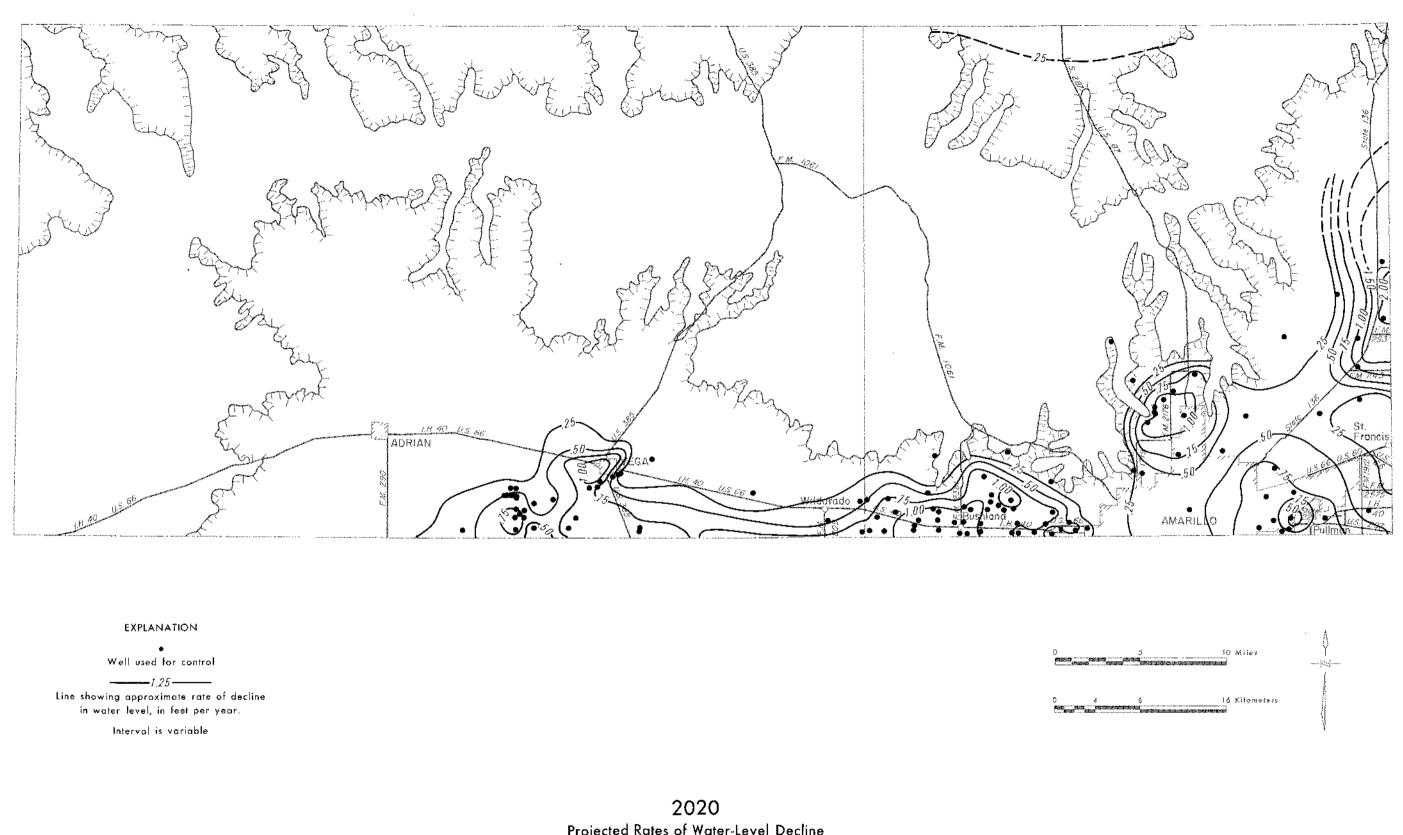
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OLDHAM COUNTY

2020

Pumpage Corresponding to Mapped Decline-Rate Intervals



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Projected Rates of Water-Level Decline

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ACKNOWLEDGEMENTS

Special appreciation is expressed to the Potter and Oldham County landowners and water users for allowing their wells to be measured by Department and Water District personnel. This study could not have been accomplished without their cooperation and the records obtained from their wells.

Special thanks are also expressed to the staff of the High Plains Underground Water Conservation District No. 1, Mr. A. Wayne Wyatt, manager, and to staff of the Panhandle Ground Water Conservation District No. 3, Mr. Felix W. Ryals, manager, for providing records and consultation during the study.

Additionally, appreciation is expressed to several individuals for consultation and for review and comment on the methodology and techniques employed in this study: Mr. Frank A. Rayner, former manager of the High Plains Underground Water Conservation District No. 1; Dr. Donald Reddell, associate professor of Engineering, Texas A&M University; Mr. Leon New, irrigation specialist, Texas Agriculture Extension Service, Lubbock, Texas; Mr. Shelby Newman, superintendent, Texas Agricultural Experiment Station, Stephenville, Texas; Dr. C. C. Reeves, Jr., professor of Geosciences, Texas Tech University; and Dr. James Osborn, former chairman of the Department of Agricultural Economics, Texas Tech University.

STAFF INVOLVEMENT

This report is one of a series of county reports being published under the title "Analytical Study of the Ogallala Aquifer." Former staff member A. Wayne Wyatt was instrumental in initiating the study and coauthored a number of the previously published reports of this series.

The Potter and Oldham Counties report was prepared under the supervision of Bernard B. Baker, head of the Ground Water Data Unit in the Texas Department of Water Resources' Data Collection and Evaluation Section, Dr. Tommy R. Knowles, chief. Numerous staff members of this Section assisted the authors in assembling and evaluating data and information. Overall technical supervision of the Ogallala study is exercised by C. R. Baskin, director, Data and Engineering Services Division. The Department's Information Systems and Services Office, David L. Ferguson, director, provided automated data processing and computational services, and prepared the manuscript copy of tabular and graphical displays.

METRIC CONVERSIONS TABLE

For those readers interested in using the International System (SI) of Units, the metric equivalents of English units of measurement have been given in parenthesis in the text. The English units used in tables of this report may be converted to metric units by the following conversion factors:

MULTIPLY ENGLISH UNITS	BY	TO OBTAIN SI UNITS
inches	2.540	centimeters (cm)
feet	.3048	méters (m)
miles	1.609	kilometers (km)
square miles	2.590	square kilometers (km²)
gallons	3.785	liters (I)
gallons per minute	.06309	liters per-second (I/s)
gallons per minute per foot	.207	liters per second per meter {[1/s] /m}
acres	.4047	square hectometers (hm²)
acros	.004047	square kilometers (km²)
acre-feet	1,233.	cubic meters (m ³)
acre-feet	1.233 X 10 ⁻⁶	cubic kilometers (km ³)
million acre-feet	1.233	cubic kilometers (km ³)

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