TTI: 9-1002-12



MASH TEST 3-21 ON TL-3 THRIE BEAM TRANSITION WITHOUT CURB



Test Report 9-1002-12-3

Cooperative Research Program

TEXAS A&M TRANSPORTATION INSTITUTE COLLEGE STATION, TEXAS

in cooperation with the Federal Highway Administration and the Texas Department of Transportation http://tti.tamu.edu/documents/9-1002-12-3.pdf

		Technical Report Documentation Page
1. Report No. FHWA/TX-13/9-1002-12-3	2. Government Accession No.	3. Recipient's Catalog No.
4. Title and Subtitle		5. Report Date
MASH TEST 3-21 ON TL-3	THRIE BEAM	January 2013
TRANSITION WITHOUT	CURB	Published: July 2013
		6. Performing Organization Code
7. Author(s)		8. Performing Organization Report No.
Dusty R. Arrington, Roger P. Bligh	, and Wanda L. Menges	Test Report 9-1002-12-3
9. Performing Organization Name and Address		10. Work Unit No. (TRAIS)
Texas A&M Transportation Institut	ē	
College Station, Texas 77843-3135		11. Contract or Grant No.
no anno ann sainne airte	altere altere alter alter al	Project 9-1002-12
12. Sponsoring Agency Name and Address		13. Type of Report and Period Covered
Texas Department of Transportation		Test Report:
Research and Technology Implementation Office		September 2011–August 2012
P.O. Box 5080		14. Sponsoring Agency Code
Austin, Texas 78763-5080		
 Supplementary Notes Project performed in cooperation w Administration. 	ith the Texas Department of Transpo	rtation and the Federal Highway

Project Title: Roadside Safety Device Crash Testing Program

URL: http://tti.tamu.edu/documents/9-1002-12-3.pdf

16. Abstract

This project evaluated the impact performance of a modified TxDOT three beam transition to rigid concrete barrier without a curb element below the transition rail. In a previous test described in TxDOT Research Report 0-4564, a three beam transition without curb failed to meet *NCHRP Report 350* performance criteria. However, it could not be discerned whether the vehicle instability observed in that test was attributable to the missing curb or the rotation of the three beam transition rail into the sloped face of the concrete safety shape rail at the bridge end connection point.

A transition design without curb would reduce the complexity of the field installations and would provide an option for dealing with different drainage requirements at bridge ends. A fabricated steel blockout was incorporated into the transition system to keep the three beam rail and terminal connector in a vertical plane at its connection to the concrete bridge rail.

The modified thrie beam transition without curb failed to meet *MASH* TL-3 requirements due to rollover of the impacting vehicle. Further discussions as to the possible cause of the failure are described within the report.

17. Key Words		18. Distribution Statemer	at a second second	
Guardrails, Terminals, End Treatments, W-Beam, Thrie Beam, Longitudinal Barriers, Crash Testing,		No restrictions. This document is available to the public through NTIS:		
Roadside Safety		National Technical Information Service		
		Alexandria, Virg	inia 22312	
		http://www.ntis.g	gov	
19. Security Classif.(of this report) Unclassified	20. Security Classif.(of the Unclassified	his page)	21. No. of Pages 76	22. Price

Form DOT F 1700.7 (8-72)

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by

Dusty R. Arrington Engineering Research Associate Texas A&M Transportation Institute

Roger P. Bligh, P.E. Research Engineer Texas A&M Transportation Institute

and

Wanda L. Menges Research Specialist Texas A&M Transportation Institute

Test Report No. 9-1002-12-3 Project 9-1002-12 Project Title: Roadside Safety Device Crash Testing Program

> Performed in cooperation with the Texas Department of Transportation and the Federal Highway Administration

> > January 2013 Published: July 2013

TEXAS A&M TRANSPORTATION INSTITUTE College Station, Texas 77843-3135

DISCLAIMER

This research was performed in cooperation with the Texas Department of Transportation (TxDOT) and the Federal Highway Administration (FHWA). The contents of this report reflect the views of the authors, who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official view or policies of the FHWA or TxDOT. This report does not constitute a standard, specification, or regulation, and its contents are not intended for construction, bidding, or permit purposes. In addition, the above listed agencies assume no liability for its contents or use thereof. The United States Government and the State of Texas do not endorse products or manufacturers. Trade or manufacturers' names appear herein solely because they are considered essential to the object of this report. The engineer in charge of the project was Roger P. Bligh, P.E. (Texas, #78550).

TTI PROVING GROUND DISCLAIMER

The results of the crash testing reported herein apply only to the article being tested.



Wanda L. Menges, Research Specialist Deputy Quality Manager

Richard A. Zimmer, Senior Research Specialist Test Facility Manager Quality Manager Technical Manager

ACKNOWLEDGMENTS

This research project was conducted under a cooperative program between the Texas A&M Transportation Institute, the Texas Department of Transportation, and the Federal Highway Administration. The TxDOT project director for this research was Rory Meza (DES). John Holt (BRG) and Wade Odell (RTI) also contributed significantly to the project. The authors acknowledge and appreciate their guidance and assistance.

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CHAPTER 1. INTRODUCTION

1.1 INTRODUCTION

This project was set up to provide the Texas Department of Transportation (TxDOT) with a mechanism to quickly and effectively evaluate high-priority issues related to roadside safety devices. Roadside safety devices shield motorists from roadside hazards such as non-traversable terrain and fixed objects. To maintain the desired level of safety for the motoring public, these safety devices must be designed to accommodate a variety of site conditions, placement locations, and a changing vehicle fleet. Periodically, there is a need to assess the compliance of existing safety devices with current vehicle testing criteria and develop new devices that address identified needs.

Under this project, roadside safety issues are identified and prioritized for investigation. Each roadside safety issue is addressed with a separate work plan, and the results are summarized in individual test reports.

1.2 BACKGROUND

Current roadside safety barriers can be generalized into a two categories. The first category includes rigid barriers such as permanent concrete median barriers. The second category includes flexible barriers such as metal beam guard fence. These barriers are highly effective in redirecting errant vehicles; however, they have significantly different deflection characteristics. Approach guardrail is often attached to a bridge rail to shield motorists from hazards at the bridge end and those underlying the bridge. A transition system is needed to transition the stiffness between the two systems to avoid impact performance issues such as pocketing and snagging on the rigid end of the bridge parapet.

In May 1998, Midwest Roadside Safety Facility (MwRSF) released a report detailing the design and testing of "Two Approach Guardrail Transitions for Concrete Safety Shape Barriers." This research was funded by the Midwest State's Regional Pooled Fund Program. The report details the design and testing of both steel and wood post options for transitioning W-beam guardrail to a concrete safety shape barrier. Two key features of these nested thrie beam transition designs include a curb under the transition rail near the concrete parapet end and a steel offset block that allows the thrie beam to be vertically connected to the sloped face of the concrete parapet without having to twist the thrie beam section. Both designs met National Cooperative Highway Research Program (NCHRP) *Report 350 (1)* evaluation criteria for Test Level 3 (TL-3).

In October 2003, TxDOT requested that Texas A&M Transportation Institute (TTI) evaluate a modified TL-3 nested thrie beam transition. The first modification was to eliminate the curb from under the transition rail. Second, the fabricated steel offset block under the terminal connector was removed. Instead, the nested thrie beam and terminal connector was twisted to match and connect directly to the sloped face of the concrete safety shape parapet.

TxDOT requested these modifications to reduce fabrication and installation complexity and cost. The modified transition system failed to meet *NCHRP Report 350* TL-3 performance criteria. The impacting vehicle overturned as it exited the transition system. It could not be conclusively determined which modification contributed more to the vehicle instability.

The American Association of State Highway and Transportation Officials (AASHTO) published the *Manual for Assessing Safety Hardware (MASH)* in October 2009 (2). *MASH* supersedes *NCHRP Report 350* as the recommended guidance for the safety performance evaluation of roadside safety features. In October 2006, MwRSF published Research Report TRP-03-175-06. This report documents a successful *MASH* TL-3 crash test (Test Designation 3-21) on the original nested thrie beam transition design. This test was performed as part of NCHRP Project 22-14(2).

Subsequently, TxDOT requested that a *MASH* test be performed to evaluate the impact performance of a modified TxDOT thrie beam transition to rigid concrete barrier without a curb element below the transition rail. A transition design without curb would reduce the complexity of the field installations and would provide an option for dealing with different drainage requirements at bridge ends. The difference between the previous failed transition test and the proposed design is that a fabricated steel blockout was incorporated into the transition system to keep the thrie beam rail and terminal connector in a vertical plane at its connection to the concrete bridge rail.

1.3 OBJECTIVES/SCOPE OF RESEARCH

This project evaluated the impact performance of a modified transition design for approach W-beam guardrail to a rigid concrete bridge rail without a curb element beneath the transition rail. The test was performed in accordance with *MASH* guidelines following the impact conditions for Test Designation 3-21.

CHAPTER 2. SYSTEM DETAILS

2.1 TEST ARTICLE DESIGN AND CONSTRUCTION

A total installation length of 92 ft- $6\frac{3}{4}$ inch was installed to fully evaluate the bridge rail to metal beam guard fence transition according to *MASH* TL-3 impact conditions. A 16-ft single slope concrete bridge rail served as a surrogate bride rail parapet end condition. The remaining 76 ft- $6\frac{3}{4}$ inches was constructed of metal beam guard fence. This length includes a TL-3 approved terminal and the TL-3 transition itself. A generic overall diagram of the test installation can be found in Figures 2.1 and 2.2. A full set of shop/fabrication drawings can be found in Appendix A.

The surrogate bridge rail parapet was constructed according to TxDOT 36-inch single slope traffic rail (SSTR) bridge rail standards found on the TxDOT standards website (http://www.dot.state.tx.us). As the standard suggests, the barrier is a 36-inch tall wall with a 79 degree constant slope traffic face. The barrier is $7\frac{1}{2}$ inches wide at the top of the barrier and $14\frac{1}{2}$ inches wide at the bottom of the barrier at the end of the parapet. The barrier is cast atop an 18-inch thick moment slab designed to withstand a *MASH* TL-4 impact. The concrete used in constructing the parapet and moment slab met/exceeded TxDOT Class C (3600 psi) specifications. The barrier toe was chamfered at the end of the parapet. The chamfer was $13\frac{3}{8}$ inches tall and 36 inches long. A total of five 1-inch holes were cast into the parapet to allow for the attachment of the 10 gauge thrie-beam terminal end shoe (RTE01b) and a custom $\frac{1}{4}$ -inch thick adapter plate using five $\frac{7}{8}$ -inch A325 bolts.

The reinforcement in the parapet included the following according to TxDOT SSTR barrier standards. "S-bars" and "U-bars" are placed every 5 inches along the length of the parapet. A total of eight #4 bars (½-inch) were equally spaced along the face of the parapet. The 18-inch deck was reinforced with two distinct rebar mats each containing #5 bars spaced every 6 inches perpendicular to the parapet and #4 bars spaced every 9 inches parallel to the parapet. The first mat maintained a 3-inch cover from the bottom of the moment slab. The second mat maintained a 2-inch cover from the top of the moment slab.

The metal beam guard fence was constructed using a total of 19 posts that were numbered from 1 to 19 starting with the ET-2000 Terminal control release post (CRP) anchor post. Posts 1 and 2 were installed as part of the standard 31-inch ET-2000 Terminal. Posts 3 through 11 are installed as part of a standard 12 gauge W-Beam Guardrail (RWM04a). Each post in this section is a 72-inch long W6×8.5 SLP (PEW01) attached to the 12 gauge rail element using an 8-inch wood blockout. The posts in this section were placed at the mid-span of the guardrail (not at a splice). Between posts 11 and 13, a 10 gauge thrie beam to W-beam nonsymmetric transition segment is used and is supported by a 72-inch long W6×8.5 SLP. Between Post 13 and the end of the bridge parapet, a nested 12 gauge thrie beam (RTM02a) configuration is used and is supported by 84-inch long W6×8.5 posts with 6×8×18-inch wood blockouts. A 10 gauge thrie-beam end shoe (RTE01b) was used to connect the nested thrie beam to the $\frac{1}{4}$ -inch thick adapter plate.



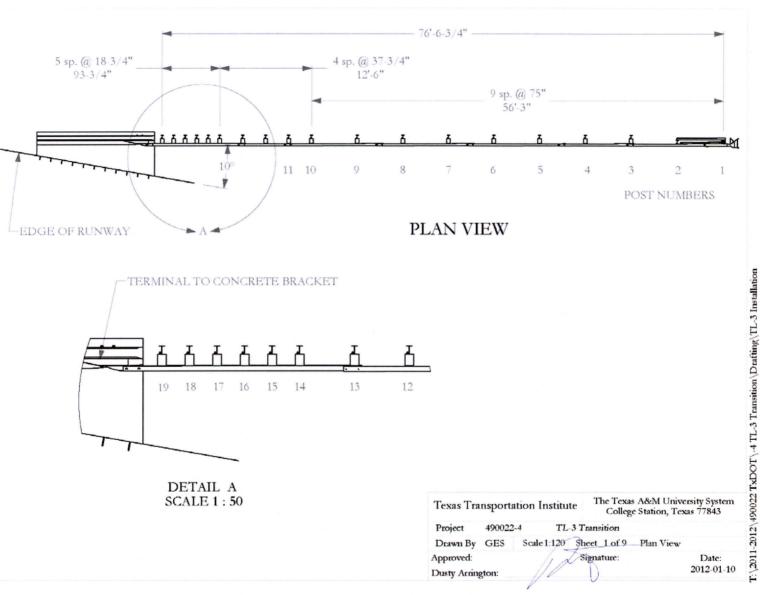


Figure 2.1. Layout of the TxDOT TL-3 Transition.

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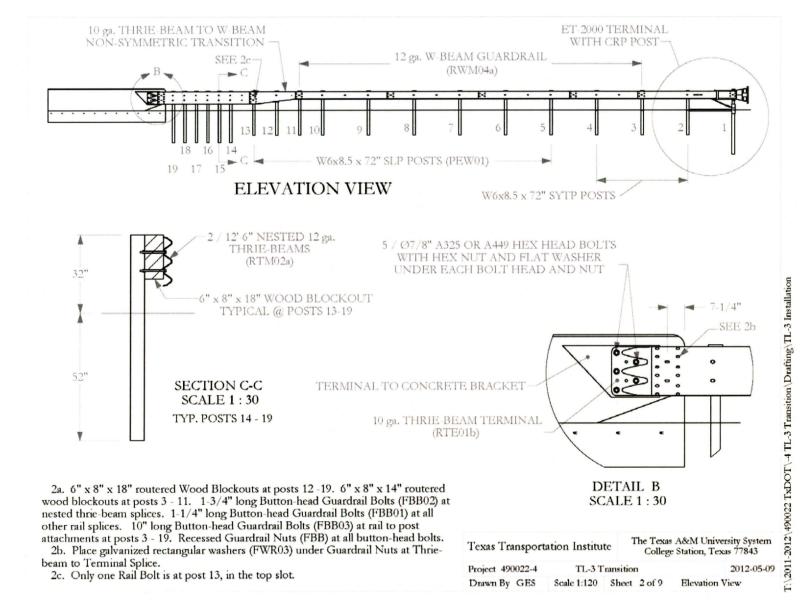


Figure 2.2. Details of the TxDOT TL-3 Transition.

TR No. 9-1002-12-4



Figure 2.3. TxDOT TL-3 Transition Installation before Test No. 490022-4.

The adapter plate is constructed using ¹/₄-inch steel plate. The adapter is 21 inches tall and 40 inches wide. The adapter plate allows for a 4-inch blockout at the top of the plate and tapers down to a 0-inch blockout distance. Quarter-inch thick stiffener plates are then welded to the back of the plate to stiffen the plate.

2.2 MATERIAL SPECIFICATIONS

As discussed in section 2.1, the concrete used to construct the concrete parapet meets/exceeds TxDOT Class C (3600 psi) specifications. All steel plates and structural members meet A36 material specifications. All standard American Road and Transportation Builders Association (ARTBA) parts meet/exceed material specifications associated with their assigned classification numbers.

2.3 SOIL CONDITIONS

The TxDOT TL-3 Transition was installed in standard soil meeting AASHTO standard specifications for "Materials for Aggregate and Soil Aggregate Subbase, Base and Surface Courses," designated M147-65(2004), grading B.

In accordance with Appendix B of *MASH*, soil strength was measured the day of the crash test (see Appendix C, Figure C1). During installation of the TxDOT TL-3 Transition for full-scale crash testing, two standard W6×16 posts were installed in the immediate vicinity of the TxDOT TL-3 Transition, utilizing the same fill materials and installation procedures used in the standard dynamic test (see Appendix C, Figure C2).

As determined in the tests shown in Appendix C, Figure C2, the minimum post load required for deflections at 5 inches, 10 inches, and 15 inches, measured at a height of 25 inches, is 3940 lb, 5500 lb, and 6540 lb, respectively (90 percent of static load for the initial standard installation). On the day of the test, April 14, 2009, load on the post at deflections of 5 inches, 10 inches, and 15 inches was 8121 lbf, 7303 lbf, and 6909 lbf, respectively. The strength of the backfill material met minimum requirements.

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CHAPTER 3. TEST REQUIREMENTS AND EVALUATION CRITERIA

3.1 CRASH TEST MATRIX

According to *MASH*, two tests are recommended to evaluate transitions to test level three (TL-3).

MASH Test Designation 3-20: A 2425-lb vehicle impacting the critical impact point (CIP) of the length of need (LON) of the barrier at a nominal impact speed and angle of 62 mi/h and 25 degrees, respectively. This test investigates a barrier's ability to successfully contain and redirect a small passenger vehicle.

MASH Test Designation 3-21: A 5000-lb pickup truck impacting the CIP of the LON of the barrier at a nominal impact speed and angle of 62 mi/h and 25 degrees, respectively. This test investigates a barrier's ability to successfully contain and redirect light trucks and sport utility vehicles.

Based on the geometry and strength of the transition design, the project team concluded that Test 3-20 was not warranted. The test reported here corresponds to Test 3-21 of *MASH* (5000-lb pickup, 62 mi/h, 25 degrees).

The crash test and data analysis procedures were in accordance with guidelines presented in *MASH*. Chapter 4 presents brief descriptions of these procedures.

3.2 EVALUATION CRITERIA

The crash test was evaluated in accordance with the criteria presented in *MASH*. The performance of the TxDOT TL-3 Transition is judged on the basis of three factors: structural adequacy, occupant risk, and post impact vehicle trajectory. Structural adequacy is judged upon the ability of the TxDOT TL-3 Transition to contain and redirect the vehicle, or bring the vehicle to a controlled stop in a predictable manner. Occupant risk criteria evaluate the potential risk of hazard to occupants in the impacting vehicle, and to some extent, other traffic, pedestrians, or workers in construction zones, if applicable. Post-impact vehicle trajectory is assessed to determine potential for secondary impact with other vehicles or fixed objects, creating further risk of injury to occupants of the impacting vehicle and/or risk of injury to occupants in other vehicles. The appropriate safety evaluation criteria from Table 5-1 of *MASH* were used to evaluate the crash test reported here and are listed in further detail under the assessment of the crash test.

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CHAPTER 4. CRASH TEST PROCEDURES

4.1 TEST FACILITY

The full-scale crash test reported here was performed at Texas A&M Transportation Institute Proving Ground, an International Standards Organization (ISO) 17025 accredited laboratory with American Association for Laboratory Accreditation (A2LA) Mechanical Testing certificate 2821.01. The full-scale crash test was performed according to TTI Proving Ground quality procedures and according to the *MASH* guidelines and standards.

The Texas A&M Transportation Institute Proving Ground is a 2000-acre complex of research and training facilities located 10 miles northwest of the main campus of Texas A&M University. The site, formerly an Air Force base, has large expanses of concrete runways and parking aprons well-suited for experimental research and testing in the areas of vehicle performance and handling, vehicle-roadway interaction, durability and efficacy of highway pavements, and safety evaluation of roadside safety hardware. The site selected for construction and testing of the T131RC Bridge Rail evaluated under this project was along the edge of an out-of-service apron. The apron consists of an unreinforced jointed-concrete pavement in 12.5 ft \times 15 ft blocks nominally 6 inches deep. The apron is over 60 years old, and the joints have some displacement, but are otherwise flat and level.

4.2 VEHICLE TOW AND GUIDANCE PROCEDURES

The test vehicle was towed into the test installation using a steel cable guidance and reverse tow system. A steel cable for guiding the test vehicle was tensioned along the path, anchored at each end, and threaded through an attachment to the front wheel of the test vehicle. An additional steel cable was connected to the test vehicle, passed around a pulley near the impact point, through a pulley on the tow vehicle, and then anchored to the ground such that the tow vehicle moved away from the test site. A 2:1 speed ratio between the test and tow vehicle existed with this system. Just prior to impact with the installation, the test vehicle was released to be unrestrained. The vehicle remained free-wheeling (i.e., no steering or braking inputs) until it cleared the immediate area of the test site, after which the brakes were activated to bring it to a safe and controlled stop.

4.3 DATA ACQUISITION SYSTEMS

4.3.1 Vehicle Instrumentation and Data Processing

The test vehicle was instrumented with a self-contained, on-board data acquisition system. The signal conditioning and acquisition system is a 16-channel, Tiny Data Acquisition System (TDAS) Pro produced by Diversified Technical Systems, Inc. The accelerometers that measure the x, y, and z axis of vehicle acceleration are strain gauge type with linear millivolt output proportional to acceleration. Angular rate sensors measuring vehicle roll, pitch, and yaw rates are ultra-small size, solid state units designed for crash test service. The TDAS Pro hardware and software conform to the latest SAE J211, Instrumentation for Impact Test. Each of the 16 channels is capable of providing precision amplification, scaling, and filtering based on transducer specifications and calibrations. During the test, data are recorded from each channel at a rate of 10,000 values per second with a resolution of one part in 65,536. Once the data are recorded, internal batteries back these up inside the unit should the primary battery cable be severed. Initial contact of the pressure switch on the vehicle bumper provides a time zero mark and initiates the recording process. After each test, the data are downloaded from the TDAS Pro unit into a laptop computer at the test site. The Test Risk Assessment Program (TRAP) software then processes the raw data to produce detailed reports of the test results. Each of the TDAS Pro units are returned to the factory annually for complete recalibration. Accelerometers and rate transducers are also calibrated annually with traceability to the National Institute for Standards and Technology.

TRAP uses the data from the TDAS Pro to compute occupant/compartment impact velocities, time of occupant/compartment impact after vehicle impact, and the highest 10-millisecond (ms) average ridedown acceleration. TRAP calculates change in vehicle velocity at the end of a given impulse period. In addition, the program computes the maximum average accelerations over 50-ms intervals in each of the three directions. For reporting purposes, the data from the vehicle-mounted accelerometers are filtered with a 60-Hz digital filter, and acceleration versus time curves for the longitudinal, lateral, and vertical directions are plotted using TRAP.

TRAP uses the data from the yaw, pitch, and roll rate transducers to compute angular displacement in degrees at 0.0001-s intervals and then plots yaw, pitch, and roll versus time. These displacements are in reference to the vehicle-fixed coordinate system with the initial position and orientation of the vehicle-fixed coordinate systems being initial impact.

4.3.2 Anthropomorphic Dummy Instrumentation

According to *MASH*, the use of a dummy in the 2270P vehicle is optional. Researchers did not use any dummy in the test with the 2270P vehicle.

4.3.3 Photographic Instrumentation and Data Processing

Photographic coverage of the test included three high-speed cameras: one overhead with a field of view perpendicular to the ground and directly over the impact point; one placed behind the installation at an angle; and a third placed to have a field of view parallel to and aligned with the installation at the downstream end. A flashbulb activated by pressure-sensitive tape switches was positioned on the impacting vehicle to indicate the instant of contact with the installation and was visible from each camera. The films from these high-speed cameras were analyzed on a computer-linked motion analyzer to observe phenomena occurring during the collision and to obtain time-event, displacement, and angular data. A mini-DV camera and still cameras recorded and documented conditions of the test vehicle and installation before and after the test.

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CHAPTER 5. CRASH TEST RESULTS

5.1 TEST DESIGNATION AND ACTUAL IMPACT CONDITIONS

MASH Test 3-21 involves a 2270P vehicle weighing 5000 lb ±100 lb and impacting the bridge rail transition at an impact speed of 62.2 mi/h ±2.5 mi/h and an angle of 25 degrees ±1.5 degrees. The target impact point of 93 inches upstream of concrete parapet was determined through Barrier VII simulations and the tables found within *MASH* for determining CIP. The 2006 Dodge Ram 1500 pickup truck used in the test weighed 5002 lb and the actual impact speed and angle were 62.6 mi/h and 23.9 degrees, respectively. The actual impact point was 89.0 inches upstream of the concrete parapet. Target impact severity (IS) was calculated at 115.1 kip*ft, and actual IS was calculated at 107.6 kip*ft, which was 6.5 percent less than target IS (acceptable limit for IS is not less than 8 percent of target IS).

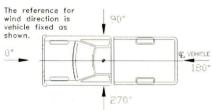
5.2 TEST VEHICLE

A 2006 Dodge Ram 1500 pickup truck, shown in Figure 5.1, was used for the crash test. Test inertia weight of the vehicle was 5002 lb, and its gross static weight was 5002 lb. The height to the lower edge of the vehicle bumper was 13.7 inches, and it was 25.38 inches to the upper edge of the bumper. Tables D1 and D2 in Appendix D give additional dimensions and information on the vehicle. The vehicle was directed into the installation using the cable reverse tow and guidance system, and was released to be unrestrained just prior to impact.

5.3 WEATHER CONDITIONS

The test was performed on the morning of May 14, 2012. Weather conditions at the time of testing were: wind speed: 2 mi/h; wind direction: 206 degrees with respect to the vehicle (vehicle was traveling

in a southwesterly direction); temperature: 80°F, relative humidity: 58 percent.



5.4 TEST DESCRIPTION

The 2006 Dodge Ram 1500 pickup truck, traveling at an impact speed of 62.6 mi/h, impacted the TxDOT TL-3 Transition 89.0 inches upstream of the concrete parapet at an impact angle of 23.9 degrees. At 0.010 s after impact, the vehicle began to redirect, and at 0.012 s, the thrie-beam guardrail and posts on either side of impact began to deflect toward the field side. The right front tire contacted the concrete parapet at 0.101 s, and the right front tire and wheel rim separated from the vehicle. At 0.168 s, the vehicle was traveling parallel with the transition at a speed of 52.7 mi/h. The rear of the vehicle contacted the transition at 0.176 s. At 0.316 s, the vehicle lost contact with the transition and was traveling at an exit speed and angle of 52.3 mi/h and 16.2 degrees. As the vehicle exited the transition, it rolled onto its right side and came to rest 208.4 ft downstream of impact and 75.0 ft toward traffic lanes. Figures E1 and E2 in Appendix E show sequential photographs of the test period.



Figure 5.1. Vehicle before Test No. 490022-4.

5.5 DAMAGE TO TEST INSTALLATION

Figures 5.2 and 5.3 show damage to the TxDOT TL-3 Transition. The soil was disturbed around post 1 and posts 10 through 12. Post 13 was leaning toward the field side and downstream 0.5 degree (from upright), and there was a gap of 0.25 inch between the edge of the soil and the traffic side of the post. Post 14 was deflected toward the field side 1.12 inches and was leaning 6 degrees toward the field side and 1 degree downstream. Post 15 was deflected toward the field side 1.62 inches and leaning toward field side 6 degrees and downstream 3 degrees. Post 16 was deflected toward the field side 2.0 inches and leaning toward the field side 5 degrees and downstream 7 degrees. Post 17 was deflected toward the field side 1.9 inches and was leaning toward the field side 4 degree and downstream 4 degrees. Post 18 was deflected toward the field side 1.5 inches and leaning toward the field side 5 degrees and downstream 3 degrees. Post 19 was deflected toward the field side 1.4 inches and leaning toward the field side 7 degrees and downstream 6 degrees. Maximum permanent deformation of the thrie beam rail element was 4.5 inches at the top ridge, 3.9 inches at the middle ridge, and 6.5 inches at the bottom ridge. Total length of contact of the vehicle with the thrie beam rail element was 149.0 inches. Working width was 22.8 inches and maximum dynamic deflection of the top of the rail element was 5.9 inches.

5.6 VEHICLE DAMAGE

As shown in Figure 5.4, the 2270P vehicle was damaged in the right front and right side. The right frame rail, right front upper and lower A-arms, right front upper and lower ball joints, and right outer tie rods were deformed. Also damaged were the front bumper, hood, grill, right front fender, right front tire and wheel rim, right front door and door glass, right rear door, right exterior bed, rear bumper, tailgate, and right rear wheel rim. Maximum exterior crush to the vehicle was 170.0 inches in the front plane at the right front corner at bumper height. Maximum occupant compartment deformation was 3.75 inches in the lateral area across the occupant compartment in the kickpanel area near the front passenger's feet. Figure 5.5 shows the occupant compartment before and after the test. Tables D3 and D4 of Appendix D present the exterior and interior crush measurement.

5.7 OCCUPANT RISK FACTORS

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk. In the longitudinal direction, the occupant impact velocity was 16.4 ft/s at 0.099 s, the highest 0.010-s occupant ridedown acceleration was 14.4 Gs from 0.114 to 0.124 s, and the maximum 0.050-s average acceleration was -8.9 Gs between 0.075 and 0.125 s. In the lateral direction, the occupant impact velocity was 27.6 ft/s at 0.099 s, the highest 0.010-s occupant ridedown acceleration was 9.0 Gs from 0.103 to 0.113 s, and the maximum 0.050-s average was -13.6 Gs between 0.043 and 0.093 s. Theoretical Head Impact Velocity (THIV) was 34.9 km/h or 9.7 m/s at 0.097 s; Post-Impact Head Decelerations (PHD) was 16.2 Gs between 0.114 and 0.124 s; and Acceleration Severity Index (ASI) was 1.63 between 0.044 and 0.094 s. Figure 5.6 summarizes these data and other pertinent information from the test. Vehicle angular displacements and accelerations versus time traces are presented in Appendix F, Figures F1 through F7.

TR No. 9-1002-12-4



Figure 5.2. TxDOT TL-3 Transition/Vehicle after Test No. 490022-4.



Figure 5.3. TxDOT TL-3 Transition after Test No. 490022-4.



Figure 5.4. Vehicle after Test No. 490022-4.

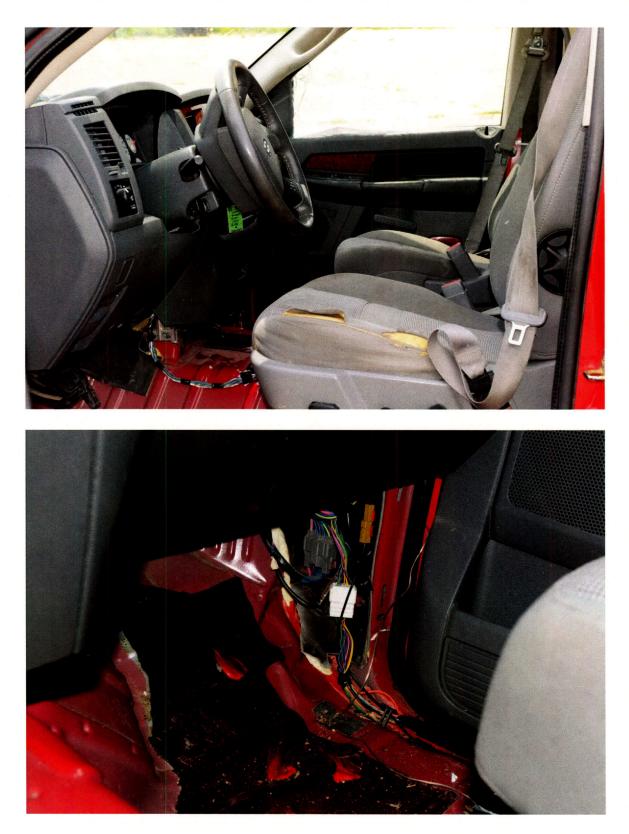
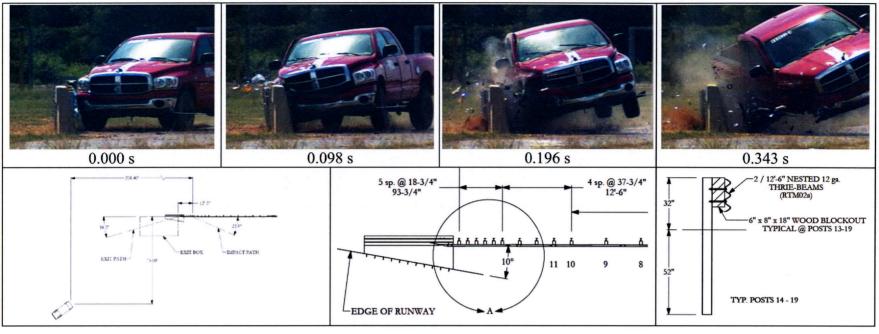


Figure 5.5. Interior of Vehicle after Test No. 490022-4.



General Information	
Test Agency Texas A&M Transportation Institu	ute (TTI)
Test Standard Test No MASH Test 3-21	. ,
TTI Test No 490022-4	
Test Date 2012-05-14	
Test Article	
Type Transition	
Name TxDOT TL-3 Transition	
Installation Length 92.5 ft	
Material or Key Elements Nested 10 gauge thrie beam gua	rdrail
on steel posts spaced at 18.75 in	ches
on center	
Soil Type and Condition Standard Soil, Dry	
Test Vehicle	
Type/Designation 2270P	
Make and Model 2006 Dodge Ram 1500	
Curb 5026 lb	
Test Inertial 5002 lb	
Dummy No dummy	
Gross Static 5002 lb	

Impact Conditions

impact conditions	
Speed	62.6 mi/h
Angle	23.9 degrees
Location/Orientation	89 inches upstrm
Exit Conditions	of parapet
Speed	
Angle	
Occupant Risk Values	J
Impact Velocity	
Longitudinal	16.4 ft/s
Lateral	
Ridedown Accelerations	6
Longitudinal	14.4 G
Lateral	
THIV	34.9 km/h
PHD	
ASI	1.63
Max. 0.050-s Average	
Longitudinal	8.9 G
Lateral	
Vertical	

Post-Impact Trajectory

m

Figure 5.6. Summary of Results for MASH Test 3-21 on the TxDOT TL-3 Transition.

CHAPTER 6. SUMMARY AND CONCLUSIONS

6.1 ASSESSMENT OF TEST RESULTS

An assessment of the test based on the applicable *MASH* safety evaluation criteria is provided below.

6.1.1 Structural Adequacy

- A. Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.
- <u>Results</u>: The TxDOT TL-3 Transition contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection of the metal rail element was 7.9 inches. (PASS)

6.1.2 Occupant Risk

D. Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.

Deformation of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH. (roof ≤ 4.0 inches; windshield = ≤ 3.0 inches; side windows = no shattering by test article structural member; wheel/foot well/toe pan ≤ 9.0 inches; forward of A-pillar ≤ 12.0 inches; front side door area above seat ≤ 9.0 inches; front side door below seat ≤ 12.0 inches; floor pan/transmission tunnel area ≤ 12.0 inches)

- <u>Results</u>: No detached elements, fragments, or other debris was present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area. (PASS) Maximum occupant compartment deformation was 3.75 inches in the lateral area across the occupant compartment in the kickpanel area near the front passenger's feet. (PASS)
- *F.* The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.
- <u>Results</u>: The 2270P vehicle rolled 90 degrees onto its right side after exiting the transition. (FAIL)

Occupant impact velocities should satisfy the following: Longitudinal and Lateral Occupant Impact Velocity <u>Preferred</u> 30 ft/s 40 ft/s

<u>Results</u>: Longitudinal occupant impact velocity was 16.4 ft/s, and lateral occupant impact velocity was 27.6 ft/s. (PASS)

I. Occupant ridedown accelerations should satisfy the following: <u>Longitudinal and Lateral Occupant Ridedown Accelerations</u> <u>Preferred</u> <u>Maximum</u> 15.0 Gs 20.49 Gs

<u>Results</u>: Longitudinal ridedown acceleration was 14.4 G, and lateral ridedown acceleration was 9.0 G. (PASS)

6.1.3 Vehicle Trajectory

H.

For redirective devices, the vehicle shall exit the barrier within the exit box. Report vehicle rebound distance and velocity for crash cushions.

<u>Result</u>: The 2270P vehicle exited within the exit box. (PASS)

6.2 CONCLUSIONS

The TxDOT TL-3 Transition did not perform acceptably for *MASH* test 3-21 due to vehicle rollover (see Table 6.1). There were indications of wheel snagging on the end of the concrete parapet that may have contributed to destabilization of the vehicle.

6.3 **RECOMMENDATIONS***

The researchers suggest that the following are possible design changes may improve the performance of the system. First, a short curb may be placed at the end of the parapet under the rail to help prevent the wheel snagging. This is consistent with previous design details; however, the researchers feel the length may be reduced to help with the draining problems that prompted this test. Second, the steel blockout at the end of the parapet could be increased in depth to offset the rail to decrease the amount of snagging. Finally, the posts in the nested section of the guardrail could be strengthened by using a larger size post and increasing the embedment depth. This would serve to further stiffen the transition and reduce dynamic deflection. Some previous studies suggest that excessive deflection in the transition region can induce vehicle instability. However, if the system becomes too stiff, the upstream end of the transition section may need to be redesigned and evaluated. Further development, analysis, and full-scale crash testing would be required to evaluate any of these proposed modifications.

^{*} TTI Proving Ground's A2LA scope of accreditation does not cover recommendations. These recommendations were provided by the engineering research team.

Te	est Agency: Texas A&M Transportation Institute		Test Date: 2012-05-14
	MASH Test 3-21 Evaluation Criteria	Test Results	Assessment
<u>St</u> A.	<u>ructural Adequacy</u> Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable	The TxDOT TL-3 Transition contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection of the metal rail element was 7.9 inches.	Pass
	ccupant Risk Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.	No detached elements, fragments, or other debris was present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area.	Pass
	Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH.	Maximum occupant compartment deformation was 3.75 inches in the lateral area across the occupant compartment in the kickpanel area near the front passenger's feet.	Pass
F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.	The 2270P vehicle rolled 90 degrees onto its right side after exiting the transition.	Fail
H.	Longitudinal and lateral occupant impact velocities should fall below the preferred value of 30 ft/s, or at least below the maximum allowable value of 40 ft/s.	Longitudinal occupant impact velocity was 16.4 ft/s, and lateral occupant impact velocity was 27.6 ft/s.	Pass
Ι.	Longitudinal and lateral occupant ridedown accelerations should fall below the preferred value of 15.0 Gs, or at least below the maximum allowable value of 20.49 Gs.	Longitudinal ridedown acceleration was 14.4 G, and lateral ridedown acceleration was 9.0 G.	Pass
<u>V</u> e	<u>ehicle Trajectory</u> For redirective devices, the vehicle shall exit the barrier within the exit box (not less than 32.8 ft).	The 2270P vehicle exited within the exit box.	Pass

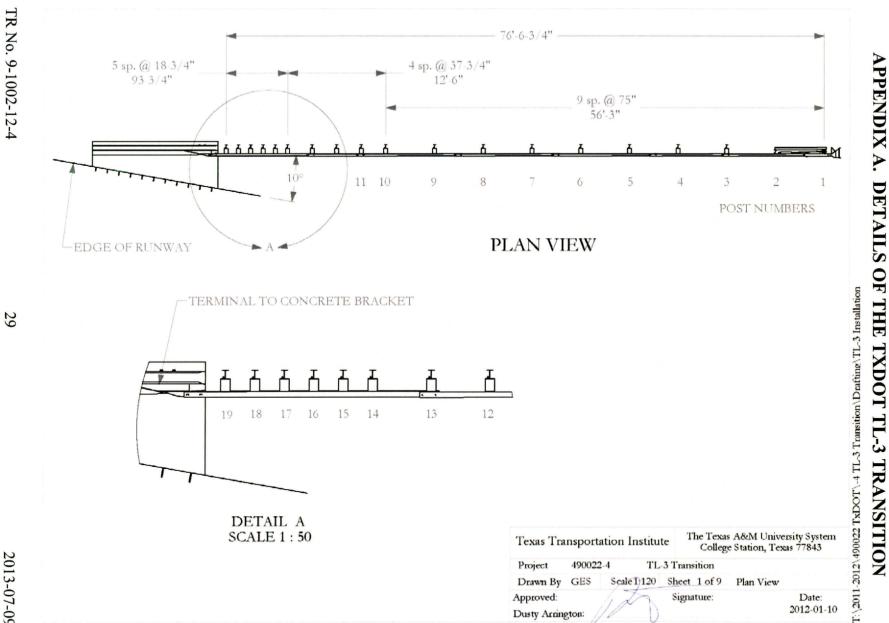
Table 6.1. Performance Evaluation Summary for MASH Test 3-21 on the TxDOT TL-3 Transition.

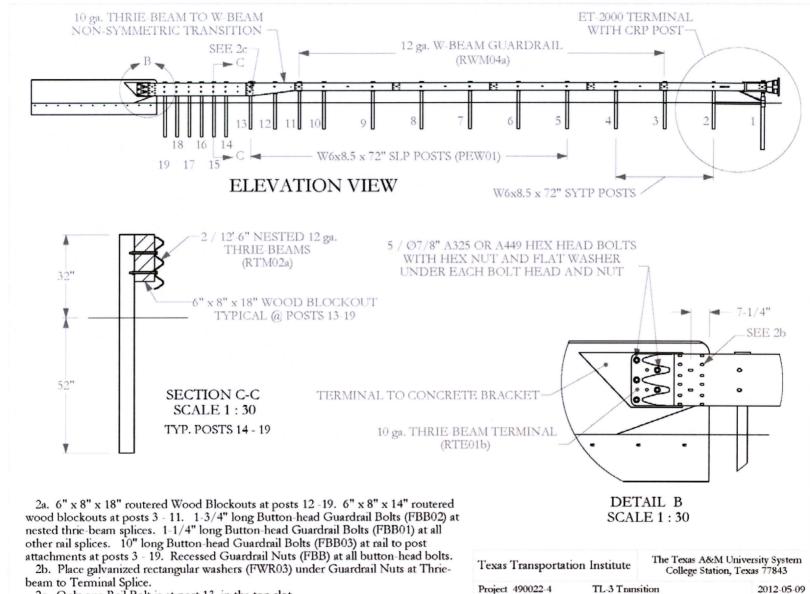
CHAPTER 7. IMPLEMENTATION STATEMENT

The modified transition system without curb did not meet the impact performance requirements of MASH. Consequently, no implementation is recommended at this time. Several possible design modifications are presented to mitigate the vehicle instability observed in the test. One or more if these modifications can be analyzed and evaluated at the discretion of TxDOT.

REFERENCES

- 1. H. E. Ross, D. L. Sicking, R. A. Zimmer, and J. D. Michie. "Recommended Procedures for the Safety Performance Evaluation." *NCHRP Report 350*. National Academy Press, Washington, D.C., National Cooperative Highway Research Program, 1993.
- 2. AASHTO, *Manual for Assessing Safety Hardware*, American Association of State Highway and Transportation Officials, Washington, D.C., 2009.





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Scale 1:120 Sheet 2 of 9

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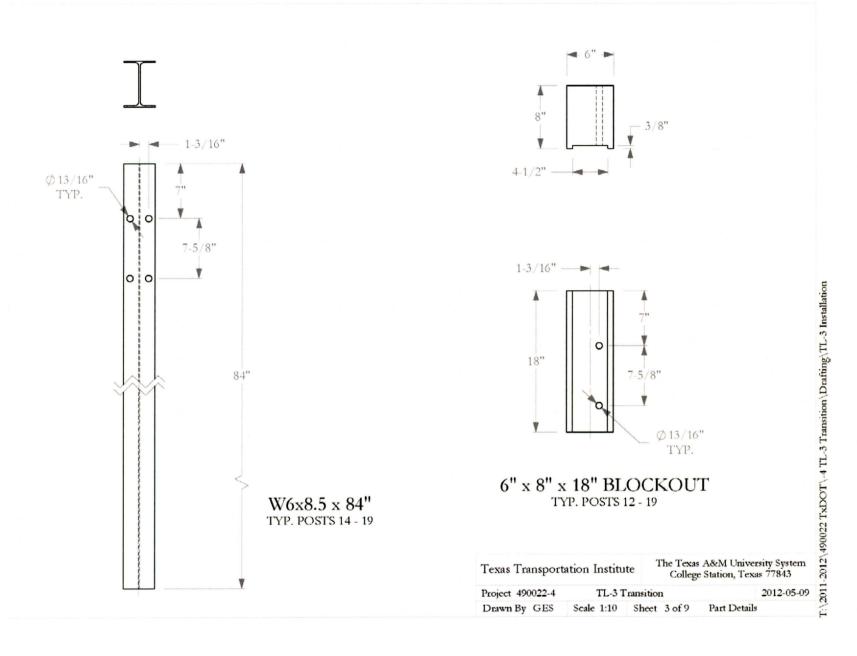
Elevation View

2c. Only one Rail Bolt is at post 13, in the top slot.

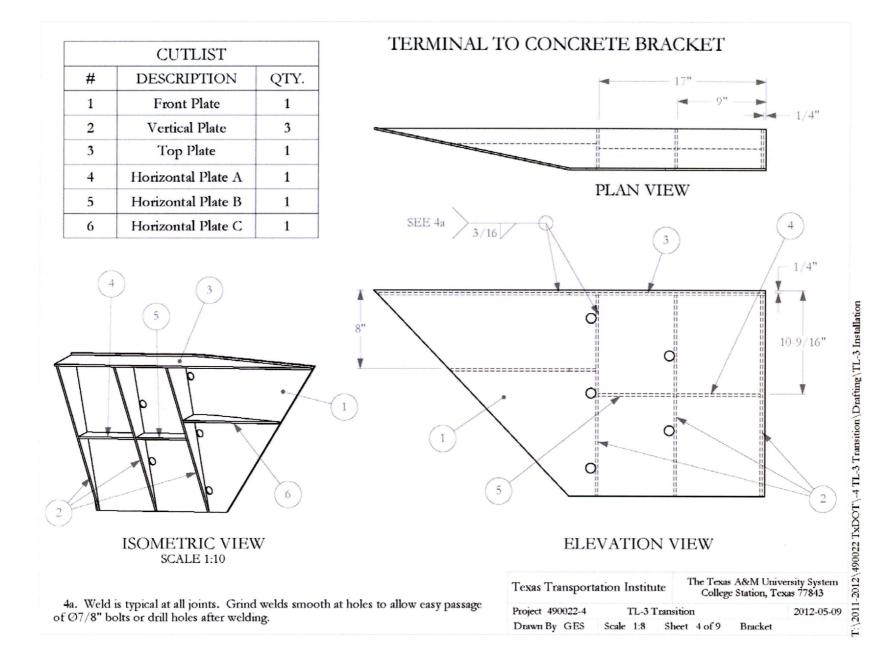
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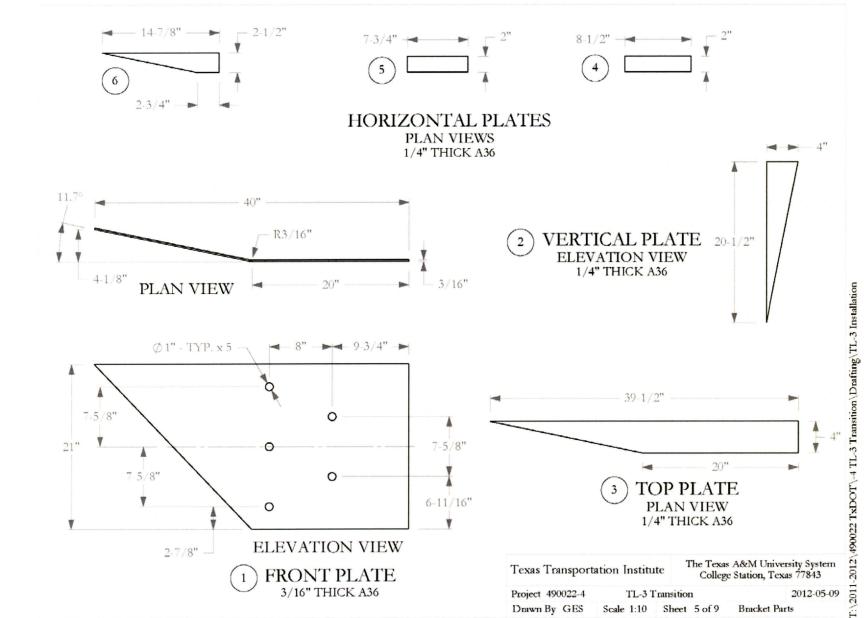
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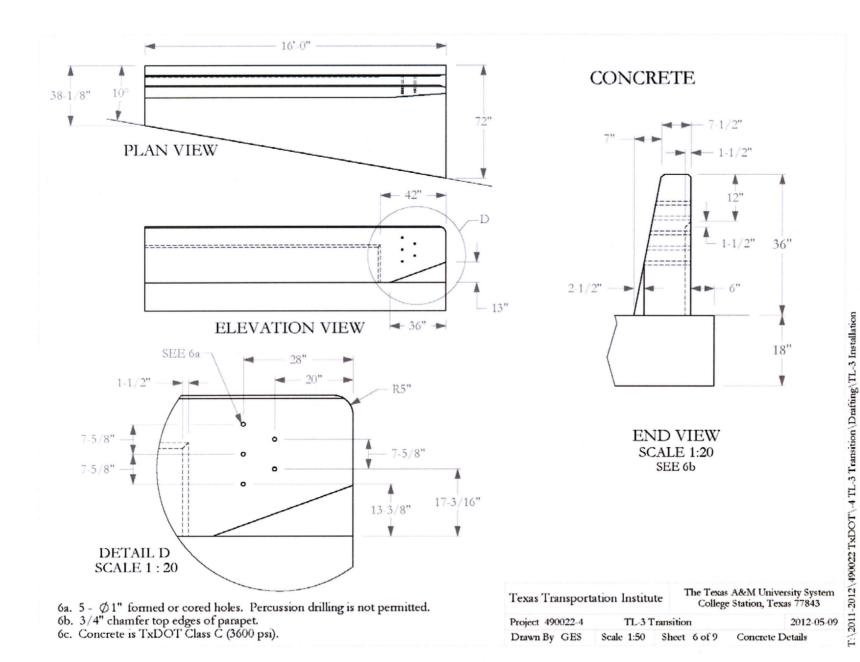
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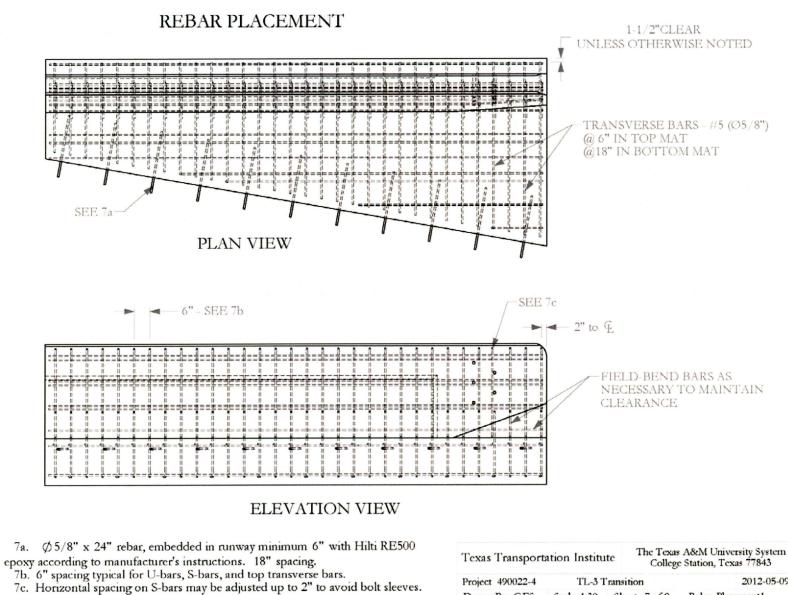




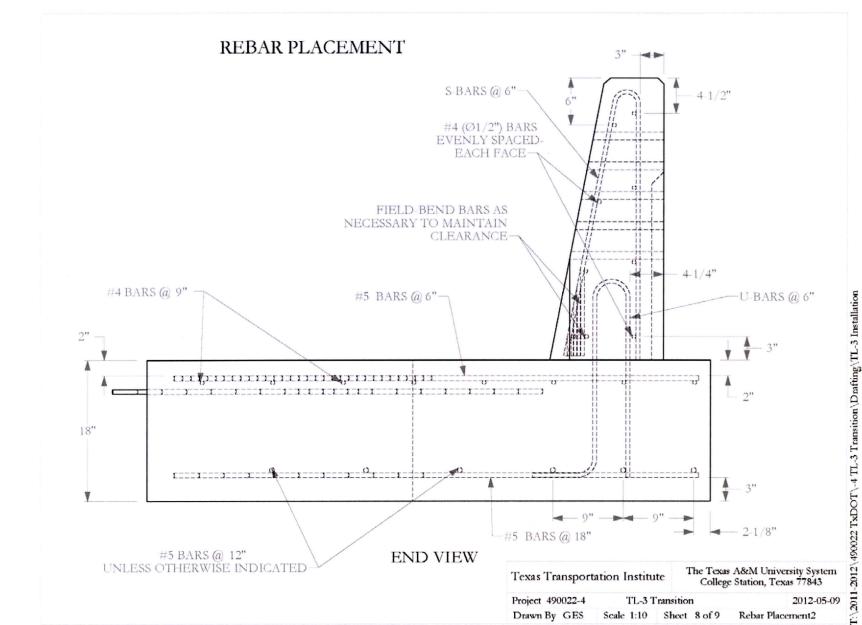
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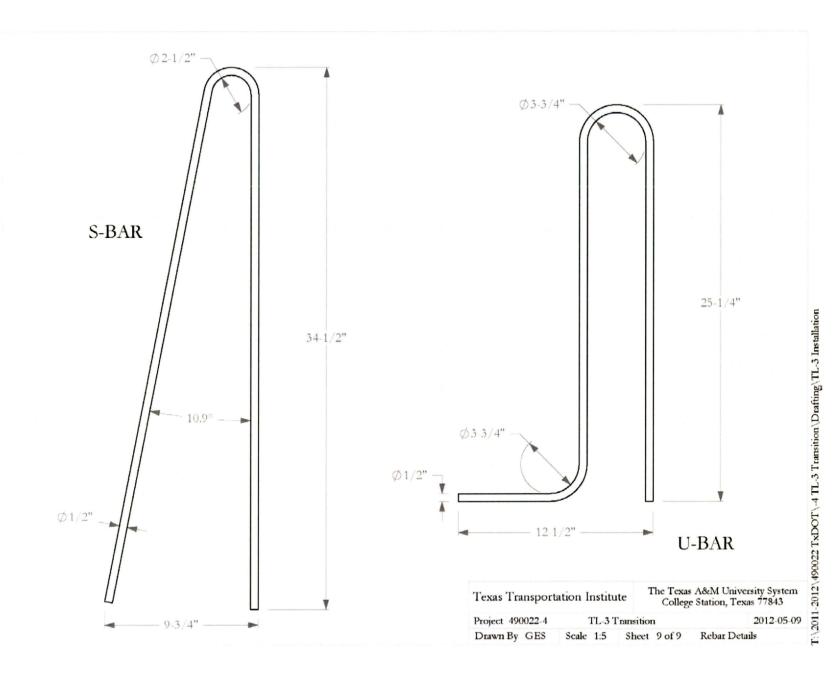


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TR No. 9-1002-12-4

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APPENDIX B. CERTIFICATION DOCUMENTATION

MATERIAL USED

TEST NUMBER 490022-4

TEST NAME TL-3 Transition

DATE 2012-05-14

DATE RECEIVED	ITEM NUMBER	DESCRIPTION	SUPPLIER	HEAT #
2012-02-08 2012-02-23	Parts-16 Rebar 04-26	Guardrail Parts 1/2" x 20' gr 60	Trinity CMC-Sheplers	see file 3029770
2012-02-23	Rebar 05-15	5/8" x 20' grd 60	CMC-Sheplers	3028494

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AGENT CE This Stiched and we without to product and		SIGNHERE		1974 Auf	EIA.	
SIGN HERE AGENT CR This shipher incrues subject to exceptions a DRIVET terms and conditions hered. (SIGN HERE)	a noted and eccording to the	SIGN HERE	DATE	TIME	EII.	

(This Bit of Lading is to be signed by the shipper and agent of the carrier issuing asmo.)

CONSIGNEE/CUSTOMER COPY

¢

Customer: SAMPLES, TESTING, TRAINING MTRLS 2525 STEMMONS FRWY

Sales Order: 1164772 Customer PO: TTI-ET 2000 BOL # 40479 Document # 1



Print Date: 2/7/12 Project: SAMPLES & TESTING TT1 ET-2000 GILCHRIST/SHI Shipped To: TX Use State: TX

DALLAS, TX 75207

Trinity Highway Products. LLC

Certificate Of Compliance For Trinity Industries, Inc. ** E.T. PLUS EXTRUDER TERMINAL **

NCHRP Report 350 Compliant

Pieces	Description	 	 Part N						
2	12/12'6/6'3/S ET2000 ANC								0000320
2	CABLE ANCHOR BRKT ET-2000								0007044
2	CBL 3/4X6'6/DBL SWG/NOHWD								0030000
22	5/8" GR HEX NUT								0033400
18	5/8"X1.25" GR BOLT								0033600
4	5/8"X10" GR BOLT A307								0035000
4	3/4" ROUND WASHER F436								0037010
4	3/4" HVY HEX NUT A563 DH								0037040
4	3/4"X2.5" HEX BOLT A325								0037170
4	1" ROUND WASHER F844								0039000
4	1" HEX NUT A563								0039100
4	WD BLK RTD 6X8X14								0040761
8	3/8" ROUND WASHER F436								0042540
4	3/8" FENDER WASHER F844								0042550
4	3/8" LOCK WASHER								0042580
4	3/8"X1.5" HEX BOLT GR-5								0042610
4	7/16" WASHER F844								0043890
4	7/16"X1.5" HEX BOLT GRD 5								0043900
4	7/16" LOCK WASHER								0043930
4	7/16" HEX NUT A563 DH								004396
4	3/4" LOCK WASHER								0046990
4	3/8"X2" HEX BOLT GR-5 HDG								0063210
8	3/8" HVY HEX NUT A563GRDH								0064050
2	12/9'4.5/3'1.5/S								0109670
6	6'0 SYT PST/8.5/31" GR HT								015000
2	HBA-BRG PL/WELDED TABS								019258
4	.135(10Ga)X1.75X1.75 WSHR								019948
2	SYT-3"AN STRT 3-HL 6'6								0337950
2	DI I-J AN DIRI J-NG 00								055795

1 of 2

TR No. 9-1002-12-4

Trinity Highway Products , LLC 2548 N.E. 28th St. Ft Worth, TX 76111

Customer: SAMPLES, TESTING, TRAINING MTRLS 2525 STEMMONS FRWY
 Sales Order:
 1164772

 Customer PO:
 TTI-ET 2000

 BOL #
 40479

 Document #
 1

Print Date: 2/7/12 Project: SAMPLES & TESTING TTI ET-2000 GILCHRIST/SHI Shipped To: TX Use State: TX

DALLAS, TX 75207

Trinity Highway Products, LLC

Certificate Of Compliance For Trinity Industries, Inc. ** E.T. PLUS EXTRUDER TERMINAL **

NCHRP Report 350 Compliant

Upon delivery, all materials subject to Trinity Highway Products, LLC Storage Stain Policy No. LG-002.

TL -3 or TL-4 COMPLIANT when installed according to manufactures specifications

ALL STEEL USED WAS MELTED AND MANUFACTURED IN USA AND COMPLIES WITH THE BUY AMERICA ACT

ALL GUARDRAIL MEETS AASHTO M-180, ALL STRUCTURAL STEEL MEETS ASTM A36

ALL COATINGS PROCESSES OF THE STEEL OR IRON ARE PERFORMED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT"

ALL GALVANIZED MATERIAL CONFORMS WITH ASTM-123, UNLESS OTHERWISE STATED.

BOLTS COMPLY WITH ASTM A-307 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED. NUTS COMPLY WITH ASTM A-563 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED. WASHERS COMPLY WITH ASTM F-436 SPECIFICATION AND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM F-2329. 3/4" DIA CABLE 6X19 ZINC COATED SWAGED END AISI C-1035 STEEL ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BREAKING STRENGTH - 49100 LB

State of Texas, County of Tarrant. Sworn and Subscribed before me this 7th day of February, 2012

Notary Public: Commission Expires:

JOMARY LUCINSLAND MY COMMISSION EXPIRES May 24, 2015

Certified By: Quality Assurance

Trinity Highway

forkery Jugenland

2 of 2

							Certif	ied Analy	sis						Time in the second seco	Way Produ	is to
	Trinity I	lighway l	Products, LLC						•		•		÷				7
	2548 N.E	. 28th St.					Ord	ler Number: 116471	5.								
	Ft Worth,						0	stomer PO: Samples									
								OL Number: 40480							Asof: 2/7/12		
	Custome		LES, TESTING, TRAININ	GMIRLS													
		2525 5	STEMMONS FRWY				··· (Document #: 1									
÷.							:	Shipped To: TX									
		DALL	AS, TX 75207					Use State: TX									
	Project:	SAM	LES & TESTING TRAIN	ING MTR	LS											·	
							· · · ·				• •		·····				
	· · ·															۰.	
	Qty		Description	Spec	CL		Heat Code/ Heat #	Yield	TS	Elg	C	Mn	P S	Si Cu	Cb Ci		ACW
	6	110	12/12'6/3'1.5/S	A-500 M-180		2	202248	53,600	75,500 73,300					0.120 0.120			4
· .				M-180 M-180	A	2	101800	50,000	73,300					0.020 0.120			
				M-180 M-180	A	2	101802	54,500	75,800					0.020 0.120			
				M-180	A	2	102475	58,700	79,800					0.007 0.130			
			, · · ·	M-180	A	2	102476	58,100	77,900					0.020 0.130			
				M-180	A	2	202249	51,800	74,500					0.020 0.120			
				M-180		2	202250	54,100	76,100					0.020 0.120			
				M-180	A	2	202938	57,600	80,400					0.020 0.130			
				M-180	A	2	202939	56,800	78,400	25.0	0.190	0.770 0.	.009 0.004	0.020 0.13	0.000 0.05	0 0.003	4
	14	533G	6'0 POST/8.5/DDR	A-36		•	1017017	53,642	71,899	26.8	0.110 0.	.960 0.0	08 0.038	0.180 0.260	0.00 0.090	0.004	4
			· · ·				1017007	CD CLD			A 140 A			A 100 0			
		533G		A-36			1017007	53,613	72,244	25.7	U.120 ° 0.	.930 0.0	12 0.040	0.180 0.360	0.00 0.140	0.003	4
		533G		A-36			1016666	56,666	73,288	29.7	0.110 0.	.940 0.0	13 0.037	0.190 0.320	0.00 0.15	0.004	4
					1											•	
		533G		A-36	*		1017003	55,742	71,204	24.3	0.100_0	.950 0.0	14 0.046	0.180 0.300	0.00 0.16	0.004	4
							105045	50 100	66 100	21.0		670 A -	10 0 00-	0.030 0			
	:	980G	TI0/END SHOE/SLANT	A-36			125745	58,100	66,100	31.9	0.050_0	.570 0.0	12 0.003	0.030 0.100	0.01 0.05	0.000	4
		12227G	T12/12'6/3'1.5:6@1'6.75/S	M-180	A	2	150054	61,580	80,600	25.0	0.190 0	720 0.0	10 0.003	0.010 0.130	0.00 0.06	0.001	4
	, l	14784G	7'0 POST/8.5#/3HI TX	A-36			1014849	50,787	69,032	25.6	0.100 0	.960 0.0	15 0.037	0.180 0.310	0.00 0.18	0.003	4
							1014844	62.142	60.092			000 00	10 0000	0.100 0.222			
		14784G	i .	A-36			1014844	53,141	69,983	28.3	0.110 0	.900 0.0	0.037	0.180 0.330	0.00 0.11	U 0.003	4
· .		14784G	i i i i i i i i i i i i i i i i i i i	A-36			1014840	57,069	73,001	30.4	0.110 0	.960 0.0	10 0.035	0.170 0.320	0.00 0.15	0.004	4

TR No. 9-1002-12-4

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2013-07-09

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						Certifie	d Anal	ysis									Highw	ay Prod	is.E
uity Hi	ghway P	roducts, LLC																	
8 N.E.	28th St.					Order N	lumber: 1164	715											
/orth, T	X 76111					Custor	mer PO: Samp	les							А	sof:2	17/12		
tomer:	SAMPI	.ES,TESTING,TRAINING	3 MTRLS	5		BOLN	Number: 4048	0											
	2525 S	TEMMONS FRWY				Docu	iment #: 1												
						Ship	ped To: TX												
	DALLA	.S, TX 75207				Us	e State: TX												
ject:	SAMPI	LES & TESTING TRAINI	NG MTR	LS		·	· .											··	
		,			ту	Heat Code/ Heat #	Vield	TS	Ete	<u>с</u>	Mn	. P	<u> </u>	Si	 Cu			Vn	ACW
ject: Qty	Part #	LES & TESTING TRAIN	Spec	CL CL	тү		Yield	TS	Etg	С	Mn	P	s	Si	Си	Съ	Cr		ACW
		,			ТҰ	Heat Code/ Heat # 1014843	Yield 55,191	TS 72,737		C 0.110		. P 0.010	<u>s</u> 0.035						
Qty	Part #	,	Spec		тү				29.7		0.950			0.180	0.310	0.00	0.120	0.003	4
Qty 2	Part # 14784G	Description	Spec А-36		TY	1014843	55,191	72,737	29.7 26.7	0.110	0.950 0.970	0.012	0.032	0.180 0.180	0.310	0.00 0.00	0.120	0.003 0.004	4
Qty 2	Part # 14784G 14785G	Description 6'0 POST/8.5#/3111 TX	Spec A-36 A-36 A-36	CL	TY 2	1014843 1013730	55,191 50,597	72,737 70,003	29.7 26.7 29.7	0.110	0.950 0.970 0.950	0.012 0.010	0.032 0.035	0.180 0.180 0.180	0.310 0.270 0.310	0.00 0.00 0.00	0.120 0.140	0.003 0.004 0.003	4

Upon delivery, all materials subject to Trinity Highway Products, LLC Storage Stain Policy No. LG-002.

ALL STEEL USED WAS MELTED AND MANUFACTURED IN USA AND COMPLIES WITH THE BUY AMERICA ACT. ALL GUARDRAIL MEETS AASHTO M-180, ALL STRUCTURAL STEEL MEETS ASTM A36

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	· ·			(Cert	ified A	nalys	sis				in Highway Pro	aucis E
Trinity 1	Highway Products ,	LLC											
2548 N.	E. 28th St.				· · · (Order Number:	1164715				·		*
Ft Worth	, TX 76111					Customer PO:	Samples				As of:	27/12	
Custome	er: SAMPLES,TES	TING, TRAIND	IG MTRLS			BOL Number:	40480				A301.	2//112	
	2525 STEMMO	NS FRWY				Document #:	1				· · · ·		
		1			:	Shipped To:	TX						
	DALLAS, TX 752	107				Use State:	тх						
Project:	SAMPLES & TI	ESTING TRAD	VING MTRLS)		つ
State of	f Texas, County of Tar	rant. Sworn and s	ubscribed before m	e this 7th day	ofFebru	ary, 2012				Trinity High	ay Produce	HZ/	/
	ry Public:						· ,		Certified B	y: 1.	us C4	ng	
Commis	sion Expires: /	or Reven	MARY LUGINSLAND	7						Jual	ity Assurance	0	
· .		MY C	XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX						· .	•			
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3 of 3

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CMC STEEL TEXAS 1 STEEL MILL DRIVE SEGUIN TX 78155-7510 CERTIFIED MILL TEST REPORT For additional copies call 830-372-8771 We hereby certify that the test results presented here are accurate and conform to the reported grade specification

Aniel J. Schacht

Quality Assurance Manager

HEAT NO.:3029770	S	CMC Construction Svcs College Stati	S	CIMC Construction Svcs College Stati	Delivery#: 80681077
SECTION: REBAR 13MM (#4) 20'0"	0		H		BQL#: 70240462
420/60	L	10650 State Hwy 30	Ŧ	10650 State Hwy 30	CUST PO#: 53534v
GRADE: ASTM A615-09b Gr 420/60	D	College Station TX	P	College Station TX	CUST P/N:
ROLL DATE: 01/22/2012		US 77845-7950		US 77845-7950	DLVRY LBS / HEAT: 43820.000 LB
MELT DATE: 01/15/2012	т	979 774 5900	T	979 774 5900	DLVRY PCS / HEAT: 3280 EA
	0		0		

Characteristic	Value	Characteristic Value	Characteristic Value
¢	0.45%	аннан на н	
Mn	0.83%		
P	0.009%	· · · · ·	
. S	0.034%		
Si	0.18%		
Cu	0.41%		
Cr	0.15%		
Ni	0.22%	· · ·	
Mo	0.070%		
v	0.002%		
Cb	0.002%		
Sn	0.014%		
. A I	0.002%		
Yield Strength test 1	65.7ksi		
Tensile Strength test 1	102.8ksi		
Elongation test 1	12%		
Elongation Gage Lgth test 1	81N		
Bend Test Diameter	1.750IN		
Bend Test 1	Passed		

THIS MATERIAL IS FULLY KILLED. 100% MELTED AND MANUFACTURED IN THE USA. WITH NO WELD REPAIR OR MERCURY CONTAMINATION IN THE PROCESS. REMARKS :

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02/02/2012 23:04:38 Page 1 OF 1

1 STEEL MILL DRIVE For additional copies call Acuser f. Achaster Daniel J. Schacht SEGUIN TX 78155-7510 830-372-8771 cmc Quality Assurance Manager HEAT NO .: 3028494 S CMC Construction Svcs College Stati S CMC Construction Svcs College Stati Delivery#: 80669347 SECTION: REBAR 16MM (#5) 20'0" 0 H BOL#: 70236513 L 420/60 10650 State Hwy 30 ŧ 10650 State Hwy 30 CUST PO#: 5434V GRADE: ASTM A615-09b Gr 420/60 D College Station TX Ρ **College Station TX** CUST P/N: US 77845-7950 US 77845-7950 DLVRY LBS / HEAT: 45990.000 LB ROLL DATE: 11/18/2011 979 774 5900 979 774 5900 DLVRY PCS / HEAT: 2205 EA MELT DATE: 11/14/2011 т Т 0 0 Value Characteristic Value Characteristic Characteristic Value 0.38% С Mn. 1.00% Ρ 0.015% 0.030% S Si-0.22% 0.33% Cu Cr 0.21% 0.19% Ni 0.088% Мо v 0.003% СЬ 0.001% 0.013% รก 0.002% AI Yield Strength test 1 68.3ksi Tensile Strength test 1 108.1ksi Elongation test 1 15% Elongation Gage Lgth test 1 8IN Bend Test Diameter 2.188IN Bend Test 1 Passed

CERTIFIED MILL TEST REPORT

CMC STEEL TEXAS

We hereby certify that the test results presented here

are accurate and conform to the reported grade specification

THIS MATERIAL IS FULLY KILLED, 100% MELTED AND MANUFACTURED IN THE USA, WITH NO WELD REPAIR OR MERCURY CONTAMINATION IN THE PROCESS. REMARKS :

> 01/17/2012 21:56:23 Page 1 OF 1

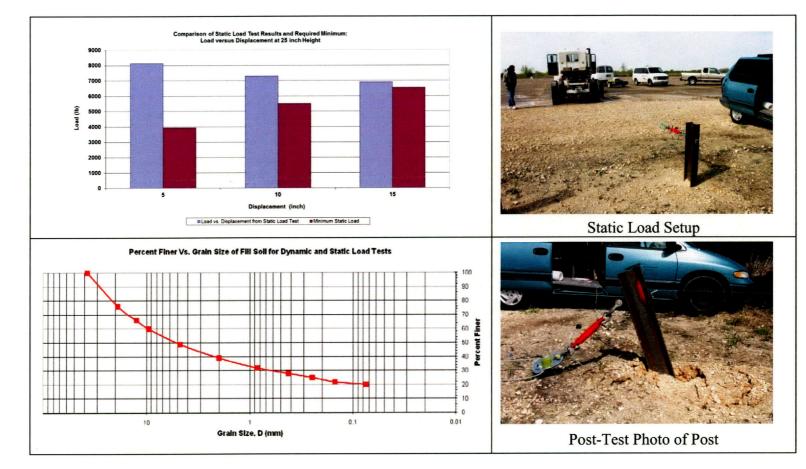


Table C1. Test Day Static Soil Strength Documentation for Test No. 490022-4.

Date	2012-05-14
Test Facility and Site Location	TTI Proving Ground—3100 SH 47, Bryan, TX
In Situ Soil Description (ASTM D2487)	
Fill Material Description (ASTM D2487) and sieve analysis	
Description of Fill Placement Procedure	6-inch lifts tamped with a pneumatic compactor

APPENDIX C. SOIL STRENGTH DOCUMENTATION

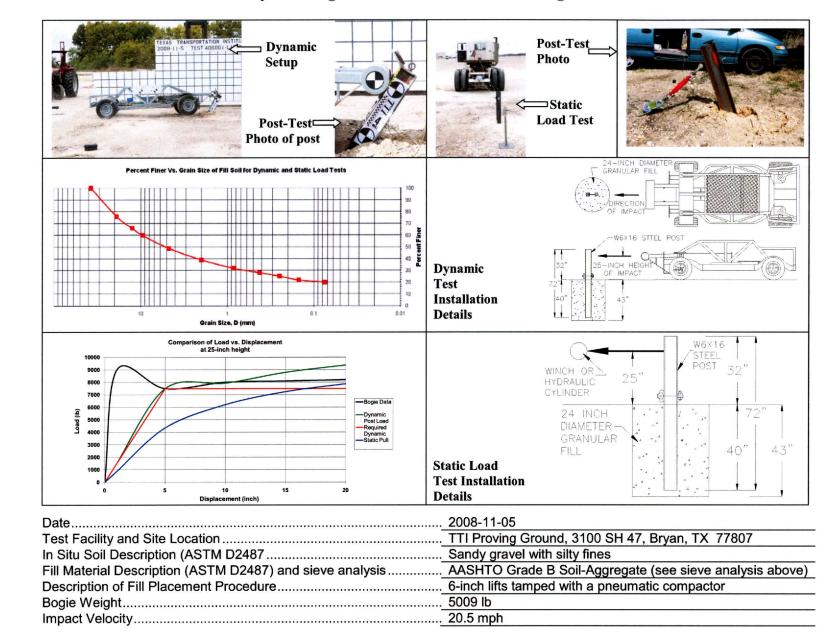


Table C2. Summary of Strong Soil Test Results for Establishing Installation Procedure.

APPENDIX D. TEST VEHICLE PROPERTIES AND INFORMATION

Date: _2012	-05-11	Test No.:	490022-4	4	VIN No.:	1D7HA182	236565998	81
Year: 2006	;	Make:	Dodge		Model	Ram 1500)	
Tire Size:	P265/70R17	,		Tire	Inflation Pre	essure: 35 p	osi	
Tread Type:	Highway							
		aiolo prior to f	loct:		out	<u> </u>		
Note any dam	age to the ver				X-	>	<u>.</u>	
 Denotes ac 	celerometer lo	ocation.			- W			
NOTES:						그슈(\square	
		· · ·		· [
Engine Type:	V-8			THEEL RACK				<u>ни т</u>
Engine CID:	4.7 liter						j	WHEEL TRACK
Transmission	Туре:		· • •				EST INERTIAL C. M.	
<u>x</u> Auto FWD	or x RWD	_ Manual 4WD		_ [+Q- >			
		4WD				71/711		Î
Optional Equi	oment:			-67				
							(m)	
Dummy Data: Type:	No dumm	N/					Ψ_{-}	K L
Mass:			-	◄ F	н			
Seat Position	ו:		- -			— Е ——		
Geometry:	inches				Ψ M FRONT	0	V M rear	
A 78.25		36.00	К	20.50	Р	2.88	U	28.50
В 75.00	<u> </u>	28.31	_ L _	29.12	Q	31.25		29.50
C223.75	<u>н</u>	60.39	_ M _	68.50	_ R _	18.38		60.50
D <u>47.25</u>	<u> </u>	13.75	_ N	68.00	S	12.00	_ X _	
E 140.50 Wheel Cent		25.38	O Wheel W	44.50	T _	77.00		
Height Fro		14.75 Cle	earance (From		5.00	Bottom Fra Height - Fr		17.12
Wheel Cent Height Re		14.75 Cle	Wheel We earance (Rea		10.25	Bottom Fra Height - Re		24.75
-	: A=78 ±2 inches	; C=237 ±13 in	ches; E=148	±12 inches;	F=39 ±3 inche	-		
				M+N/2=67 ±			-	
GVWR Ratin	-	Mass: Ib) <u>(</u>	<u>Surb</u>	Tes	t Inertial	Gros	ss Static
Front Back	<u> </u>	M _{front} M _{rear}		2875		<u>2852</u> 2150	<u> </u>	
Total	6700	M _{Total}		5026		5002		
		• • • I OTAI			wable Range fo	r TIM and GSM	= 5000 lb ±1	10 lb)
Mass Distrib	ution: LF:	1424	RF:	1428	LR:	1066	RR: 1	084

Table D1. Vehicle Properties for Test No. 490022-4.

TR No. 9-1002-12-4

Table D2. Vehicle Parametric Measurements for Test No. 490022-4.

Date: 2012-05	<u>-11</u> Te	st No.: _49	90022-4	<u> </u>	/IN: <u>1D7</u>	HA182365	65998	31	· · · ·
Year: 2006	· · ·	Make: D	odge	· · · ·	Model: F	Ram 1500	·		
Body Style: _Q	uad cab			Ň	/lileage: <u>1</u>	80713	· · ·		
Engine: 4.7 lite	er V-8			Transn	nission:	· · · · ·		· · · · ·	······································
Fuel Level: Er	npty	Balla	st: <u>120</u>) Ib at fror	nt of bed	<u> </u>		(440 lb	max)
Tire Pressure: F	Front: <u>3</u>	8 <u>5 </u>	Rear	35	psi Siz	e: <u>265/7</u>	0R17		· · · ·
Measured Ver	nicle Wei	ghts: (l	b)						
LF:	1424		RF:	1428		Front A	Axle:	2852	
LR:	1066		RR:	1084		Rear A	Axle:	2150	
Left:	2490		Right:	2512		Т	otal:	5002	
			- 			50	00 ±110	lb allow ed	
Whe	el Base:	140.5	inches	Track: F:	68.5	inches	R:	68	inches
	148 ±12 inch	es allow ed		 	Track = (F+R)/2 = 67 ±1.5	inches	allow ed	· · · · · · · · · · · · · · · · · · ·
Center of Gra	vity , SAE	J874 Sus	pension N	/lethod					
X:	60.39	in	Rear of F	ront Axle	(63 ±4 inches	s allow ed)			,
Y:	0.15	in	Left -	Right +	of Vehicle	Centerlin	ne		
Z:	28.31	in	Above Gr	ound	(minumum 28	.0 inches allo	ow ed)		• • • • • • • • • • • • • • • • • • •

Hood Height: 44.50 inches Front Bumper Height: 25.38 inches

Front Overhang:	36.00	inches	Rear I	Bump	er Height:	 29	.18	inches	
	39 ±3 inches allowed								
Overall Length:	223.75	inches							
	237 ±13 inches allowe	ed							

Date:	2012-05-11	Test No.:	490022-4	VIN No.:	1D7HA182365659981
Year:	2006	Make:	Dodae	Model:	Ram 1500

Table D3. Exterior Crush Measurements for Test No. 490022-4.

VEHICLE CRUSH MEASUREMENT SHEET¹ Complete When Applicable End Damage Side Damage Undeformed end width Bowing: B1 X1 Corner shift: A1 B2 X2 A2 A2 Bowing constant (check one) X1 + X2 X1 + X2 < 4 inches</td> 2 ----

Note: Measure C₁ to C₆ from Driver to Passenger side in Front or Rear impacts – Rear to Front in Side Impacts.

< 4 inches _____ ≥ 4 inches _____

		Direct Damage									
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	Ci	C ₂	C3	C4	C ₅	C ₆	±D
1	Front plane at bumper ht	16.0	10.0	27	0	2	4	4	6	10	+10.5
2	Side plane at bumper ht	16.0	17.0	50	1	4			15	17	+69
	· · · · · · · · ·										
	Measurements recorded						· .				
	in inches					-					

¹Table taken from National Accident Sampling System (NASS).

*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

**Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

***Measure and document on the vehicle diagram the location of the maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

Date:	2012-05-11	Test No.:	490022-4	· · · ·	VIN No.:	1D7HA1823	65659981
Year:	2006	Make:	Dodge	····	Model:	Ram 1500	· · · · · · · · · · · · · · · · · · ·
	11				FORMA	the second s	SUREMENT
<u> </u>						Before nches)	After (inches)
		(I I I E2 E3	E4	A1		64.50	64.50
	G			A2	· · · · ·	64.50	64.50
V				A3	· · · · · · · · · · · · · · · · · · ·	65.00	65.00
				B1	· · · · ·	45.25	45.25
		· · · · · · · · · ·		B2		39.25	39.25
				B 3		45.25	45.25
				B4		42.00	42.00
(– <u>I</u> AI-3 – –	34-6	B5	· · ·	42.50	42.50
		D1-3.		B6	· · · ·	42.00	42.00
\Box	CI CI	-3		C1	· · · · · · · · · · · · · · · · · · ·	27.25	27.25
(· · · ·		C2	·····		
				C3	 	29.25	27.50
				D1	 	12.75	12.75
				D2	 		· · · · · · · · · · · · · · · · · · ·
				D3		11.25	11.75
		B2,5		E1	·.·.· <u>.</u>	63.00	61.50
	B1,4	B3,6	· · ·	E2		64.50	64.00
		E1-4	-	E3	·	64.00	63.00
				E4		64.50	63.75
				F	· · ·	60.00	59.50
				G	· ·	60.00	60.00
				Н		39.00	39.00
*1	ana area tha a	ob from			· · · · ·	39.00	39.00
	l area across the c side kickpanel to		e kickpanel.	J*		63.25	59.75

Table D4. Occupant Compartment Measurements for Test No. 490022-4.

TR No. 9-1002-12-4

APPENDIX E. SEQUENTIAL PHOTOGRAPHS

0.000 s

0.049 s

0.098 s

















Figure E1. Sequential Photographs for Test No. 490022-4 (Overhead and Frontal Views).

0.147 s











0.196s

0.245 s

0.294 s







Figure E1. Sequential Photographs for Test No. 490022-4 (Overhead and Frontal Views) (continued).

0.343 s





0.049 s



0.098 s



0.147 s





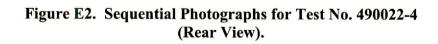
0.245 s

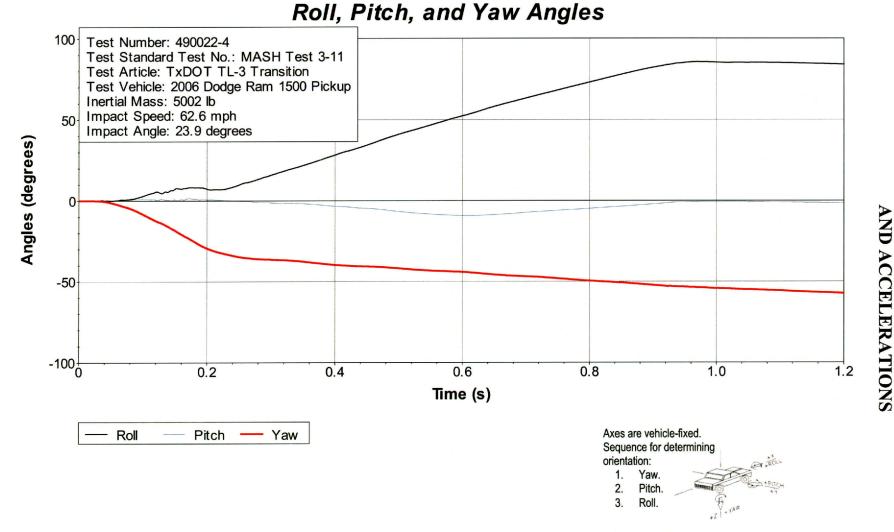


0.294 s



0.343 s





APPENDIX F. VEHICLE ANGULAR DISPLACEMENTS

Figure F1. Vehicle Angular Displacements for Test No. 490022-4.

TR No. 9-1002-12-4

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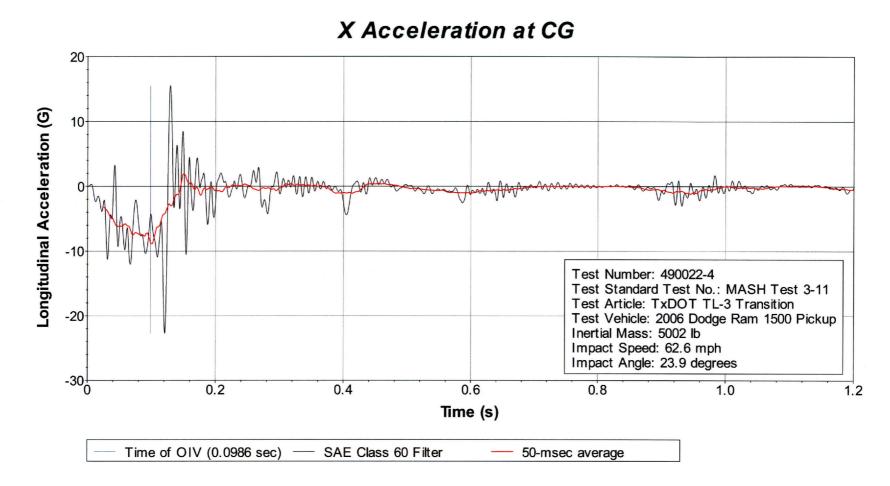


Figure F2. Vehicle Longitudinal Accelerometer Trace for Test No. 490022-4 (Accelerometer Located at Center of Gravity).

TR No. 9-1002-12-4

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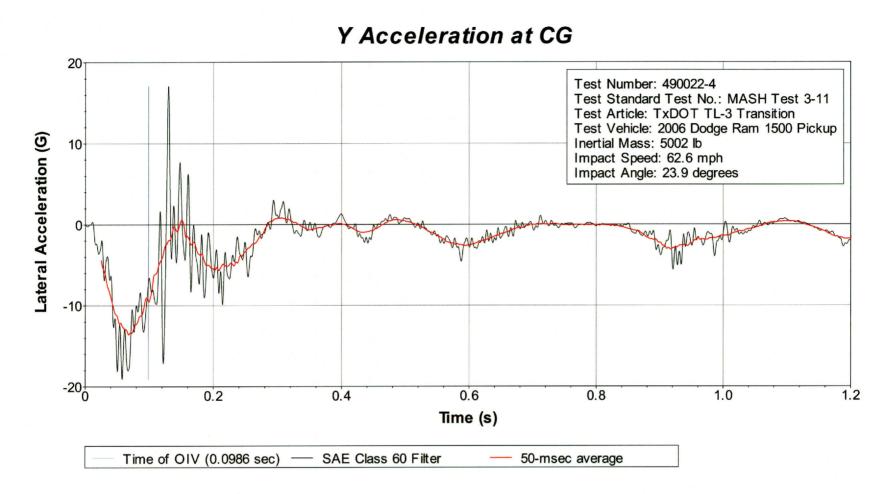


Figure F3. Vehicle Lateral Accelerometer Trace for Test No. 490022-4 (Accelerometer Located at Center of Gravity).

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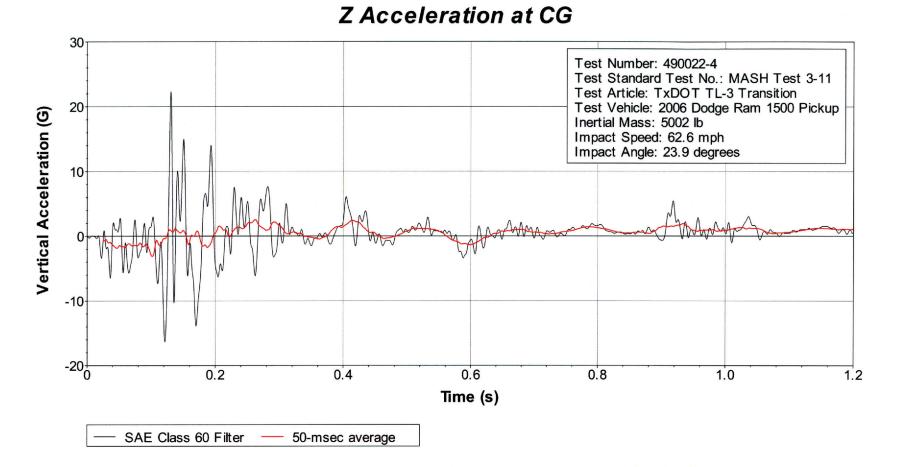


Figure F4. Vehicle Vertical Accelerometer Trace for Test No. 490022-4 (Accelerometer Located at Center of Gravity).

TR No. 9-1002-12-4

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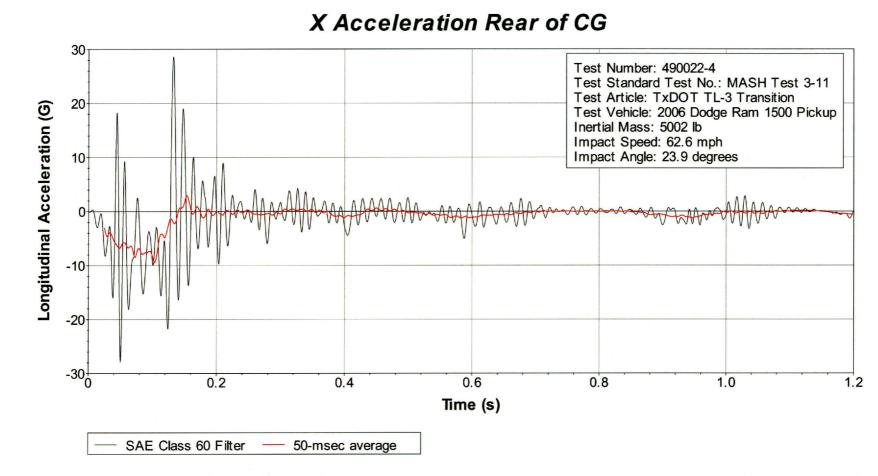
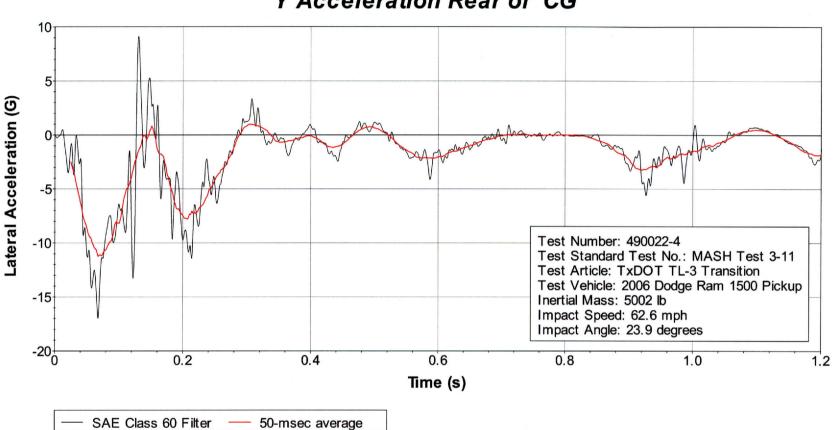


Figure F5. Vehicle Longitudinal Accelerometer Trace for Test No. 490022-4 (Accelerometer Located Rear of Center of Gravity).

2013-07-09

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Y Acceleration Rear of CG

Figure F6. Vehicle Lateral Accelerometer Trace for Test No. 490022-4 (Accelerometer Located Rear of Center of Gravity).

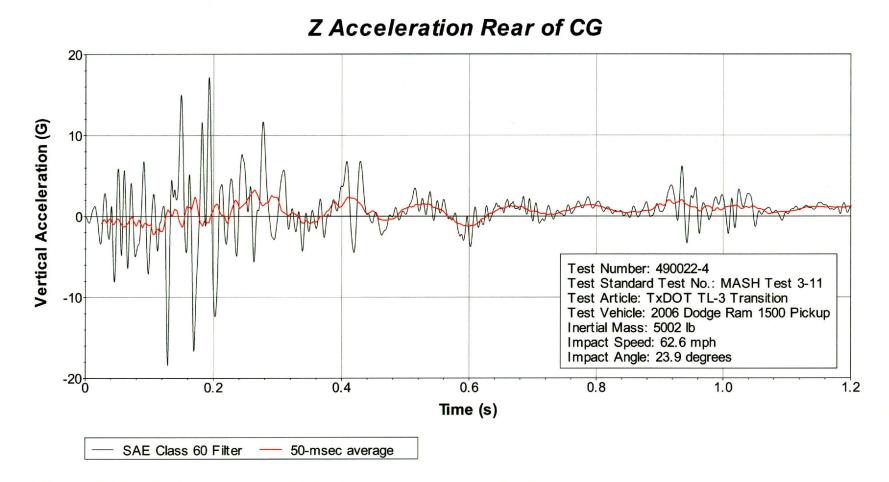


Figure F7. Vehicle Vertical Accelerometer Trace for Test No. 490022-4 (Accelerometer Located Rear of Center of Gravity).

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