## Texas A\&M Transportation Institute

## MASH TEST 3-21 ON TL-3 THRIE BEAM TRANSITION WITHOUT CURB



Crash testing performed at:
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| 16. Abstract <br> This project evaluated the impact performance of a modified TxDOT thrie beam transition to rigid concrete barrier without a curb element below the transition rail. In a previous test described in TxDOT Research Report 0-4564, a thrie beam transition without curb failed to meet NCHRP Report 350 performan criteria. However, it could not be discerned whether the vehicle instability observed in that test was attributable to the missing curb or the rotation of the thrie beam transition rail into the sloped face of the concrete safety shape rail at the bridge end connection point. <br> A transition design without curb would reduce the complexity of the field installations and would provide an option for dealing with different drainage requirements at bridge ends. A fabricated steel blockout was incorporated into the transition system to keep the thrie beam rail and terminal connector in vertical plane at its connection to the concrete bridge rail. <br> The modified thrie beam transition without curb failed to meet MASH TL-3 requirements due to rollover of the impacting vehicle. Further discussions as to the possible cause of the failure are described within the report. |  |  |  |  |
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# MASH TEST 3-21 ON TL-3 THRIE BEAM TRANSITION WITHOUT CURB 

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## DISCLAIMER

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## TTI PROVING GROUND DISCLAIMER

The results of the crash testing reported herein apply only to the article being tested.


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## CHAPTER 1. INTRODUCTION

### 1.1 INTRODUCTION

This project was set up to provide the Texas Department of Transportation (TxDOT) with a mechanism to quickly and effectively evaluate high-priority issues related to roadside safety devices. Roadside safety devices shield motorists from roadside hazards such as non-traversable terrain and fixed objects. To maintain the desired level of safety for the motoring public, these safety devices must be designed to accommodate a variety of site conditions, placement locations, and a changing vehicle fleet. Periodically, there is a need to assess the compliance of existing safety devices with current vehicle testing criteria and develop new devices that address identified needs.

Under this project, roadside safety issues are identified and prioritized for investigation. Each roadside safety issue is addressed with a separate work plan, and the results are summarized in individual test reports.

### 1.2 BACKGROUND

Current roadside safety barriers can be generalized into a two categories. The first category includes rigid barriers such as permanent concrete median barriers. The second category includes flexible barriers such as metal beam guard fence. These barriers are highly effective in redirecting errant vehicles; however, they have significantly different deflection characteristics. Approach guardrail is often attached to a bridge rail to shield motorists from hazards at the bridge end and those underlying the bridge. A transition system is needed to transition the stiffness between the two systems to avoid impact performance issues such as pocketing and snagging on the rigid end of the bridge parapet.

In May 1998, Midwest Roadside Safety Facility (MwRSF) released a report detailing the design and testing of "Two Approach Guardrail Transitions for Concrete Safety Shape Barriers." This research was funded by the Midwest State's Regional Pooled Fund Program. The report details the design and testing of both steel and wood post options for transitioning W-beam guardrail to a concrete safety shape barrier. Two key features of these nested thrie beam transition designs include a curb under the transition rail near the concrete parapet end and a steel offset block that allows the thrie beam to be vertically connected to the sloped face of the concrete parapet without having to twist the thrie beam section. Both designs met National Cooperative Highway Research Program (NCHRP) Report 350 (1) evaluation criteria for Test Level 3 (TL-3).

In October 2003, TxDOT requested that Texas A\&M Transportation Institute (TTI) evaluate a modified TL-3 nested thrie beam transition. The first modification was to eliminate the curb from under the transition rail. Second, the fabricated steel offset block under the terminal connector was removed. Instead, the nested thrie beam and terminal connector was twisted to match and connect directly to the sloped face of the concrete safety shape parapet.

TxDOT requested these modifications to reduce fabrication and installation complexity and cost. The modified transition system failed to meet NCHRP Report 350 TL-3 performance criteria. The impacting vehicle overturned as it exited the transition system. It could not be conclusively determined which modification contributed more to the vehicle instability.

The American Association of State Highway and Transportation Officials (AASHTO) published the Manual for Assessing Safety Hardware (MASH) in October 2009 (2). MASH supersedes NCHRP Report 350 as the recommended guidance for the safety performance evaluation of roadside safety features. In October 2006, MwRSF published Research Report TRP-03-175-06. This report documents a successful MASH TL-3 crash test (Test Designation 3-21) on the original nested thrie beam transition design. This test was performed as part of NCHRP Project 22-14(2).

Subsequently, TxDOT requested that a $M A S H$ test be performed to evaluate the impact performance of a modified TxDOT thrie beam transition to rigid concrete barrier without a curb element below the transition rail. A transition design without curb would reduce the complexity of the field installations and would provide an option for dealing with different drainage requirements at bridge ends. The difference between the previous failed transition test and the proposed design is that a fabricated steel blockout was incorporated into the transition system to keep the thrie beam rail and terminal connector in a vertical plane at its connection to the concrete bridge rail.

### 1.3 OBJECTIVES/SCOPE OF RESEARCH

This project evaluated the impact performance of a modified transition design for approach W-beam guardrail to a rigid concrete bridge rail without a curb element beneath the transition rail. The test was performed in accordance with $M A S H$ guidelines following the impact conditions for Test Designation 3-21.

## CHAPTER 2. SYSTEM DETAILS

### 2.1 TEST ARTICLE DESIGN AND CONSTRUCTION

A total installation length of $92 \mathrm{ft}-63 / 4$ inch was installed to fully evaluate the bridge rail to metal beam guard fence transition according to MASH TL-3 impact conditions. A $16-\mathrm{ft}$ single slope concrete bridge rail served as a surrogate bride rail parapet end condition. The remaining $76 \mathrm{ft}-63 / 4$ inches was constructed of metal beam guard fence. This length includes a TL-3 approved terminal and the TL-3 transition itself. A generic overall diagram of the test installation can be found in Figures 2.1 and 2.2. A full set of shop/fabrication drawings can be found in Appendix A.

The surrogate bridge rail parapet was constructed according to TxDOT 36-inch single slope traffic rail (SSTR) bridge rail standards found on the TxDOT standards website (http://www.dot.state.tx.us). As the standard suggests, the barrier is a 36 -inch tall wall with a 79 degree constant slope traffic face. The barrier is $71 / 2$ inches wide at the top of the barrier and $141 / 2$ inches wide at the bottom of the barrier at the end of the parapet. The barrier is cast atop an 18 -inch thick moment slab designed to withstand a MASH TL-4 impact. The concrete used in constructing the parapet and moment slab met/exceeded TxDOT Class C ( 3600 psi ) specifications. The barrier toe was chamfered at the end of the parapet. The chamfer was $133 / 8$ inches tall and 36 inches long. A total of five 1 -inch holes were cast into the parapet to allow for the attachment of the 10 gauge thrie-beam terminal end shoe (RTE01b) and a custom $1 / 4$-inch thick adapter plate using five $7 / 8$-inch A325 bolts.

The reinforcement in the parapet included the following according to TxDOT SSTR barrier standards. "S-bars" and "U-bars" are placed every 5 inches along the length of the parapet. A total of eight \#4 bars ( $1 / 2$-inch) were equally spaced along the face of the parapet. The 18 -inch deck was reinforced with two distinct rebar mats each containing \#5 bars spaced every 6 inches perpendicular to the parapet and \#4 bars spaced every 9 inches parallel to the parapet. The first mat maintained a 3-inch cover from the bottom of the moment slab. The second mat maintained a 2 -inch cover from the top of the moment slab.

The metal beam guard fence was constructed using a total of 19 posts that were numbered from 1 to 19 starting with the ET-2000 Terminal control release post (CRP) anchor post. Posts 1 and 2 were installed as part of the standard 31-inch ET-2000 Terminal. Posts 3 through 11 are installed as part of a standard 12 gauge W-Beam Guardrail (RWM04a). Each post in this section is a 72 -inch long W $6 \times 8.5$ SLP (PEW01) attached to the 12 gauge rail element using an 8 -inch wood blockout. The posts in this section were placed at the mid-span of the guardrail (not at a splice). Between posts 11 and 13, a 10 gauge thrie beam to W -beam nonsymmetric transition segment is used and is supported by a 72 -inch long W6 $\times 8.5$ SLP. Between Post 13 and the end of the bridge parapet, a nested 12 gauge thrie beam (RTM02a) configuration is used and is supported by 84 -inch long W $6 \times 8.5$ posts with $6 \times 8 \times 18$-inch wood blockouts. A 10 gauge thrie-beam end shoe (RTE01b) was used to connect the nested thrie beam to the $1 / 4$-inch thick adapter plate.



DETAIL A
SCALE 1：50

Texas Transportation Institute The Texas A\＆M University System College Station，Iexas 77843
Project 490022－4 TL－3 Transition Drawn By GES Scale 1：120 Sheet 1 of 9 Plan View
Approved：Dignature：Date： Dusty Arrington：

Signature： 2012－01－10

Figure 2．1．Layout of the TxDOT TL－3 Transition．


2 a. $6^{\prime \prime} \times 8^{\prime \prime} \times 18^{\prime \prime}$ routered Wood Blockouts at posts $12-19.6^{\prime \prime} \times 8^{\prime \prime} \times 14^{\prime \prime}$ routered wood blockouts at posts $3-11$. 1-3/4" long Button-head Guardrail Bolts (FBB02) at nested thrie-beam splices. 1-1/4" long Button-head Guardrail Bolts (FBB01) at all other rail splices. $10^{\prime \prime}$ long Button-head Guardrail Bolts (FBB03) at rail to post attachments at posts 3-19. Recessed Guardrail Nuts (FBB) at all button-head bolts. 2b. Place galvanized rectangular washers (FWR03) under Guardrail Nuts at Thriebeam to Terminal Splice.
2c. Only one Rail Bolt is at post 13 , in the top slot.


Figure 2.2. Details of the TxDOT TL-3 Transition.


Figure 2.3. TxDOT TL-3 Transition Installation before Test No. 490022-4.

The adapter plate is constructed using $1 / 4$-inch steel plate. The adapter is 21 inches tall and 40 inches wide. The adapter plate allows for a 4 -inch blockout at the top of the plate and tapers down to a 0 -inch blockout distance. Quarter-inch thick stiffener plates are then welded to the back of the plate to stiffen the plate.

### 2.2 MATERIAL SPECIFICATIONS

As discussed in section 2.1, the concrete used to construct the concrete parapet meets/exceeds TxDOT Class C ( 3600 psi ) specifications. All steel plates and structural members meet A36 material specifications. All standard American Road and Transportation Builders Association (ARTBA) parts meet/exceed material specifications associated with their assigned classification numbers.

### 2.3 SOIL CONDITIONS

The TxDOT TL-3 Transition was installed in standard soil meeting AASHTO standard specifications for "Materials for Aggregate and Soil Aggregate Subbase, Base and Surface Courses," designated M147-65(2004), grading B.

In accordance with Appendix B of $M A S H$, soil strength was measured the day of the crash test (see Appendix C, Figure C1). During installation of the TxDOT TL-3 Transition for full-scale crash testing, two standard W $6 \times 16$ posts were installed in the immediate vicinity of the TxDOT TL- 3 Transition, utilizing the same fill materials and installation procedures used in the standard dynamic test (see Appendix C, Figure C2).

As determined in the tests shown in Appendix C, Figure C2, the minimum post load required for deflections at 5 inches, 10 inches, and 15 inches, measured at a height of 25 inches, is $3940 \mathrm{lb}, 5500 \mathrm{lb}$, and 6540 lb , respectively ( 90 percent of static load for the initial standard installation). On the day of the test, April 14, 2009, load on the post at deflections of 5 inches, 10 inches, and 15 inches was $8121 \mathrm{lbf}, 7303 \mathrm{lbf}$, and 6909 lbf , respectively. The strength of the backfill material met minimum requirements.

## CHAPTER 3. TEST REQUIREMENTS AND EVALUATION CRITERIA

### 3.1 CRASH TEST MATRIX

According to MASH, two tests are recommended to evaluate transitions to test level three (TL-3).

MASH Test Designation 3-20: A 2425-lb vehicle impacting the critical impact point (CIP) of the length of need (LON) of the barrier at a nominal impact speed and angle of $62 \mathrm{mi} / \mathrm{h}$ and 25 degrees, respectively. This test investigates a barrier's ability to successfully contain and redirect a small passenger vehicle.

MASH Test Designation 3-21: A 5000-lb pickup truck impacting the CIP of the LON of the barrier at a nominal impact speed and angle of $62 \mathrm{mi} / \mathrm{h}$ and 25 degrees, respectively. This test investigates a barrier's ability to successfully contain and redirect light trucks and sport utility vehicles.

Based on the geometry and strength of the transition design, the project team concluded that Test 3-20 was not warranted. The test reported here corresponds to Test 3-21 of MASH ( $5000-\mathrm{lb}$ pickup, $62 \mathrm{mi} / \mathrm{h}, 25$ degrees).

The crash test and data analysis procedures were in accordance with guidelines presented in MASH. Chapter 4 presents brief descriptions of these procedures.

### 3.2 EVALUATION CRITERIA

The crash test was evaluated in accordance with the criteria presented in MASH. The performance of the TxDOT TL-3 Transition is judged on the basis of three factors: structural adequacy, occupant risk, and post impact vehicle trajectory. Structural adequacy is judged upon the ability of the TxDOT TL-3 Transition to contain and redirect the vehicle, or bring the vehicle to a controlled stop in a predictable manner. Occupant risk criteria evaluate the potential risk of hazard to occupants in the impacting vehicle, and to some extent, other traffic, pedestrians, or workers in construction zones, if applicable. Post-impact vehicle trajectory is assessed to determine potential for secondary impact with other vehicles or fixed objects, creating further risk of injury to occupants of the impacting vehicle and/or risk of injury to occupants in other vehicles. The appropriate safety evaluation criteria from Table 5-1 of $M A S H$ were used to evaluate the crash test reported here and are listed in further detail under the assessment of the crash test.

## CHAPTER 4. CRASH TEST PROCEDURES

### 4.1 TEST FACILITY

The full-scale crash test reported here was performed at Texas A\&M Transportation Institute Proving Ground, an International Standards Organization (ISO) 17025 accredited laboratory with American Association for Laboratory Accreditation (A2LA) Mechanical Testing certificate 2821.01. The full-scale crash test was performed according to TTI Proving Ground quality procedures and according to the $M A S H$ guidelines and standards.

The Texas A\&M Transportation Institute Proving Ground is a 2000 -acre complex of research and training facilities located 10 miles northwest of the main campus of Texas A\&M University. The site, formerly an Air Force base, has large expanses of concrete runways and parking aprons well-suited for experimental research and testing in the areas of vehicle performance and handling, vehicle-roadway interaction, durability and efficacy of highway pavements, and safety evaluation of roadside safety hardware. The site selected for construction and testing of the T131RC Bridge Rail evaluated under this project was along the edge of an out-of-service apron. The apron consists of an unreinforced jointed-concrete pavement in $12.5 \mathrm{ft} \times$ 15 ft blocks nominally 6 inches deep. The apron is over 60 years old, and the joints have some displacement, but are otherwise flat and level.

### 4.2 VEHICLE TOW AND GUIDANCE PROCEDURES

The test vehicle was towed into the test installation using a steel cable guidance and reverse tow system. A steel cable for guiding the test vehicle was tensioned along the path, anchored at each end, and threaded through an attachment to the front wheel of the test vehicle. An additional steel cable was connected to the test vehicle, passed around a pulley near the impact point, through a pulley on the tow vehicle, and then anchored to the ground such that the tow vehicle moved away from the test site. A $2: 1$ speed ratio between the test and tow vehicle existed with this system. Just prior to impact with the installation, the test vehicle was released to be unrestrained. The vehicle remained free-wheeling (i.e., no steering or braking inputs) until it cleared the immediate area of the test site, after which the brakes were activated to bring it to a safe and controlled stop.

### 4.3 DATA ACQUISITION SYSTEMS

### 4.3.1 Vehicle Instrumentation and Data Processing

The test vehicle was instrumented with a self-contained, on-board data acquisition system. The signal conditioning and acquisition system is a 16 -channel, Tiny Data Acquisition System (TDAS) Pro produced by Diversified Technical Systems, Inc. The accelerometers that measure the $\mathrm{x}, \mathrm{y}$, and z axis of vehicle acceleration are strain gauge type with linear millivolt output proportional to acceleration. Angular rate sensors measuring vehicle roll, pitch, and yaw
rates are ultra-small size, solid state units designed for crash test service. The TDAS Pro hardware and software conform to the latest SAE J211, Instrumentation for Impact Test. Each of the 16 channels is capable of providing precision amplification, scaling, and filtering based on transducer specifications and calibrations. During the test, data are recorded from each channel at a rate of 10,000 values per second with a resolution of one part in 65,536 . Once the data are recorded, internal batteries back these up inside the unit should the primary battery cable be severed. Initial contact of the pressure switch on the vehicle bumper provides a time zero mark and initiates the recording process. After each test, the data are downloaded from the TDAS Pro unit into a laptop computer at the test site. The Test Risk Assessment Program (TRAP) software then processes the raw data to produce detailed reports of the test results. Each of the TDAS Pro units are returned to the factory annually for complete recalibration. Accelerometers and rate transducers are also calibrated annually with traceability to the National Institute for Standards and Technology.

TRAP uses the data from the TDAS Pro to compute occupant/compartment impact velocities, time of occupant/compartment impact after vehicle impact, and the highest 10 -millisecond ( ms ) average ridedown acceleration. TRAP calculates change in vehicle velocity at the end of a given impulse period. In addition, the program computes the maximum average accelerations over $50-\mathrm{ms}$ intervals in each of the three directions. For reporting purposes, the data from the vehicle-mounted accelerometers are filtered with a $60-\mathrm{Hz}$ digital filter, and acceleration versus time curves for the longitudinal, lateral, and vertical directions are plotted using TRAP.

TRAP uses the data from the yaw, pitch, and roll rate transducers to compute angular displacement in degrees at 0.0001 -s intervals and then plots yaw, pitch, and roll versus time. These displacements are in reference to the vehicle-fixed coordinate system with the initial position and orientation of the vehicle-fixed coordinate systems being initial impact.

### 4.3.2 Anthropomorphic Dummy Instrumentation

According to $M A S H$, the use of a dummy in the 2270 P vehicle is optional. Researchers did not use any dummy in the test with the 2270 P vehicle.

### 4.3.3 Photographic Instrumentation and Data Processing

Photographic coverage of the test included three high-speed cameras: one overhead with a field of view perpendicular to the ground and directly over the impact point; one placed behind the installation at an angle; and a third placed to have a field of view parallel to and aligned with the installation at the downstream end. A flashbulb activated by pressure-sensitive tape switches was positioned on the impacting vehicle to indicate the instant of contact with the installation and was visible from each camera. The films from these high-speed cameras were analyzed on a computer-linked motion analyzer to observe phenomena occurring during the collision and to obtain time-event, displacement, and angular data. A mini-DV camera and still cameras recorded and documented conditions of the test vehicle and installation before and after the test.

## CHAPTER 5. CRASH TEST RESULTS

### 5.1 TEST DESIGNATION AND ACTUAL IMPACT CONDITIONS

MASH Test 3-21 involves a 2270 P vehicle weighing $5000 \mathrm{lb} \pm 100 \mathrm{lb}$ and impacting the bridge rail transition at an impact speed of $62.2 \mathrm{mi} / \mathrm{h} \pm 2.5 \mathrm{mi} / \mathrm{h}$ and an angle of 25 degrees $\pm 1.5$ degrees. The target impact point of 93 inches upstream of concrete parapet was determined through Barrier VII simulations and the tables found within MASH for determining CIP. The 2006 Dodge Ram 1500 pickup truck used in the test weighed 5002 lb and the actual impact speed and angle were $62.6 \mathrm{mi} / \mathrm{h}$ and 23.9 degrees, respectively. The actual impact point was 89.0 inches upstream of the concrete parapet. Target impact severity (IS) was calculated at $115.1 \mathrm{kip} * \mathrm{ft}$, and actual IS was calculated at 107.6 kip ftt, which was 6.5 percent less than target IS (acceptable limit for IS is not less than 8 percent of target IS).

### 5.2 TEST VEHICLE

A 2006 Dodge Ram 1500 pickup truck, shown in Figure 5.1, was used for the crash test. Test inertia weight of the vehicle was 5002 lb , and its gross static weight was 5002 lb . The height to the lower edge of the vehicle bumper was 13.7 inches, and it was 25.38 inches to the upper edge of the bumper. Tables D1 and D2 in Appendix D give additional dimensions and information on the vehicle. The vehicle was directed into the installation using the cable reverse tow and guidance system, and was released to be unrestrained just prior to impact.

### 5.3 WEATHER CONDITIONS

The test was performed on the morning of May 14, 2012. Weather conditions at the time of testing were: wind speed: $2 \mathrm{mi} / \mathrm{h}$; wind direction: 206 degrees with respect to the vehicle (vehicle was traveling in a southwesterly direction); temperature: $80^{\circ} \mathrm{F}$, relative humidity: 58 percent.


### 5.4 TEST DESCRIPTION

The 2006 Dodge Ram 1500 pickup truck, traveling at an impact speed of $62.6 \mathrm{mi} / \mathrm{h}$, impacted the TxDOT TL-3 Transition 89.0 inches upstream of the concrete parapet at an impact angle of 23.9 degrees. At 0.010 s after impact, the vehicle began to redirect, and at 0.012 s , the thrie-beam guardrail and posts on either side of impact began to deflect toward the field side. The right front tire contacted the concrete parapet at 0.101 s , and the right front tire and wheel rim separated from the vehicle. At 0.168 s , the vehicle was traveling parallel with the transition at a speed of $52.7 \mathrm{mi} / \mathrm{h}$. The rear of the vehicle contacted the transition at 0.176 s . At 0.316 s , the vehicle lost contact with the transition and was traveling at an exit speed and angle of $52.3 \mathrm{mi} / \mathrm{h}$ and 16.2 degrees. As the vehicle exited the transition, it rolled onto its right side and came to rest 208.4 ft downstream of impact and 75.0 ft toward traffic lanes. Figures E1 and E2 in Appendix E show sequential photographs of the test period.


Figure 5.1. Vehicle before Test No. 490022-4.

### 5.5 DAMAGE TO TEST INSTALLATION

Figures 5.2 and 5.3 show damage to the TxDOT TL-3 Transition. The soil was disturbed around post 1 and posts 10 through 12. Post 13 was leaning toward the field side and downstream 0.5 degree (from upright), and there was a gap of 0.25 inch between the edge of the soil and the traffic side of the post. Post 14 was deflected toward the field side 1.12 inches and was leaning 6 degrees toward the field side and 1 degree downstream. Post 15 was deflected toward the field side 1.62 inches and leaning toward field side 6 degrees and downstream 3 degrees. Post 16 was deflected toward the field side 2.0 inches and leaning toward the field side 5 degrees and downstream 7 degrees. Post 17 was deflected toward the field side 1.9 inches and was leaning toward the field side 4 degree and downstream 4 degrees. Post 18 was deflected toward the field side 1.5 inches and leaning toward the field side 5 degrees and downstream 3 degrees. Post 19 was deflected toward the field side 1.4 inches and leaning toward the field side 7 degrees and downstream 6 degrees. Maximum permanent deformation of the thrie beam rail element was 4.5 inches at the top ridge, 3.9 inches at the middle ridge, and 6.5 inches at the bottom ridge. Total length of contact of the vehicle with the thrie beam rail element was 149.0 inches. Working width was 22.8 inches and maximum dynamic deflection of the top of the rail element was 5.9 inches.

### 5.6 VEHICLE DAMAGE

As shown in Figure 5.4, the 2270P vehicle was damaged in the right front and right side. The right frame rail, right front upper and lower A-arms, right front upper and lower ball joints, and right outer tie rods were deformed. Also damaged were the front bumper, hood, grill, right front fender, right front tire and wheel rim, right front door and door glass, right rear door, right exterior bed, rear bumper, tailgate, and right rear wheel rim. Maximum exterior crush to the vehicle was 170.0 inches in the front plane at the right front corner at bumper height. Maximum occupant compartment deformation was 3.75 inches in the lateral area across the occupant compartment in the kickpanel area near the front passenger's feet. Figure 5.5 shows the occupant compartment before and after the test. Tables D3 and D4 of Appendix D present the exterior and interior crush measurement.

### 5.7 OCCUPANT RISK FACTORS

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk. In the longitudinal direction, the occupant impact velocity was $16.4 \mathrm{ft} / \mathrm{s}$ at 0.099 s , the highest $0.010-\mathrm{s}$ occupant ridedown acceleration was 14.4 Gs from 0.114 to 0.124 s , and the maximum $0.050-\mathrm{s}$ average acceleration was -8.9 Gs between 0.075 and 0.125 s . In the lateral direction, the occupant impact velocity was $27.6 \mathrm{ft} / \mathrm{s}$ at 0.099 s , the highest 0.010 -s occupant ridedown acceleration was 9.0 Gs from 0.103 to 0.113 s , and the maximum 0.050 -s average was -13.6 Gs between 0.043 and 0.093 s . Theoretical Head Impact Velocity (THIV) was $34.9 \mathrm{~km} / \mathrm{h}$ or $9.7 \mathrm{~m} / \mathrm{s}$ at 0.097 s ; Post-Impact Head Decelerations (PHD) was 16.2 Gs between 0.114 and 0.124 s ; and Acceleration Severity Index (ASI) was 1.63 between 0.044 and 0.094 s. Figure 5.6 summarizes these data and other pertinent information from the test. Vehicle angular displacements and accelerations versus time traces are presented in Appendix F, Figures F1 through F7.


Figure 5.2. TxDOT TL-3 Transition/Vehicle after Test No. 490022-4.


Figure 5.3. TxDOT TL-3 Transition after Test No. 490022-4.


Figure 5.4. Vehicle after Test No. 490022-4.


Figure 5.5. Interior of Vehicle after Test No. 490022-4.


0.098 s

0.196 s



0.343 s


| General Information |  |
| :---: | :---: |
| Test Agency ........................ | Texas A\&M Transportation Institute (TTI) |
| Test Standard Test No. ......... | MASH Test 3-21 |
| TTI Test No. ..................... | 490022-4 |
| Test Date ......................... | 2012-05-14 |
| Test Article |  |
| Type................................. | Transition |
| Name ................................. | TxDOT TL-3 Transition |
| Installation Length ............... | 92.5 ft |
| Material or Key Elements ...... | Nested 10 gauge thrie beam guardrail on steel posts spaced at 18.75 inches on center |
| Soil Type and Condition........ | Standard Soil, Dry |
| Test Vehicle |  |
| Type/Designation ................. | 2270P |
| Make and Model.................. | 2006 Dodge Ram 1500 |
| Curb ................................... | 5026 lb |
| Test Inertial ......................... | 5002 lb |
| Dummy............................... | No dummy |
| Gross Static......................... | 5002 lb |



| Post-Impact Trajectory |  |
| :---: | :---: |
| Stopping Distance ....... | 208.4 ft dwmstr , 75.4 ft twd traffic |
| Vehicle Stability |  |
| Maximum Yaw Angle............... 61 degrees |  |
| Maximum Pitch Angle.............. 9 degrees |  |
| Maximum Roll Angle................ 90 degrees |  |
| Vehicle Snagging.................... No |  |
| Vehicle Pocketing................... No |  |
| Test Article Deflections |  |
| Dynamic ............................... 5.9 inches @ top |  |
| Permanent............................. 6.5 inches @ bottom |  |
| Working Width ........................ 22.8 inches |  |
| Vehicle Damage |  |
| VDS...................................... 01FREW4 |  |
| CDC .................................... 01RFQ5 |  |
| Max. Exterior Deformation ....... 17.0 inches |  |
| OCDI ..................................... RF0010000 |  |
| Max. Occupant Compartment |  |
| Deformation........... | 3.5 inches |

Figure 5.6. Summary of Results for MASH Test 3-21 on the TxDOT TL-3 Transition.

## CHAPTER 6. SUMMARY AND CONCLUSIONS

### 6.1 ASSESSMENT OF TEST RESULTS

An assessment of the test based on the applicable $M A S H$ safety evaluation criteria is provided below.

### 6.1.1 Structural Adequacy

A. Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.

Results: The TxDOT TL-3 Transition contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection of the metal rail element was 7.9 inches. (PASS)

### 6.1.2 Occupant Risk

D. Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.
Deformation of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH. (roof $\leq 4.0$ inches; windshield $=\leq 3.0$ inches; side windows $=$ no shattering by test article structural member; wheel/foot well/toe pan $\leq 9.0$ inches; forward of A-pillar $\leq 12.0$ inches; front side door area above seat $\leq 9.0$ inches; front side door below seat $\leq 12.0$ inches; floor pan/transmission tunnel area $\leq 12.0$ inches)

Results: No detached elements, fragments, or other debris was present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area. (PASS)
Maximum occupant compartment deformation was 3.75 inches in the lateral area across the occupant compartment in the kickpanel area near the front passenger's feet. (PASS)
F. The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.

Results: The 2270 P vehicle rolled 90 degrees onto its right side after exiting the transition. (FAIL)
H. Occupant impact velocities should satisfy the following:

Longitudinal and Lateral Occupant Impact Velocity
$\frac{\text { Preferred }}{30 \mathrm{ft} / \mathrm{s}} \quad \frac{\text { Maximum }}{40 \mathrm{ft} / \mathrm{s}}$

Results: Longitudinal occupant impact velocity was $16.4 \mathrm{ft} / \mathrm{s}$, and lateral occupant impact velocity was $27.6 \mathrm{ft} / \mathrm{s}$. (PASS)
I. Occupant ridedown accelerations should satisfy the following:

Longitudinal and Lateral Occupant Ridedown Accelerations Preferred $\quad$ Maximum 15.0 Gs $\quad \because 20.49$ Gs

Results: Longitudinal ridedown acceleration was 14.4 G , and lateral ridedown acceleration was 9.0 G . (PASS)

### 6.1.3 Vehicle Trajectory

For redirective devices, the vehicle shall exit the barrier within the exit box. Report vehicle rebound distance and velocity for crash cushions.

Result: The 2270 P vehicle exited within the exit box. (PASS)

### 6.2 CONCLUSIONS

The TxDOT TL-3 Transition did not perform acceptably for MASH test 3-21 due to vehicle rollover (see Table 6.1). There were indications of wheel snagging on the end of the concrete parapet that may have contributed to destabilization of the vehicle.

### 6.3 RECOMMENDATIONS*

The researchers suggest that the following are possible design changes may improve the performance of the system. First, a short curb may be placed at the end of the parapet under the rail to help prevent the wheel snagging. This is consistent with previous design details; however, the researchers feel the length may be reduced to help with the draining problems that prompted this test. Second, the steel blockout at the end of the parapet could be increased in depth to offset the rail to decrease the amount of snagging. Finally, the posts in the nested section of the guardrail could be strengthened by using a larger size post and increasing the embedment depth. This would serve to further stiffen the transition and reduce dynamic deflection. Some previous studies suggest that excessive deflection in the transition region can induce vehicle instability. However, if the system becomes too stiff, the upstream end of the transition section may need to be redesigned and evaluated. Further development, analysis, and full-scale crash testing would be required to evaluate any of these proposed modifications.

[^0]| Test Agency: Te | Test No.: 490022-4 | Test Date: 2012-05-14 |
| :---: | :---: | :---: |
| MASH Test 3-21 Evaluation Criteria | Test Results | Assessment |
| Structural Adequacy <br> A. Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable | The TxDOT TL-3 Transition contained and redirected the 2270 P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection of the metal rail element was 7.9 inches. | Pass |
| Occupant Risk <br> D. Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone. | No detached elements, fragments, or other debris was present to penetrate or show potential for penetrating the occupant compartment, or to present hazard to others in the area. | Pass |
| Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH. | Maximum occupant compartment deformation was 3.75 inches in the lateral area across the occupant compartment in the kickpanel area near the front passenger's feet. | Pass |
| F. The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees. | The 2270P vehicle rolled 90 degrees onto its right side after exiting the transition. | Fail |
| H. Longitudinal and lateral occupant impact velocities should fall below the preferred value of $30 \mathrm{ft} / \mathrm{s}$, or at least below the maximum allowable value of $40 \mathrm{ft} / \mathrm{s}$. | Longitudinal occupant impact velocity was $16.4 \mathrm{ft} / \mathrm{s}$, and lateral occupant impact velocity was $27.6 \mathrm{ft} / \mathrm{s}$. | Pass |
| I. Longitudinal and lateral occupant ridedown accelerations should fall below the preferred value of 15.0 Gs, or at least below the maximum allowable value of 20.49 Gs. | Longitudinal ridedown acceleration was 14.4 G , and lateral ridedown acceleration was 9.0 G . | Pass |
| Vehicle Trajectory <br> For redirective devices, the vehicle shall exit the barrier within the exit box (not less than 32.8 ft ). | The 2270 P vehicle exited within the exit box. | Pass |

## CHAPTER 7. IMPLEMENTATION STATEMENT

The modified transition system without curb did not meet the impact performance requirements of MASH. Consequently, no implementation is recommended at this time. Several possible design modifications are presented to mitigate the vehicle instability observed in the test. One or more if these modifications can be analyzed and evaluated at the discretion of TxDOT.

## REFERENCES

1. H. E. Ross, D. L. Sicking, R. A. Zimmer, and J. D. Michie. "Recommended Procedures for the Safety Performance Evaluation." NCHRP Report 350. National Academy Press, Washington, D.C., National Cooperative Highway Research Program, 1993.
2. AASHTO, Manual for Assessing Safety Hardware, American Association of State Highway and Transportation Officials, Washington, D.C., 2009.



ELEVATION VIEW
W6 $68.5 \times 72^{\prime \prime}$ SYTP POSTS


2a. $6^{\prime \prime} \times 8^{\prime \prime} \times 18^{\prime \prime}$ routered Wood Blockouts at posts $12-19.6^{\prime \prime} \times 8^{\prime \prime} \times 14^{\prime \prime}$ routered wood blockouts at posts $3-11$. 1-3/4" long Button-head Guardrail Bolts (FBB02) at nested thrie-beam splices. 1-1/4" long Button-head Guardrail Bolts (FBB01) at all other rail splices. $10^{\prime \prime}$ long Button-head Guardrail Bolts (FBB03) at rail to post attachments at posts 3-19. Recessed Guardrail Nuts (FBB) at all button-head bolts. 2b. Place galvanized rectangular washers (FWR03) under Guardrail Nuts at Thriebeam to Terminal Splice.
2c. Only one Rail Bolt is at post 13 , in the top slot.




HORIZONTAL PLATES
PLAN VIEWS
1/4" THICK A36

(2) VERTICAL PLATE

ELEVATION VIEW
1/4" THICK A36
$\stackrel{\sim}{\omega}$

ELEVATION VIEW
$N$
0
0
0
0
0
0
(1) FRON'T PLATE

3/16" THICK A36

Texas Transportation Institute
Project 4900224 Tl-3 Transition Drawn By GES Scale 1:10 Sheet 5 of 9 Bracket Parts
$T: \backslash 2011-2012 \backslash 490022$ TxDOT $\backslash-4$ TL-3 Transition $\backslash$ Drafting $\backslash T L-3$ Installation


## CONCRETE



$$
\begin{gathered}
\text { END VIEW } \\
\text { SCALE } 1: 20 \\
\text { SEE } 6 b
\end{gathered}
$$

Texas Transportation Institute The Texas A\&M University System College Station, Texas 77843
Project 490022-4 TL-3 Transition 2012-05-09 Drawn By GES Scale 1:50 Sheet 6 of 9 Concrete Details

## REBAR PLACEMENT

UNIESS OTHERWISE NOTED


TRANSVERSE BARS－\＃5（05／8＂）
（a） $6^{\prime \prime}$ IN TOP MAT
（a） $18^{\prime \prime}$ IN BOTTOM MAT


7a．$\varnothing 5 / 8^{\prime \prime} \times 24^{\prime \prime}$ rebar，embedded in runway minimum $6^{\prime \prime}$ with Hilti RE500 epoxy according to manufacturer＇s instructions．18＂spacing．
7b． $6^{\prime \prime}$ spacing typical for U－bars，S－bars，and top transverse bars．
7c．Horizontal spacing on S－bars may be adjusted up to $2^{\prime \prime}$ to avoid bolt sleeves．

Texas Transportation Institute
The Texas A\＆M University System Collcge Station，Texas 77843
Project 490022－4
Drawn By GES
TL－3 T
heet 7 of 9
Rebar Placement 1

## REBAR PLACEMENT




## APPENDIX B. CERTIFICATION DOCUMENTATION

MATERIAL USED
TEST NUMBER 490022-4
TEST NAME TL-3 Transition

DATE 2012-05-14

| DATE RECEIVED | ITEM NUMBER | DESCRIPTION | SUPPLIER | HEAT \# |
| :---: | :---: | :---: | :---: | :---: |
| $2012-02-08$ | Parts-16 | Guardrail Parts | Trinity | see file |
| $2012-02-23$ | Rebar $04-26$ | $1 / 2^{\prime \prime} \times 20^{\prime}$ gr 60 | CMC-Sheplers | 3029770 |
| $2012-02-23$ | Rebar $05-15$ | $5 / 8^{\prime \prime} \times 20^{\prime}$ grd 60 | CMC-Sheplers | 3028494 |



$16-40479$




Trinity Highway Products, LLC
2548 N.E. 28th St
Ft Worth, TX 7611

Customer: SAMPLES,TESTING,TRAINING MTRLS 2525 STEMMONS FRWY

DALLAS, TX 75207


Sales Order: 1164772
Customer PO: TTI-ET 2000
BOL \# 40479
Document\# 1

Print Date: 2/7/12
Project: SAMPLES \& TESTING TTI ET-2000 GILCHRIST/SH। Shipped To: TX
Use State: TX

Trinity Highway Products. LLC
Certificate Of Compliance For Trinity Industries, Inc. ${ }^{* *}$ E.T. PLUS EXTRUDER TERMINAL **
NCHRP Report 350 Compliant


Trinity Highway Products ，LLC
2548 N．E． 28 th St．
Fit Worth，TX 76111

Customer：SAMPLES，TESTING，TRANNING MTRLS 2525 STEMMONS FRWY

DALLAS，TX 75207

Sales Order： 1164772 Customer PO：TTI－ET 2000 BOL \＃ 40479 Document \＃ 1

Print Date：2／7／12
Project：SAMPLES \＆TESTING TTI ET－2000 GILCHRIST／SH hipped To：TX
Use State：TX

Trinity Highway Products．LLC
Certificate Of Compliance For Trinity Industries，Inc．＊＊E．T．PLUS EXTRUDER TERMINAL＊＊ NCHRP Report 350 Compliant

Upon delivery，all naterials subject to Trinity Highway Products，LLC Storage Stain Policy No．LG－002．
TL－3 or TL－4 COMPLIANT when installed according to manufactures specifications

ALL STEEL USED WAS MELTED AND MANUFACTURED IN USA AND COMPLIES WITH THE BUY AMERICA ACT
ALL GUARDRAIL MEETS AASHTO M－180，ALL STRUCTURAL STEEL MEETS ASTM A36
ALL COATINGS PROCESSES OF THE STEEL OR IRON ARE PERFORMED N USA AND COMPLJES WITH THE＂BUY AMERICA ACT＂ ALL GALVANIZED MATERIAL CONFORMS WITH ASTM－123，UNLESS OTHERWISE STATED．
BOLTS COMPLY WITH ASTM A－307 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A－153，UNLESS OTHERWISE STATED
NUTS COMPLY WITH ASTM A－563 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A－153，UNLESS OTHERWISE STATED．
WASHERS COMPLY WITH ASTM F－436 SPECIFICATION AND／OR F－844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM F－2329．
3／4＂DIA CABLE 6 XI9 ZNC COATED SWAGED END AISI C－1035 STEEL ANNEALED STUD I＂DIA ASTM 449 AASHTO M30，TYPE IIBREAKING
STRENGTH－ 49100 LB
State of Texas，County of Tarrant．Sworn and Subscribed before me this 7th day of February， 2012

Notary Public：
Commission Expires：


## Certified Analysis

Trinity Highway Products，LLC
2548 N．E． 28 th St
Ft Worth，TX 76111
Customer：SAMPLES，TESTING，TRAINING MTRLS 2525 STEMMONS FRWY

DALLAS，TX 75207
Order Number： 1164715
Customer PO：Samples
BOL Number： 40480
Document \＃： 1
Shipped To：TX
Use State：TX
Project：SAMPLES \＆TESTING TRAINING MTRLS

| Qty | Part\＃ | Description | Spee | CL | TY | Heat Code／Heat \＃ | Yield | Ts | Eig | c | Mn | P | S | Si | Cu | Cb | Cr | Vn | ACW |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{6}$ | 116 | $12 / 12^{16 / 31} 1.5 / \mathrm{S}$ | A－500 |  | 2 | 202248 | 53，600 | 75，500 | 29.0 | 0.190 | 0.780 | 0.011 | 0.020 | 0.120 | 0.120 | 0.00 | 0.050 | 0.002 | 4 |
|  |  |  | M－180 | $\wedge$ | 2 | 101800 | 50，000 | 73，300 | 30.0 | 0.190 | 0.750 | 0.012 | 20.002 | 0.020 | 0.120 | 0.000 | 0.070 | 0.002 | 4 |
|  |  |  | M－180 | A | 2 | 101802 | 51，800 | 74，700 | 29.0 | 0.190 | 0.770 | 0.009 | 0.002 | 0.020 | 0.120 | 0.000 | 0.050 | 0.002 | 4 |
|  |  |  | M－180 | A | 2 | 101804 | 54，500 | 75，800 | 28.0 | 0.190 | 0.800 | 0.011 | 10.002 | 0.020 | 0.120 | 0.000 | 0.050 | 0.002 | 4 |
|  |  |  | M－180 | A | 2 | 102475 | 58，700 | 79，800 | 25.0 | 0.200 | 0.820 | 0.010 | 0.010 | 0.007 | 0.130 | 0.000 | 0.050 | 0.000 | 4 |
|  | ． |  | M－180 | A | 2 | 102476 | 58，100 | 77，900 | 26.0 | 0.190 | 0.750 | 0.009 | 0.001 | 0.020 | 0.130 | 0.000 | 0.060 | 0.002 | 4 |
|  |  |  | M－180 | A | 2 | 202249 | 51，800 | 74，500 | 30.0 | 0.190 | 0.790 | 0.010 | 00.002 | 0.020 | 0.120 | 0.000 | 0.050 | 0.002 | 4 |
|  |  |  | M－180 | $\wedge$ | 2 | 202250 | 54，100 | 76，100 | 27.0 | 0.200 | 0.820 | 0.012 | 20.002 | 0.020 | 0.120 | 0.000 | 0.050 | 0.003 | 4 |
|  |  |  | M－180 | A | 2 | 202938 | 57，600 | 80，400 | 25.0 | 0.190 | 0.830 | 0.009 | 0.001 | 0.020 | 0.130 | 0.000 | 0.050 | 0.003 | 4 |
|  |  |  | M－180 | A | 2 | 202939 | 56,800 | 78，400 | 25.0 | 0.190 | 0.770 | 0.009 | 9.004 | 0.020 | 0.130 | 0.000 | 0.050 | 0.003 | 4 |
| 14 | 533G | $6^{6} 0$ POST／8．5／DDR | A．36． |  |  | 1017017 | 53，642 | 71，899 | 26.8 | 0.110 | 0.960 | 0.008 | 0.038 | 0.180 | 0.260 | 0.00 | 0.090 | 0.004 | 4 |
|  | 533G |  | A－36 |  |  | 1017007 | 53，613 | 72，244 | 25.7 | 0.120 | 0.930 | 0.012 | 0.040 | 0.180 | 0.360 | 0.00 | 0.140 | 0.003 | 4 |
|  | 533 C |  | A－36 |  |  | 1016666 | 56，666 | 73，288 | 29.7 | 0.110 | 0.940 | 0.013 | 0.037 | 0.190 | 0.320 | 0.00 | 0.150 | 0.004 | 4 |
|  | 533G |  | A．36． |  |  | 1017003 | 55，742 | 71，204 | 24.3 | 0.100 | 0.950 | 0.014 | 0.046 | 0.180 | 0.300 | 0.00 | 0.160 | 0.004 | 4 |
| 2 | 980 C | TIOEND SHOESLANT | A－36 |  |  | 125745 | 58，100 | 66，100 | 31.9 | 0.050 | 0.570 | 0.012 | 0.003 | 0.030 | 0.100 | 0.01 | 0.050 | 0.000 | 4 |
| 4 | 12227 G | T12／126／311．5：6＠16．75／S | M－180 | A | 2 | 150054 | 61，580 | 80，600 | 25.0 | 0.190 | 0.720 | 0.010 | 0.003 | 0.010 | 0.130 | 0.00 | 0.060 | 0.001 | 4 |
| 12 | 14784 G | 70 POST／8．SH13HILX | A－36 |  |  | 1014849 | 50，787 | 69，032 | 25.6 | 0.100 | 0.960 | 0.015 | 0.037 | 0.180 | 0.310 | 0.00 | 0.180 | 0.003 | 4 |
|  | 14784 G |  | A－36 |  |  | 1014844 | 53，141 | 69.983 | 28.3 | 0.110 | 0.960 | 0.010 | 0.037 | 0.180 | 0.330 | 0.00 | 0.110 | 0.003 | 4 |
|  | 147846 |  | A－36 |  |  | 1014840 | 57，069 | 73，001 | 30.4 | 0.110 | 0.960 | 0.010 | 0.035 | 0.170 | 0.320 | 0.00 | 0.150 | 0.004 | 4 |

## Certified Analysis

Trinity Highway Products, LLC
2548 N.E. 28th St.
Ft Worth, TX 76111
Customer: SAMPLES,TESTING,TRANNING MTRLS
2525 STEMMONS FRWY

DALLAS, TX 75207
Project: SAMPLES \& TESTING TRAINING MTRLS

Order Number: 1164715
Customer PO: Samples
BOL Number: 40480
Document\#: 1
Shipped To: TX
Use State: TX

| Qty | Part\# | Description | Spec | CL | TY | Heat Code Heat \# | Yield | Ts | Elg | c | Mn | P | S | Si | Cu | Cb | Cr | Vn | ACW |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 14784G |  | A.36 |  |  | 1014843 | 55.191 | 72,737 | 29.7 | 0.110 | 0.950 | 0.010 | 0.035 | 0.180 | 0.310 | 0.00 | 0.120 | 0.003 | 4 |
| 2 | 14785G | 60 POST/8.SH/3HITX | A-36 |  |  | 1013730 | 50,597 | 70,003 | 26.7 | 0.110 | 0.970 | 0.012 | 0.032 | 0.180 | 0.270 | 0.00 | 0.140 | 0.004 | 4 |
| 2 | 14786G | 60 POST/8.5ATTRANS TX | A-36 |  |  | 1014843 | 55,191 | 72,737 | 29.7 | 0.110 | 0.950 | 0.010 | 0.035 | 0.180 | 0.310 | 0.00 | 0.120 | 0.003 | 4 |
| 2 | 32218 G | TIOTRAN/TB:WB/ASYM/R | M-180 | B | 2 | 24240 | 66,000 | 77,100 | 33.1 | 0.060 | 1.250 | 0.011 | 0.004 | 0.021 | 0.030 | 0.04 | 0.030 | 0.004 | 4 |
| 2 | 35247A | CONN PL 40"X20" RT MO | A-36 |  |  | B056774 | 59,800 | 70,100 | 31.9 | 0.200 | 0.410 | 0.010 | 0.007 | 0.060 | 0.290 | 0.00 | 0.080 | 0.001 | 4 |

TL-3 or TL-4 COMPLLANT when installed according to manufactures specifications

Upon delivery, all materials subject to Trinity Highway Products , LLC Storage Stain Policy No. LG-002.
ALL STEEL USED WAS MLLTED AND MANUFACTURED IN USA AND COMPLIES WITH THE BUY AMERICA ACT.
ALL GUARDRAIL MEETS AASHTO M-180, ALL STRUCTURAL STEEL MEETS ASTM A36
ALL COATINGS PROCESSES OF THE STEEL OR IRON ARE PERFORMED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT"
ALL GALVANIZED MATERIAL CONFORMS WITH ASTM-123, UNLESS OTHERWISE STATED.
BOLTS COMPLY WITH ASTM A-307 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED.
NUTS COMPLY WITH ASTM A-563 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED.
WASHERS COMPLY WITH ASTMF-436 SPECIFICATION AND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTMF-2329.
3/4" DIA CABLE 6XI9 ZNC COATED SWAGED END AISI C-1035 STEEL ANNEALED STUD 1" DIA ASTM449 AASHTO M30, TYPE II BREAKING
STRENGTH - 49100 LB

## Certified Analysis

Trinity Highway Products, LLC
2548 N.E. 28 ht St.
Ft Worth, TX 76111
Customer: SAMPLES,TESTING,TRAINING MTRLS 2525 STEMMONS RWY

DALLAS, TX 75207
Order Number: 1164715
Customer PO: Samples BOL Number: 40480


Document \#: 1
Shipped To: TX
Use State: TX
Project: SAMPLES \& TESTING TRAINING MTRLS
State of Texas, County of Tarrant. Sworn and subscribed before me this 7th day of February, 2012


Commission Expires:


Certified By:

Gamay Luyembad
CERTIFIED MILL TEST REPORT
For additional copics call 830-372-8771 or addic 372 apics call

We hereby certify that the test results presented here are accurate and conform to the reported grade specification

Anair f. Achencte
Daniel I. Schacht
Quality Assurance Manager

| HEAT NO.:3029770 <br> SECTION: REBAR 13MME (\#4) 20'0" $420 / 60$ <br> GRADE: ASTM A615-09b G: 420160 <br> ROLL DATE: 01/22/2012 <br> MELT DATE: 01/15/2012 |  | CMC Construction Sves College Stati <br> 10650 State Hwy 30 <br> Collage Station $7 \times$ <br> US 77845-7950 <br> 9797745900 | $\begin{gathered} \mathrm{S} \\ \mathrm{H} \\ 1 \\ \mathrm{P} \\ \mathrm{~T} \end{gathered}$ | CMC Construction Svcs College Stati <br> 10650 State Hwy 30 <br> College Station TX <br> US 77845-7950 <br> 9797745900 |  | Delivery\#; 80681077 <br> BOL\#: 70240462 <br> CUST PO\#: 53534v. <br> CUST PN: <br> OLVAY LES / HEAT: 43820.000 LE <br> DLVRY PCS / HEAT: 3280 EA |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Characteristic | Value |  | Characteristic |  | Value | Characteristic | Value |
| C 0 <br> Mn 0 <br> P 0 <br> S 0 <br> Si 0 <br> Cu 0 <br> Cr 0 <br> Ni 0 <br> Mo 0 <br> V 0 <br> Cb 0 <br> Sn 0 <br> Al 0 <br>   <br> Elongation Gage Lgth test 1 8 <br> Bend Test Diameter  <br> Bend Test 1 Prength test 1 | $0.45 \%$ <br> 0.83\% <br> 0.009\% <br> $0.034 \%$ <br> $0.18 \%$ <br> $0.41 \%$ <br> $0.15 \%$ <br> 0.22\% <br> $0.070 \%$ <br> 0.002\% <br> $0.002 \%$ <br> 0.014\% <br> $0.002 \%$ <br> 65.7ksi <br> 102.8ksi <br> 12\% <br> BIN <br> 1.7501 N <br> Passed |  |  |  |  | , |  |

THIS MATERIAL IS FULUY KILLED. $100 \%$ MELTED AND MANUFAGTURED IN THE USA. WITH NO WELD REPAIR OR MERCURY CONTAMINATION IN THE PROCESS.
REMARKS :

CERTIFIED MILL TEST REPORT For additional copies call 830372.8771

Wo hereby cartify that the test results presented here are occurate and conform to the reported grade specification

$$
\begin{aligned}
& \text { Anver i. Achache } \\
& \text { Dantel 3. Schacht } \\
& \text { Qualty Assurance Naneger }
\end{aligned}
$$

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline \begin{tabular}{l}
HEAT NO．：3028494 \\
SECTION：REBAR 9 6MM（＂5）20＇0＊ \(420 / 60\) \\
GRADE：ASTM A615－09b Gr \(420 / 60\) \\
ROLL DATE：11／18／2011 \\
MELT DATE：11／14／2011
\end{tabular} \&  \& \multicolumn{2}{|l|}{\begin{tabular}{l}
CMC Construction Sves College Stati \\
10650 State Hwy 30 \\
Collage Station TX \\
US 77845－7950 \\
9797745900
\end{tabular}} \&  \& \multicolumn{3}{|l|}{\begin{tabular}{l}
CMC Construction Sucs College Stati \\
10650 State Hwy 30 \\
Collego Station TX \\
US 77845－7950 \\
9797745900
\end{tabular}} \& \multicolumn{2}{|l|}{\begin{tabular}{l}
Dalivaryf： 80669347 \\
BOL：： 70236513 \\
CUST POF：5434V \\
CUST PA： \\
DLVRY LBS／HEAT： 45990.000 LB \\
DLVRY PCS／HEAT： 2205 EA
\end{tabular}} \\
\hline Characteristic Vald \& \multicolumn{3}{|l|}{Value} \& \multicolumn{2}{|l|}{Characteristic} \& \multicolumn{2}{|l|}{Value} \& Characteristic \& Value \\
\hline  \& \begin{tabular}{l}
\(0.38 \%\) \\
1．00\％ \\
\(0.015 \%\) \\
\(0.030 \%\) \\
0．22\％ \\
0．33\％ \\
\(0.21 \%\) \\
\(0.19 \%\) \\
\(0.088 \%\) \\
\(0.003 \%\) \\
\(0.001 \%\) \\
\(0.013 \%\) \\
\(0.002 \%\) \\
68.3 ksi \\
108.1 ksi \\
15\％ \\
8IN \\
2.1881 N \\
Passed
\end{tabular} \& \begin{tabular}{l}
\％ \％ \\
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\end{tabular} \&  \&  \& \％ \& \& \&  \& \(\vdots\)
\(\vdots\)
\(\vdots\)

$\vdots$ <br>
\hline
\end{tabular}

THIS MATERIAL IS FULLY KILLED，100\％MELTED AND MANUFACTURED IN THE USA，WITH NO WELO REPAIR OR MERCURY CONTAMINATION IN THE PROCESS． REMARKS ：

Table C1．Test Day Static Soil Strength Documentation for Test No．490022－4．


Date．
2012－05－14
Test Facility and Site Location
TTI Proving Ground－3100 SH 47，Bryan，TX
In Situ Soil Description（ASTM D2487） Sandy gravel with silty fines
Fill Material Description（ASTM D2487）and sieve analysis ．．．．．AASHTO Grade B Soil－Aggregate（see sieve analysis）
Description of Fill Placement Procedure 6－inch lifts tamped with a pneumatic compactor

Table C2．Summary of Strong Soil Test Results for Establishing Installation Procedure．


Date
2008－11－05
Test Facility and Site Location
TTI Proving Ground， 3100 SH 47，Bryan，TX 77807
In Situ Soil Description（ASTM D2487
Sandy gravel with silty fines
Fill Material Description（ASTM D2487）and sieve analysis AASHTO Grade B Soil－Aggregate（see sieve analysis above）
Description of Fill Placement Procedure．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．． 6 －inch lifts tamped with a pneumatic compactor
Bogie Weight．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．． 5009 lb
Impact Velocity．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．．． 20.5 mph

## APPENDIX D. TEST VEHICLE PROPERTIES AND INFORMATION

Table D1. Vehicle Properties for Test No. 490022-4.

| Date: | $2012-05-11$ |
| :--- | :--- |
| Year: 2006 |  |

Test No.: 490022-4
Make: Dodge $\qquad$
VIN No.: 1D7HA182365659981
Model: Ram 1500

Tire Size: $\quad$ P265/70R17
Tread Type: Highway

Tire Inflation Pressure: 35 psi
Odometer: 180713

Note any damage to the vehicle prior to test:

- Denotes accelerometer location.

NOTES:


Optional Equipment:

Dummy Data:

| Type: | No dummy |
| :--- | :--- |
| Mass: |  |
| Seat Position: |  |

Geometry: inches


RANGE LIMIT: $A=78 \pm 2$ inches; $C=237 \pm 13$ inches; $E=148 \pm 12$ inches; $F=39 \pm 3$ inches; $G=>28$ inches; $H=63 \pm 4$ inches; $\mathrm{O}=43 \pm 4$ inches; $\mathrm{M}+\mathrm{N} / 2=67 \pm 1.5$ inches

GVWR Ratings:

| Front | 3700 |
| :--- | ---: |
| Back | 3900 |
|  | 6700 |

Mass: lb
$M_{\text {front }}$
$M_{\text {rear }}$
$M_{\text {Total }}$
Mass Distribution:

LF: 1424
$\qquad$

Curb

| Test Inertial |
| ---: |
| 2852 |
| 2150 |
| 5002 |

(Allowable Range for TIM and $\mathrm{G} S M=500 \overline{\mathrm{lb} \pm 110 \mathrm{lb} \text { ) }}$
lb LF: 1424 RF: 1428 LR: 1066 RR: 1084

Table D2. Vehicle Parametric Measurements for Test No. 490022-4.


$$
\text { Hood Height: } \frac{44.50}{43 \pm 4 \text { inches allowed }} \text { inches Front Bumper Height: } \quad 25.38 \text { inches }
$$

Front Overhang: $\qquad$ 36.00 inches
$39 \pm 3$ inches allowed

Table D3. Exterior Crush Measurements for Test No. 490022-4.

| Date: $2012-05-11$ | Test No.: $\frac{490022-4}{}$ | VIN No.:1D7HA182365659981  <br> Year: 2006$\quad$ Make: Dodge | Model: Ram 1500 |
| :--- | :--- | :--- | :--- |

## VEHICLE CRUSH MEASUREMENT SHEET ${ }^{1}$

| Complete When Applicable |  |
| :---: | :---: |
| End Damage | Side Damage |
| Undeformed end width $\qquad$ <br> Corner shift: A1 $\qquad$ <br> A2 $\qquad$ <br> End shift at frame (CDC) <br> (check one) <br> $<4$ inches $\qquad$ <br> $\geq 4$ inches $\qquad$ | Bowing: B1 $\qquad$ X1 <br> B2 $\qquad$ X2 <br> Bowing constant $\frac{X 1+X 2}{2}=$ $\qquad$ |

Note: Measure $\mathrm{C}_{1}$ to $\mathrm{C}_{6}$ from Driver to Passenger side in Front or Rear impacts - Rear to Front in Side Impacts.

| Specific Impact Number | Plane* of C-Measurements | Direct Damage |  | Field <br> L** | $\mathrm{C}_{3}$ | $\mathrm{C}_{2}$ | $\mathrm{C}_{3}$ | $\mathrm{C}_{4}$ | $\mathrm{C}_{5}$ | $\mathrm{C}_{6}$ | $\pm$ D |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Width** <br> (CDC) | Max*** Crush |  |  |  |  |  |  |  |  |
| 1 | Front plane at bumper ht | 16.0 | 10.0 | 27 | 0 | 2 | 4 | 4 | 6 | 10 | +10.5 |
| 2 | Side plane at bumper ht | 16.0 | 17.0 | 50 | 1 | 4 | -- | --- | 15 | 17 | +69 |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  | Measurements recorded |  |  |  |  |  |  |  |  |  |  |
|  | in inches |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |

${ }^{1}$ Table taken from National Accident Sampling System (NASS).
*Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc.
Record the value for each C -measurement and maximum crush.
**Measure and document on the vehicle diagram the beginning or end of the direct damage width and field $L$ (e.g., side damage with respect to undamaged axle).
${ }^{* * *}$ Measure and document on the vehicle diagram the location of the maximum crush.
Note: Use as many lines/columns as necessary to describe each damage profile.

Table D4. Occupant Compartment Measurements for Test No. 490022-4.


## APPENDIX E. SEQUENTIAL PHOTOGRAPHS



Figure E1. Sequential Photographs for Test No. 490022-4 (Overhead and Frontal Views).


Figure E1. Sequential Photographs for Test No. 490022-4
(Overhead and Frontal Views) (continued).


Figure E2. Sequential Photographs for Test No. 490022-4 (Rear View).


## Roll, Pitch, and Yaw Angles

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Figure F1. Vehicle Angular Displacements for Test No. 490022-4.

X Acceleration at CG


Figure F2. Vehicle Longitudinal Accelerometer Trace for Test No. 490022-4 (Accelerometer Located at Center of Gravity).

Y Acceleration at CG


Figure F3．Vehicle Lateral Accelerometer Trace for Test No．490022－4
（Accelerometer Located at Center of Gravity）．

Z Acceleration at CG


Figure F4．Vehicle Vertical Accelerometer Trace for Test No．490022－4
（Accelerometer Located at Center of Gravity）．

## X Acceleration Rear of CG



Figure F5. Vehicle Longitudinal Accelerometer Trace for Test No. 490022-4
(Accelerometer Located Rear of Center of Gravity).

## Y Acceleration Rear of CG



Figure F6. Vehicle Lateral Accelerometer Trace for Test No. 490022-4 (Accelerometer Located Rear of Center of Gravity).

Z Acceleration Rear of CG


[^1]Figure F7. Vehicle Vertical Accelerometer Trace for Test No. 490022-4
(Accelerometer Located Rear of Center of Gravity).

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http://tti.tamu.edu


[^0]:    *TTI Proving Ground's A2LA scope of accreditation does not cover recommendations. These recommendations were provided by the engineering research team.

[^1]:    - SAE Class 60 Filter

    50-msec average

